APPENDIX D

METHODOLOGY FOR DETERMINING EMISSION REDUCTIONS AND COST-EFFECTIVENESS

Zero- and Near Zero-Emission Freight Facilities Project

Mobile Source Control Division California Air Resources Board March 21, 2018





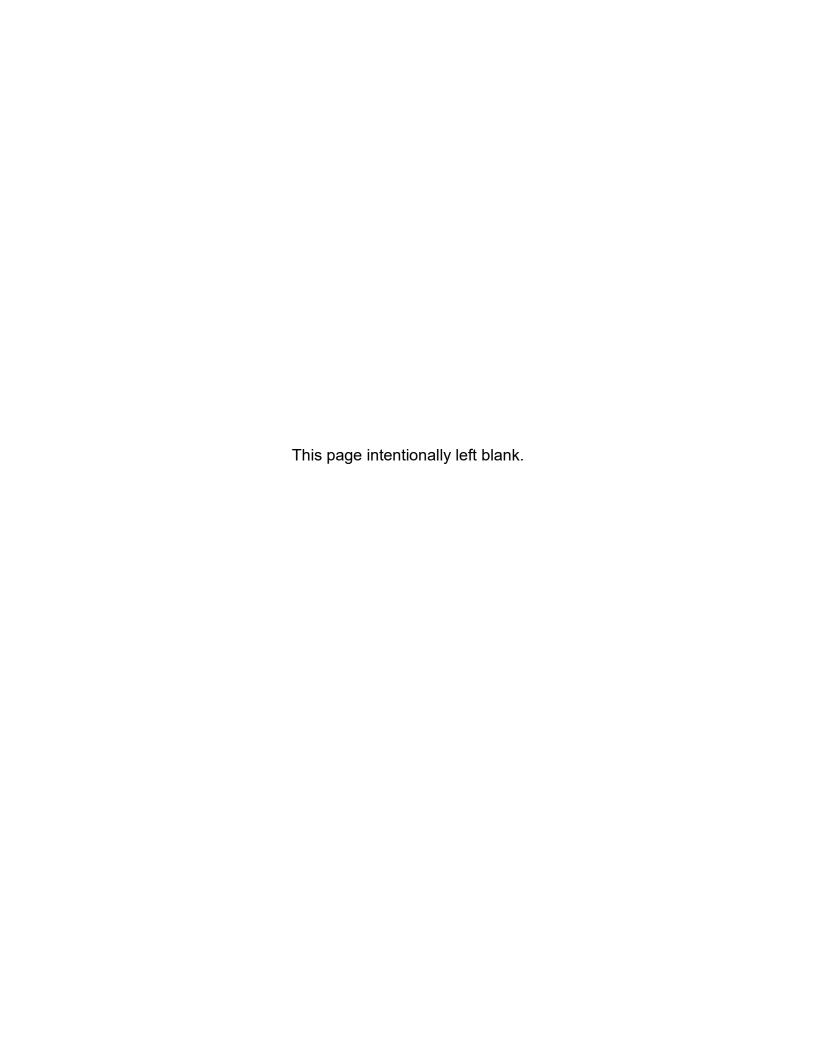


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ABBREVIATIONS

The following abbreviations are used in this appendix:

- "AQIP" means the Air Quality Improvement Program.
- "ATV" means advanced technology vehicle.
- "bhp-hr" means brake-horsepower-hour.
- "CARB" means the California Air Resources Board.
- "CARBOB" means California Reformulated Gasoline Blendstock for Oxygenate Blending.
- "CaRFG" means California reformulated gasoline.
- "CI" means carbon intensity.
- "CO2e" means carbon dioxide equivalent.
- "CNG" means compressed natural gas.
- "CRF" means capital recovery factor.
- "ED" means fuel energy density.
- "EER" means energy economy ratio.
- "EF" means emission factor.
- "ER" means emission reduction.
- "g/bhp-hr" means grams per brake-horsepower-hour.
- "gal" means gallon.
- "GHG" means greenhouse gas.
- "GVWR" means gross vehicle weight rating.
- "HC" means hydrocarbon.
- "hp" means horsepower.
- "kWh" means kilowatt-hour.
- "LNG" means liquefied natural gas.
- "LSI" means large spark-ignition.
- "MJ" means megajoule.
- "NMHC" means non-methane hydrocarbon.
- "NOx" means oxides of nitrogen.
- "PM" means particulate matter.
- "PM10" means particulate matter less than 10 microns in diameter.
- "ROG" means reactive organic gases.
- "scf" means standard cubic foot.
- "ULSD" means ultra-low sulfur diesel.
- "WER" means weighted surplus emission reduction.
- "yr" means year.

I. OVERVIEW

The methodology described within this appendix must be used to calculate the emission reductions and cost-effectiveness of projects proposed under this Solicitation. All calculations and assumptions made must be shown clearly and in their entirety in the application (Appendix A, Attachment 3).

All calculations will use the cleanest commercially available diesel-fueled engine installed in a vehicle or piece of equipment, which in many cases will employ a 2017 model year or Tier 4 Final engine, for baseline greenhouse gas (GHG) and criteria pollutant emission calculations. This technique may not adequately capture the emission profiles of all the vehicles or equipment included in an applications; however to ensure all applications are scored on an objective basis, this technique will be used for scoring all submitted applications. Alternate calculation methodologies, in addition to that required above, may be submitted to illustrate the potential emission reductions from the proposed projects.

A "well-to—wheel" analysis to quantify GHG emission reductions is required for all vehicles funded under this Solicitation. The applicant is required to determine the resulting emission reductions associated with their project (see Appendix D for the methodology). All calculations must be shown in their entirety and included in the application (see Appendix A, Attachment 3). Incomplete illustration of the mathematical processes used will result in no points being allocated for scoring criteria 5 and reduced points allocated under scoring criteria 10 in Section IV, Evaluation, Scoring, and Preliminary Selection of the solicitation, as well as possible disqualification.

If the applicant believes that the methodology for determining emission reductions and cost effectiveness does not accurately represent the emission potential of the proposed project, the applicant may submit, in addition to using the required methodology as outlined above, an alternative methodology for determining emission benefits and cost effectiveness to illustrate the potential emission reductions of the proposed technology or strategy that the applicant is proposing. Regardless of inclusion of an alternate methodology the applicant must still must utilize the required methodology as outlined in Appendix D and required under Appendix A, Attachment 3). Projects will only be scored based on the required methodology for determining emission reduction and cost effectiveness.

The GHG emission factors in Section II, below, are excerpted from the 2018 CCI Quantification Methodology Emission Factor Database. Low Carbon Fuel Standard (LCFS) regulation.¹ Please note that while the LCFS fuel carbon intensity values may change during the Solicitation period, project applicants must use the values listed in this appendix. The remaining emission factors and methodology below are from Appendices C, D, and G of the California Air Resources Board (CARB or Board)

¹ CARB, 2018; 2018 CCI Quantification Methodology Emission Factor Database https://www.arb.ca.gov/cc/capandtrade/auctionproceeds/cci_emissionfactordatabase.xlsx accessed [March 20, 2018

approved 2017 Carl Moyer Program Guidelines (Moyer Guidelines), as updated in 2017.² Language has been modified where necessary for the purposes of this Solicitation. The complete Moyer Guidelines, including all of its appendices, can be found at http://www.arb.ca.gov/msprog/moyer/guidelines/current.htm.

Emission factors for engines that meet an optional low oxides-of-nitrogen (NOx) standard are given for the purpose of this Solicitation only and are based on emission factors developed for the FY 2017-18 Clean Transportation Incentives Funding Plan (Funding Plan).

If a proposed project is for an application that uses a baseline diesel engine of 24 horsepower (hp) or lower, for the purpose of this solicitation and to calculate the needed emission reductions and cost-effectiveness, use the relevant tables for a 25 hp baseline diesel engine in the Moyer Guidelines.

Please see the example calculations provided in Section V of this Appendix to better understand how the following formulas and figures used to calculate emission reduction and cost-effectiveness values. Any examples provided herein are for reference only and do not imply additional project types or categories, nor do Carl Moyer Program funding amounts limit the amount of funding that may be available for project projects. Criteria pollutant and particulate matter (PM) table numbers are the same as those in the 2017 Moyer Guidelines. While Carl Moyer Program guidelines may change during the Solicitation period, project applicants must use the values listed in this appendix.

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² CARB, 2017; The 2017 Carl Moyer Program Guidelines, https://www.arb.ca.gov/msprog/moyer/guidelines/current.htm

II. GHG EMISSIONS CALCULATIONS³: COST-EFFECTIVENESS AND EMISSION REDUCTION FORMULAS

A. Well-to-Wheel GHG Emission Calculations

Formula 1 and Formula 2 are used to calculate the GHG emission factor in grams of carbon dioxide equivalent (CO2e) per year of use. Formula 2 is used to determine the fuel usage of the baseline vehicle or equipment.

Formula 1 calculates the greenhouse gas emission factor (GHG EF) using the carbon intensity (CI) of the fuel, the fuel's energy density, and the annual fuel usage for the technology employed in the vehicle/equipment.

Formula 1: Greenhouse Gas Emission Factor Based on Fuel Usage

$$\begin{aligned} \textit{GHG EF}\left(\frac{\textit{metric tons CO2e}}{\textit{year}}\right) &= \textit{CI} * \textit{fuel energy density} * \textit{fuel usage} * \frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}} \\ &= \left(\frac{\textit{gram CO2e}}{\textit{MJ}}\right) * \left(\frac{\textit{MJ}}{\textit{gal}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kg}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{scf}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kWh}}\right) \\ &* \left(\frac{\textit{gal}}{\textit{year}} \, \textit{or} \, \frac{\textit{kg}}{\textit{year}} \, \textit{or} \, \frac{\textit{scf}}{\textit{year}} \, \textit{or} \, \frac{\textit{kWh}}{\textit{year}}\right) * \left(\frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}}\right) \end{aligned}$$

Where CI is provided in Table II-2 and fuel energy density is provided in Table II-1.

Formula 2: Annual Fuel Usage

Formula 2 should be used to determine the fuel usage for the baseline vehicle or equipment based on hours of operations and/or miles driven and the fuel economy of the baseline vehicle or equipment.

Fuel Usage
$$\left(\frac{gal}{year}\right) = \left(\frac{gal}{mile} or \frac{gal}{hour}\right) * \left(\frac{miles}{day} or \frac{hours}{day}\right) * \left(\frac{days}{year}\right)$$

B. Conversion from Diesel Fuel Usage to Electricity / Hydrogen / CNG Usage

Formula 3 is used to calculate the advanced technology vehicle (ATV) fuel usage based on the diesel usage of the baseline vehicle/equipment calculated from Formula 2.

³ GHG emissions are measured in "CO₂ equivalent", which means the number of metric tons of CO₂ emissions with the same global warming potential as one metric ton of another greenhouse gas.

Formula 3:

$$ATV \; Fuel \; Usage \left(\frac{unit}{year}\right) = Baseline \; fuel \; usage * ED_{diesel} * \left(\frac{1}{ED_{replacement \; fuel}}\right) * \left(\frac{1}{EER}\right)$$

Where:

- ED is the fuel energy density (see Table II-1: Fuel Energy Density);
- EER is the Energy Economy Ratio value for fuels relative to diesel (see Table D-3: EER Values for Fuels Used in Light-, Medium-, and Heavy-Duty Applications); and
- **Unit** is the units associated with the replacement fuel. Electricity usage is in units of kWh, hydrogen is in kg, and CNG is in standard cubic feet (scf).

C. GHG Emission Reduction Calculation

The project's GHG emission reduction value is determined by taking the difference between the GHG emissions of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

Baseline vehicles or equipment are those using the cleanest engines commercially available at the time the application for funding is submitted, which for the purposes of this solicitation is a Tier 4 Final engine, or the cleanest 2017 model year engine if a Tier 4 Final engine is not commercially available.

Formula 4 is used to determine the annual GHG emission reductions (GHG ER_{annual}) associated with the ATV.

Formula 4:

$$Project~GHG~ER_{annual}\left(\frac{metric~tons~CO2e}{year}\right) = GHG~EF_{base} - GHG~EF_{ATV}$$

Where:

- Project GHG ER_{annual} is the annual GHG emission reductions that are associated with the proposed project;
- GHG EF_{base} is the GHG emission factor associated with the baseline vehicle or equipment that the advanced technology vehicle or equipment is compared against; and
- **GHG ERATV** is the GHG emission factor that is associated with the proposed advanced technology vehicle.

D. Cost-Effectiveness Calculations for GHG

The cost-effectiveness of a project is determined by dividing the annualized cost of the potential project by the annual emission reductions that will be achieved by the project as shown in Formula 5 below.

Formula 5 is used to determine the cost-effectiveness of the project in dollars per ton of emissions reduced.

Formula 5:

$$Cost\ Effectiveness\ \left(\frac{\$}{metric\ ton\ CO2e}\right) = \frac{\mathit{CRF}\ *\ incremental\ cost}{\mathit{Project\ GHG\ ER}_{annual}}$$

Where, for the purposes of this Solicitation:

- CRF is the Capital Recovery Factor;
- CRF₂ = 0.508 (2-year life) 4;
- $CRF_{10} = 0.106 (10-year life)^{10}$; and
- **Incremental cost** is the difference between the cost of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

E. Composite Carbon Intensity Calculations

Formula 6 below is used to determine a composite carbon intensity value in the calculations if two of the same fuel types are to be blended for use in the proposed vehicle or equipment. Use values from Table II-2: Fuel Carbon Intensity Values above as inputs into Formula 6.

Formula 6:

$$CI_{composite} = (fraction \ of \ total \ fuel * CI_{fuel \ 1}) + (fraction \ of \ total \ fuel * CI_{fuel \ 2})$$

F. Advanced Technology Efficiency Calculation

Formula 7 should be used to determine the amount of fuel per year necessary to operate an advanced technology vehicle or equipment that provides a percent efficiency improvement. Use results from Formula 2 to determine the annual fuel usage for the baseline vehicle or equipment.

Formula 7:

$$Fuel\ Usage_{ATV}\left(\frac{gal}{year}\right) =\ fuel\ usage *\left(1 - \frac{(X * Y\%\ improvement)}{100\%}\right)$$

Where:

• **X** is the fraction of the time the advanced operational efficiency technology or logistic strategy is enabled and providing emission reductions. If the advanced operational efficiency technology or logistic strategy is always engaged and providing emission reductions assume that X is equal to 1; and

⁴ CARB, 2017; The 2017 Carl Moyer Program Guidelines Appendix D: Table D-24. https://www.arb.ca.gov/msprog/moyer/guidelines/2017gl/2017 gl appendix d.pdf

• Y is the percentage fuel economy improvement that is gained by having the advanced operational efficiency technology or logistic strategy efficiency improvement over the baseline engine.

III. CRITERIA POLLUTANT AND PARTICULATE MATTER EMISSIONS CALCULATIONS: COST-EFFECTIVENESS AND EMISSION REDUCTION

Formulas are taken from Appendix C of the 2017 Moyer Guidelines. Other sections of the Moyer Guidelines are referenced as well. Language has been modified where necessary for the purposes of this Solicitation. Tables that contain emission factors and necessary inputs follow at the end of this section. Updates to these tables in the Moyer Guidelines may have been made since the release of this Solicitation. Only use the information included in the tables in this Solicitation for criteria pollutant reduction and cost-effectiveness calculations.

Baseline vehicles or equipment for the purpose of this Solicitation are the cleanest vehicle or equipment commercially available at the time the application for funding is submitted.

A. Calculating Cost-Effectiveness

The cost-effectiveness of a potential project is determined by dividing the annualized cost of the project by the annual weighted surplus emission reductions that will be achieved by the project as shown in Formula 8 below.

Formula 8: Cost-Effectiveness of Weighted Surplus Emission Reductions (\$/ton)

Where Annualized Cost is calculated using Formula 9 and Annual Weighted Surplus Emission Reductions is calculated using Formula 11.

Descriptions on how to calculate annual emission reductions and annualized cost are provided in the following sections.

B. Determining the Annualized Cost

Annualized cost is the amortization of the one-time incentive grant amount for the life of the project to yield an estimated annual cost. The annualized cost is calculated by multiplying the incremental cost by the capital recovery factor (CRF). [NOTE: For the purposes of this calculation, the CRF is 0.111, which assumes a 10-year life.] The resulting annualized cost is used to complete Formula 8 above to determine the cost-effectiveness of surplus emission reductions.

Formula 9: Annualized Cost (\$)

Annualized Cost = CRF * incremental cost (\$)

Where: $CRF_2 = 0.508$, (2 year life)⁵;

 $CRF_{10} = 0.106$, $(10-year life)^{11}$; and

Incremental cost is calculated using Formula 10.

Calculating the Incremental Cost

Formula 10: Incremental Cost (\$)

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

C. Calculating the Annual Weighted Surplus Emission Reductions

Annual weighted surplus emission reductions (WER) are estimated by taking the sum of the project's annual surplus pollutant reductions following Formula 11 below. This will allow projects that reduce one, two, or all three of the covered pollutants to be evaluated. While NOx and ROG emissions are given equal weight, emissions of PM carry a greater weight in the calculation.

Formula 11: Annual Weighted Surplus Emission Reductions (tons/yr)

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

The result of Formula 11 is used to complete Formula 8 to determine the costeffectiveness of surplus emission reductions.

In order to determine the annual surplus emission reductions by pollutant, emission reduction calculations need to be completed for each pollutant (NOx, ROG, and PM), for the baseline technology and the advanced technology, totaling up to six calculations:

| Baseline Technology | Advanced Technology |
|----------------------------|----------------------------|
| 1. Annual emissions of NOx | 4. Annual emissions of NOx |
| 2. Annual emissions of ROG | 5. Annual emissions of ROG |
| 3. Annual emissions of PM | 6. Annual emissions of PM |

These calculations are completed for each pollutant by multiplying the engine emission factor or converted emission standard by the annual activity level of the technology and by other adjustment factors as specified for the calculation methodologies presented.

⁵ CARB, 2017; The 2017 Carl Moyer Program Guidelines Appendix D: Table d-25. https://www.arb.ca.gov/msprog/moyer/guidelines/2017gl/2017 gl appendix d.pdf

D. Calculating Annual Emission Reductions based on Usage

1. Calculating Annual Emission Reductions Based on Hours of Operation

When actual annual hours of equipment operation are the basis for determining emission reductions, use Formula 12 below.

Formula 12: Estimated Annual Emission Reductions Based on Hours of Operation (tons/year)

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * Horsepower * Load Factor * Activity (hrs/yr) * Percent Operation in California * ton/907,200g

Where the Emission Factor is provided in Table IV-3, IV-4, IV-6, IV-7, IV-9, IV-10, IV-11, IV-12a, IV-12b, IV-14a, IV-14b, IV-15a, or IV-15b; the Converted Emission Standard is provided in Table IV-1 or IV-2; and the Load Factor is provided in Table IV-5, IV-8, or IV-16.

2. Calculating Annual Emissions Based on Fuel Consumption

When annual fuel consumption is used for determining emission reductions, the equipment activity level must be based on annual fuel usage within California provided by the applicant.

A fuel consumption rate factor must be used to convert emissions given in g/bhp-hr to units of grams of emissions per gallon of fuel used (g/gal). The fuel consumption rate factor is a number that combines the effects of engine efficiency and the energy content of the fuel used in that engine into an approximation of the amount of work output by an engine for each unit of fuel consumed. Formulas 13 and 14 below are the formulas for calculating annual emissions based on annual fuel consumed.

Formula 13: Estimated Annual Emissions based on Fuel Consumed using Emission Factors or Converted Emission Standard (tons/yr)

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

Where the fuel consumption rate factor is provided in Table IV-19.

Formula 14: Estimated Annual Emissions based on Fuel using Emission Factors (tons/yr)

Annual Emission Reductions =

Emission Factor (g/gal) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

E. List of Criteria Pollutant Cost-Effectiveness Formulas

For an easy reference, the necessary formulas to calculate the cost-effectiveness of surplus emission reductions for a project funded through the Carl Moyer Program are provided below.

Formula 8: Cost-Effectiveness of Weighted Surplus Emission Reductions (\$/ton):

Cost-Effectiveness (\$/ton) = Annualized Cost (\$/year)

Annual Weighted Surplus Emission Reductions (tons/yr)

Formula 9: Annualized Cost (\$)

Annualized Cost = CRF * incremental cost (\$)

Formula 10: Incremental Cost (\$)

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

Formula 11: Annual Weighted Surplus Emission Reductions

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

Formula 12: Estimated Annual Emission Reductions Based on Hours of Operation (tons/year)

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * Horsepower * Load Factor * Activity (hrs/yr) * Percent Operation in California * ton/907,200g

Formula 13: Estimated Annual Emissions based on Fuel Consumed using Emission Factors or Converted Emission Standard (tons/yr)

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

Formula 14: Estimated Annual Emissions based on Fuel using Emission Factors (tons/yr)

Annual Emission Reductions =

Emission Factor (g/gal) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

IV. EXAMPLE CALCULATIONS

Example calculations are provided to illustrate many of the permutations that staff expects may be included in an application for funding. Example calculations are included for eight scenarios providing the values that are needed for a complete application. Those required values are:

- GHG annual emission reductions from each proposed vehicle or piece of equipment;
- Criteria pollutant and toxic air contaminant annual pollutant emission reductions for each proposed vehicle or piece of equipment;
- GHG reduction cost-effectiveness for a two-year life during the time of the proposed project;
- GHG reduction cost-effectiveness for a 10-year life, two years after the end of the proposed project, assuming the technology is fully commercialized and integrated into the marketplace at numbers described in the application;
- Criteria pollutant and toxic air contaminant reduction cost-effectiveness for a two-year life during the time of the proposed project;
- Criteria pollutant and toxic air contaminant reduction cost-effectiveness for a 10-year life, two years after the end of the proposed project, assuming the technology is fully commercialized and integrated into the marketplace at numbers described in the application;
- GHG reduction cost effectiveness for an entire proposed project, during the time of the proposed project; and
- Criteria pollutant and toxic air contaminant reduction cost effectiveness for an entire proposed project, during the time of the proposed project

GHG emission reductions are calculated on a well-to-wheel basis and the criteria pollutant emission reductions are determined under a tank-to-wheel scenario. The example calculations contained in this appendix are illustrations of:

Example A: Battery-Electric Heavy-Lift Forklift:

 This example assumes that a heavy-lift forklift will have the same energy requirements as a diesel counterpart and will be used the same number of hours. Electricity to charge the proposed forklift will come from the electrical grid.

Example B: Fuel Cell Top Handler:

 This example assumes that a fuel cell top handler will have the same energy requirements as a diesel counterpart and will be used the same number of hours. It is assumed that this project will use hydrogen that is SB 1505 compliant and therefore, has a 1/3 renewable component.

Example C: Battery-Electric Switch Locomotive with Fuel Cell Range Extender:

• This example assumes that a fuel cell switcher locomotive with battery storage will have the same energy requirements as a diesel-electric counterpart and will be used the same number of hours. Further, it is assumed that in this project, continuous power is provided by the fuel cell and peak power requirements are provided by the on-board traction battery. It is assumed that half of the advanced technology vehicle's energy needs will come from the on-board battery pack and that half of the vehicle's energy needs will come from the on-board range extending engine.

Example D: Logistic Strategy for Container Movement Technology:

 This example assumes that a piece of cargo handling equipment utilizing advanced logistic technology will have the same energy requirements as a diesel counterpart without the logistic technology and will be used the same number of hours. The logistic strategy is only functional while loading and unloading ocean going vessels and therefore, will only be engaged half of the time during the cargo handling equipment's operation.

Example E: Fuel Cell Regional Haul Truck"

• This example assumes that a fuel cell on-road regional haul truck will have the same energy requirements as a diesel counterpart and will be used the same number of miles. The proposed truck in this example will not be plugged in to the electrical grid to charge on-board battery packs, but will use the on-board fuel cell. Further, it is assumed that this project will use hydrogen that is produced from natural gas and compressed for use in the project.

Example F: Fuel Cell Transportation Refrigeration Unit:

 This example shows a project that proposes to utilize a hydrogen fuel cell as the power source for a transportation refrigeration unit. The hydrogen refueling station is proposed to be funded by the AQIP/GGRF grant and therefore must utilize renewable hydrogen as required by SB 1505.

Example G: Facility Efficiency Improvement:

• This example shows the emission reductions by increasing the efficiency at a freight facility by installing advanced technologies that reduce the electrical needs of a freight facility by 10%.

Example H: Project Wide Summation of Emission Reductions and Cost Effectiveness Determination:

• This example shows the summation of the emission reductions and cost effectiveness from an entire project utilizing the example calculations for specific vehicle and equipment types and including reductions from the freight facility efficiency improvement project. This calculation is to illustrate the emission reductions for the entire project and the determination of cost effectives for the entire project using the summation of emission reductions from each aspect of the project and using the total project cost as a basis for that determination.

All of the following examples assume diesel fuel usage by the baseline vehicle or equipment as a basis for the GHG and criteria pollutant emission calculations and grid electricity as the basis of determining GHG emission reductions from freight facility improvements. This technique may not adequately capture the emission profiles of all proposed applications; however; this technique is used to allow all submitted applications to be scored objectively. If an applicant feels that this methodology does not capture the emission reductions from their proposed project, the applicant can submit an alternative methodology, in addition to the required methodology, to illustrate the potential emission reductions

If a proposed project is for an application that uses a baseline diesel engine of 24 hp or lower, for the purpose of this solicitation and to calculate the needed emission reductions and cost-effectiveness, use the relevant tables for a 25 hp baseline diesel engine in the Moyer Guidelines.

A. Example A: Battery-Electric Heavy-Lift Forklift

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a heavy-lift forklift will have the same energy requirements as a diesel counterpart and will be used the same number of hours. Electricity to charge the proposed forklift will come from the electrical grid.

Baseline Diesel Forklift:

- Off-Road diesel engine: Tier 4 Final certification, 110 hp
- 19,000 lbs. lift capacity
- Diesel usage: 2 gallons per hour, 3,000 gallons per year
- Operation: 1,500 hours per year
- Forklift cost at project : \$40,000
- Forklift cost two years after project: \$40,000

Advanced Technology:

- Battery-electric forklift
- Forklift cost at project : \$75,000
- Forklift cost two years after project: \$65,000

Variables Used in Calculation:

Carbon Intensity

From Table II-2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$Cl_{diesel} = \frac{102.01 g CO2e}{MI}$$
 Table Pathway Identifier ULSD001

$$Cl_{electricity} = \frac{105.15 \ g \ CO2e}{MJ}$$
 Table Pathway Identifier ELC001

Energy Density

From Table II-1: Fuel Energy Density

ED = Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel} \qquad \qquad \mathsf{ED}_{\mathsf{electricity}} = \frac{3.60 \, MJ}{kWh}$$

Energy Efficiency Ratio

From Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

EER = Energy Efficiency Ratio (unit less)

 $EER_{electricity} = 5.5$

Step 1: Convert the diesel used per year to the amount of electricity needed to do the same work using Formula 3 and the variables identified above.

Formula 3:

$$Replacement \ Fuel \ Usage \left(\frac{unit}{year}\right) = fuel \ usage * ED_{diesel} * \left(\frac{1}{ED_{replacement \ fuel}}\right) * \left(\frac{1}{EER}\right)$$

Where:

- ED is the fuel energy density (see Table II-1: Fuel Energy Density);
- **EER** is the Energy Economy Ratio value for fuels relative to diesel (see Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications);
- **Unit** is the units associated with the replacement fuel. Electricity is in terms of kWh, hydrogen is in kg, and CNG is in scf.

$$\begin{aligned} Replacement \ Fuel \ Usage \left(\frac{unit}{year}\right) &= \left(3,000 \frac{gal \ diesel}{year}\right) * \left(\frac{134.47 \ MJ}{1 \ gal \ diesel}\right) * \left(\frac{1 \ kWh}{3.60 \ MJ}\right) * \left(\frac{1}{5.5}\right) \\ &= 20,374 \frac{kWh}{year} \end{aligned}$$

Step 2: Determine the GHG emissions that are attributed to the baseline diesel-fueled heavy-lift forklift using Formula 1 and the variables identified above.

Formula 1:

$$\begin{aligned} \textit{GHG EF}\left(\frac{\textit{metric tons CO2e}}{\textit{year}}\right) &= \textit{CI} * \textit{fuel energy density} * \textit{fuel usage} * \frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}} \\ &= \left(\frac{\textit{gram CO2e}}{\textit{MJ}}\right) * \left(\frac{\textit{MJ}}{\textit{gal}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kg}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{scf}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kWh}}\right) \\ &* \left(\frac{\textit{gal}}{\textit{year}} \, \textit{or} \, \frac{\textit{kg}}{\textit{year}} \, \textit{or} \, \frac{\textit{scf}}{\textit{year}} \, \textit{or} \, \frac{\textit{kWh}}{\textit{year}}\right) * \left(\frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}}\right) \end{aligned}$$

$$GHG\ EF_{base} = \left(\frac{102.01\ gram\ CO2e}{MJ}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \left(\frac{3,000\ gal\ diesel}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 41\frac{metric\ tons\ CO2e}{vear}$$

Step 3: Determine the GHG emissions that are attributed to the advanced technology forklift using Formula 1, the result from Step 1 and the variables identified above.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right)*\left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\ or\ \frac{MJ}{kWh}\right)$$

$$*\left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\ or\ \frac{kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{ATV} = \left(\frac{105.16\ gram\ CO2e}{MJ}\right)*\left(\frac{3.60\ MJ}{kWh}\right)*\left(\frac{20,374\ kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 7.7\frac{metric\ tons\ CO2e}{year}$$

Step 4: Determine the GHG emission reductions that are associated with the proposed project using Formula 4, populated by results from Step 2 and Step 3 above to give the GHG emission benefit from the proposed project.

Formula 4:

$$Project~GHG~ER_{annual}\left(\frac{metric~tons~CO2e}{year}\right) = GHG~EF_{base} - GHG~EF_{ATV}$$

Where:

- GHG ER_{annual} is the annual GHG emission reductions that are associated with the proposed project;
- GHG EF_{base} is the GHG emission factor associated with the base case vehicle or equipment that the advanced technology vehicle or equipment is compared against; and
- GHG ERATV is the GHG emission factor that is associated with the proposed advanced technology vehicle.

$$\begin{aligned} &Project\ GHG\ ER_{annual} = \left(41\frac{metric\ tons\ CO2e}{year}\right) - \left(7.7\frac{metric\ tons\ CO2e}{year}\right) \\ &= 33\frac{metric\ tons\ CO2e}{year} \end{aligned}$$

Step 5: Determine the annual criteria pollutant emission reductions that are associated with the proposed project. The baseline diesel-fueled forklift is using a 110 hp diesel engine that is certified to the Tier 4 Final emissions standard, therefore, using emission values from Table IV-7 and fuel consumption rate factors from Table IV-19, the result of Step 1 above to populate Formula 13. The forklift will be used 100% of the time in California. There are no criteria pollutant emissions associated with the use of the battery-electric forklift in a tank-to-wheel analysis.

For a Tier 4 Final off-road engine at 110 hp, Table IV-7 gives criteria pollutant emissions per bhp-hr and Table IV-5 gives the load factor. Therefore:

NOx =
$$0.26 \frac{g NOx}{bhv-hr}$$
; ROG = $0.05 \frac{g ROG}{bhv-hr}$; PM10 = $0.009 \frac{g PM10}{bhv-hr}$

Load Factor industrial forklift = 0.20

Formula 12:

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * Horsepower * Load Factor * Activity (hrs/yr) * Percent Operation in California * ton/907,200g

Annual
$$ER_{NOx} = \left(0.26 \frac{g \, NOx}{bhp-hr}\right) * (110 \, hp) * (0.20) * \left(1,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$$

$$= 0.009 \frac{tons \, NOx}{year}$$
Annual $ER_{ROG} = \left(0.05 \frac{g \, NOx}{bhp-hr}\right) * (110 \, hp) * (0.20) * \left(1,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$

$$= 0.002 \frac{tons \, ROG}{year}$$
Annual $ER_{PM10} = \left(0.009 \frac{g \, PM10}{bhp-hr}\right) * (110 \, hp) * (0.20) * \left(1,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$

$$= 0.0003 \frac{tons \, PM10}{year}$$

Step 6: Determine the weighted annual surplus emission reductions that are associated with the proposed project. Use the results from Step 5 above along with the realization that the proposed battery-electric forklift will not produce any criteria pollutant emissions in a tank-to-wheel scenario to populate Formula 11.

Formula 11:

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

$$WER = \left(0.009 \frac{tons\ NOx}{year}\right) + \left(0.002 \frac{tons\ ROG}{year}\right) + \left(20*0.0003 \frac{tons\ PM}{year}\right)$$
$$= 0.017 \frac{tons}{year}$$

Step 7: Determine the incremental cost of the proposed technology using Formula 10 and the equipment costs for the baseline diesel-fueled forklift and the battery-electric heavy lift forklift given at the start of this example. Cost-effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Baseline Equipment:

Forklift cost at project : \$40,000

• Forklift cost two years after project: \$40,000

Advanced Technology:

Forklift cost at project: \$75,000

Forklift cost two years after project : \$65,000

Formula 10:

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

Incremental Cost_{2 years} = \$75,000 - \$40,000 = \$35,000

Incremental Cost_{10 years} = \$65,000 - \$40,000 = \$25,000

Step 8: Determine the GHG emission reduction cost-effectiveness for the proposed project using Formula 5 and the results from Step 4 and Step 7.

Formula 5:

$$GHG\ Cost\ Effectiveness\ \left(\frac{\$}{metric\ ton\ CO2e}\right) = \frac{CRF\ *\ incremental\ cost}{Project\ GHG\ ER_{annual}}$$

Where, for the purposes of this Solicitation:

- CRF is the Capital Recovery Factor;
- CRF₂ = 0.508, per Moyer Table D-25 (2-year life);
- CRF₁₀ = 0.106, per Moyer Table D-25 (10-year life); and
- Incremental cost is the difference between the cost of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

$$GHG\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$35,000)}{\left(33\ \frac{metric\ tons\ CO2e}{year}\right)}$$

= \$539 per metric ton CO2e reduced

GHG Cost Effectiveness_{10 years} =
$$\frac{(0.106 * $25,000)}{\left(33 \frac{metric tons CO2e}{year}\right)}$$

= \$80 per metric ton CO2e reduced

Step 9: Determine the criteria pollutant cost-effectiveness for the proposed technology. Use the results from Step 6 and Step 7 to populate Formula 8.

Formula 8:

$$WER\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$35,000)}{\left(0.017\ \frac{tons\ WER}{year}\right)}$$

= \$1,050.000 per ton weighted criteria pollutants reduced

WER Cost Effectiveness_{10 years} =
$$\frac{(0.106 * $25,000)}{\left(0.017 \frac{tons WER}{year}\right)}$$

 $=\$156,\!000\ per\ ton\ weighted\ criteria\ pollutants\ reduced$

B. Example B: Fuel Cell Top Handler

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a fuel cell top handler will have the same energy requirements as a diesel counterpart and will be used the same number of hours. It is assumed that this project will use hydrogen that is SB 1505 compliant and therefore, has 1/3 renewable component.

Baseline Diesel Top Handler:

- Off-road diesel engine: Tier 4 final certification, 300 hp
- Diesel usage: 7.5 gallons per hour
- Operation: 2,500 hours per year, 18,750 gallons of diesel consumed per year
- Top handler cost at project : \$550,000
- Top handler cost two years after project : \$550,000

Advanced Technology:

- Hydrogen fuel cell top handler
- Top Handler cost at project: \$1,000,000
- Top Handler cost two years after project: \$750,000

Variables Used in Calculation:

Carbon Intensity

From Table II-2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$Cl_{diesel} = \frac{102.01 g CO2e}{MI}$$
 Table Pathway Identifier ULSD001

$$CI_{hydrogen} = \frac{88.33 g co2e}{MJ}$$
 Table Pathway Identifier HYGN005

Energy Density

From Table II-1: Fuel Energy Density

ED = Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel} \qquad \qquad \mathsf{ED}_{\mathsf{hydrogen}} = \frac{119.99 \, MJ}{kg}$$

Energy Efficiency Ratio

From Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

EER = Energy Efficiency Ratio (unit less)

EER_{fuel cell vehicle} = 1.9

Step 1: Convert the diesel used per year to the amount of hydrogen needed to do the same work using Formula 3 and the variables identified above.

Formula 3:

Replacement Fuel Usage
$$\left(\frac{unit}{year}\right) = fuel \ usage * ED_{diesel} * \left(\frac{1}{ED_{replacement \ fuel}}\right) * \left(\frac{1}{EER}\right)$$

Where:

- ED is the fuel energy density (see Table II-1: Fuel Energy Density);
- EER is the Energy Economy Ratio value for fuels relative to diesel (see Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications);
- Unit is the units associated with the replacement fuel. Electricity is in terms
 of kWh, hydrogen is in kg, and CNG is in scf.

Replacement Fuel Usage
$$\left(\frac{unit}{year}\right) = \left(\frac{18,750 \ gal \ diesel}{year}\right) * \left(\frac{134.47 \ MJ}{1 \ gal \ diesel}\right) * \left(\frac{1 \ kg}{119.99 \ MJ}\right) * \left(\frac{1}{1.9}\right)$$

$$= 11,059 \ \frac{kg \ hydrogen}{year}$$

Step 2: Determine the GHG emissions that are attributed to the baseline diesel-fueled top handler. Using Formula 1 and the variables identified above.

Formula 1:

$$\begin{aligned} \textit{GHG EF}\left(\frac{\textit{metric tons CO2e}}{\textit{year}}\right) &= \textit{CI} * \textit{fuel energy density} * \textit{fuel usage} * \frac{1 \textit{ metric ton CO2e}}{1,000,000 \textit{ grams}} \\ &= \left(\frac{\textit{gram CO2e}}{\textit{MJ}}\right) * \left(\frac{\textit{MJ}}{\textit{gal}} \textit{ or } \frac{\textit{MJ}}{\textit{kg}} \textit{ or } \frac{\textit{MJ}}{\textit{scf}} \textit{ or } \frac{\textit{MJ}}{\textit{kWh}}\right) \\ &* \left(\frac{\textit{gal}}{\textit{vear}} \textit{ or } \frac{\textit{kg}}{\textit{vear}} \textit{ or } \frac{\textit{scf}}{\textit{vear}} \textit{ or } \frac{\textit{kWh}}{\textit{vear}}\right) * \left(\frac{1 \textit{ metric ton CO2e}}{1,000,000 \textit{ grams}}\right) \end{aligned}$$

$$GHG\ EF_{base} = \left(\frac{102.01\ g\ CO2e}{MJ}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \left(\frac{18,750\ gal\ diesel}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 257\frac{metric\ tons\ CO2e}{vear}$$

Step 3: Determine the GHG emissions that are attributed to the advanced technology top handler. Using Formula 1, the result from Step 1 and the variables identified above.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right)*\left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\ or\ \frac{MJ}{kWh}\right)$$

$$*\left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\ or\ \frac{kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{ATV} = \left(\frac{88.33\ gram\ CO2e}{MJ}\right)*\left(\frac{119.99\ MJ}{kg}\right)*\left(\frac{11,059\ kg}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 117\frac{metric\ tons\ CO2e}{year}$$

Step 4: Determine the GHG emission reductions that are associated with the proposed project. Using Formula 4, populated by results from Step 2 and Step 3 above to give the GHG emission benefit from the proposed project.

Formula 4:

$$Project\ GHG\ ER_{annual}\left(\frac{metric\ tons\ CO2e}{year}\right) = GHG\ EF_{base} - GHG\ EF_{ATV}$$

Where:

- GHG ER_{annual} is the annual GHG emission reductions that are associated with the proposed project;
- GHG EF_{base} is the GHG emission factor associated with the base case vehicle or equipment that the advanced technology vehicle or equipment is compared against; and
- GHG ERATV is the GHG emission factor that is associated with the proposed advanced technology vehicle.

$$\begin{aligned} & \textit{Project GHG ER}_{annual} = \left(257 \frac{\textit{metric tons CO2e}}{\textit{year}}\right) - \left(117 \frac{\textit{metric tons CO2e}}{\textit{year}}\right) \\ &= 140 \frac{\textit{metric tons CO2e}}{\textit{year}} \end{aligned}$$

Step 5: Determine the annual criteria pollutant emission reductions that are associated with the proposed project. The baseline diesel-fueled top handler is using a 300 hp diesel engine that is certified to the Tier 4 Final emissions standard, therefore, using emission values from Table IV-7 and off-road load factors from Table IV-5, the result of Step 1 above to populate Formula 12. The top handler will be used 100% of the time in California. There are no criteria pollutant emissions associated with the use of the hydrogen fuel cell top handler in a tank-to-wheel analysis.

For a Tier 4 Final off-road engine at 300 hp, Table IV-7 gives criteria pollutant emissions per bhp-hr and Table IV-5 gives the load factor. Therefore:

NOx =
$$0.26 \frac{g NOx}{bhv-hr}$$
; ROG = $0.05 \frac{g ROG}{bhv-hr}$; PM10 = $0.009 \frac{g PM10}{bhv-hr}$

Load Factorcontainer handling equipment = 0.59

Formula 12:

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * Horsepower * Load Factor * Activity (hrs/yr) * Percent Operation in California * ton/907,200g

Annual
$$ER_{NOx} = \left(0.26 \frac{g \, NOx}{bhp-hr}\right) * (300 \, hp) * (0.59) * \left(2,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$$

$$= 0.127 \frac{tons \, NOx}{year}$$
Annual $ER_{ROG} = \left(0.05 \frac{g \, NOx}{bhp-hr}\right) * (300 \, hp) * (0.59) * \left(2,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$

$$= 0.024 \frac{tons \, ROG}{year}$$
Annual $ER_{PM10} = \left(\frac{0.009 \, g \, PM10}{bhp-hr}\right) * (300 \, hp) * (0.59) * \left(2,500 \frac{hours}{year}\right) * (1) * \left(\frac{1 \, ton}{907,200 \, grams}\right)$

$$= 0.004 \frac{tons \, PM10}{year}$$

Step 6: Determine the weighted annual surplus emission reductions that are associated with the proposed project. Using the results from Step 5 above along with the realization that the proposed battery-electric forklift will not produce any criteria pollutant emissions in a tank-to-wheel scenario, populate Formula 11.

Formula 11:

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

$$WER = \left(0.127 \frac{tons\ NOx}{year}\right) + \left(0.024 \frac{tons\ ROG}{year}\right) + \left(20 * 0.004 \frac{tons\ PM}{year}\right)$$
$$= 0.231 \frac{tons}{year}$$

Step 7: Determine the incremental cost of the proposed technology using Formula 10 and the equipment costs for the baseline diesel-fueled top handler and the fuel cell top handler given at the start of this example. Cost-effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Baseline Equipment:

Top handler cost at Project : \$550,000

• Top handler cost two years after project: \$550,000

Advanced Technology:

• Top handler cost at project: \$1,000,000

Top handler cost two years after project : \$750,000

Formula 10:

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

Incremental Cost_{2 years} = \$1,000,000 - \$550,000 = \$450,000

Incremental Cost_{10 years} = \$750,000 - \$550,000 = \$200,000

Step 8: Determine the GHG emission reduction cost-effectiveness for the proposed project using Formula 5 and the results from Step 4 and Step 7.

Formula 5:

$$Cost\ Effectiveness\ \left(\frac{\$}{metric\ ton\ CO2e}\right) = \frac{CRF\ *\ incremental\ cost}{Project\ GHG\ ER_{annual}}$$

Where, for the purposes of this Solicitation:

- CRF is the Capital Recovery Factor;
- CRF₂ = 0.515, per Moyer Table G-3a (2-year life);
- CRF₁₀ = 0.111, per Moyer Table G-3a (10-year life); and
- **Incremental cost** is the difference between the cost of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

$$GHG\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$450,000)}{\left(140\ \frac{metric\ tons\ CO2e}{year}\right)}$$

= \$1,630 per metric ton CO2e reduced

GHG Cost Effectiveness_{10 years} =
$$\frac{(0.106 * $200,000)}{\left(140 \frac{metric tons CO2e}{year}\right)}$$

= \$151 per metric ton CO2e reduced

Step 9: Determine the criteria pollutant cost-effectiveness for the proposed technology. Use the results from Step 6 and Step 7 to populate Formula 8.

Formula 8:

$$WER\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$450,000)}{\left(0.231\ \frac{tons\ WER}{year}\right)}$$

 $=\$990,\!000~per~ton~weighted~criteria~pollutants~reduced$

WER Cost Effectiveness_{10 years} =
$$\frac{(0.106 * $200,000)}{\left(0.231 \frac{tons WER}{year}\right)}$$

= \$91,800 per ton weighted criteria pollutants reduced

C. Example C: Battery-Electric Switch Locomotive with Fuel Cell Range Extender

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a fuel cell locomotive with battery storage will have the same energy requirements as a diesel-electric counterpart and will be used the same number of hours. Further, it is assumed that in this project, continuous power is provided by the fuel cell and peak power requirements are provided by the on-board traction battery. It is assumed that half of the advanced technology vehicle's energy needs will come from the on-board battery pack and that half of the vehicle's energy needs will come from the on-board range extending engine. It is assumed that this project will use hydrogen that is SB 1505 compliant and therefore, has 1/3 renewable component.

Baseline Locomotive:

- Off-road diesel engine with electric drivetrain: Tier 4 certification, 1,500 hp
- Diesel usage: 23 gallons per hour
- Operation: 6,000 hours per year, 138,000 gallons per year
- Locomotive cost at project : \$1,500,000
- Locomotive cost two years after project: \$1,500,000

Advanced Technology:

- Battery-electric locomotive with fuel cell range extender
- Energy requirements during operation: 50% on electricity, 50% on hydrogen
- Locomotive cost at project: \$3,500,000
- Locomotive cost two years after project : \$2,500,000

Variables Used in Calculation:

Carbon Intensity

From Table II-2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$CI_{diesel} = \frac{102.01 g CO2e}{MI}$$
 Table Pathway Identifier ULSD001

$$Cl_{electricity} = \frac{105.15 \ g \ CO2e}{MI}$$
 Table Pathway Identifier ELC001

$$CI_{hydrogen} = \frac{88.33 g CO2e}{MI}$$
 Table Pathway Identifier HYGN005

Energy Density

From Table II-1: Fuel Energy Density

ED = Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel} \qquad \qquad \mathsf{ED}_{\mathsf{hydrogen}} = \frac{119.99 \, MJ}{kg}$$

$$\mathsf{ED}_{\mathsf{electricity}} = \frac{3.60 \, MJ}{kWh}$$

Energy Efficiency Ratio

From Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

EER = Energy Efficiency Ratio (unit less)

Step 1: Convert the diesel used per year to the amount of electricity and hydrogen needed to do the same work using Formula 3 and the variables identified above.

Formula 3:

$$Replacement \ Fuel \ Usage \left(\frac{unit}{year}\right) = fuel \ usage * ED_{diesel} * \left(\frac{1}{ED_{replacement \ fuel}}\right) * \left(\frac{1}{EER}\right)$$

Where:

- ED is the fuel energy density (see Table II-1: Fuel Energy Density);
- EER is the Energy Economy Ratio value for fuels relative to diesel (see Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications);
- **Unit** is the units associated with the replacement fuel. Electricity is in terms of kWh, hydrogen is in kg, and CNG is in scf.

$$Replacement \ Fuel \ Usage_{electricity} = \left(\frac{69,000 \ gal \ diesel}{year}\right) * \left(\frac{134.47 \ MJ}{1 \ gal \ diesel}\right) * \left(\frac{1 \ kWh}{3.60 \ MJ}\right) * \left(\frac{1}{4.6}\right) = 560,000 \ \frac{kWh}{year}$$

$$\begin{aligned} \textit{Replacement Fuel Usage}_{\textit{hydrogen}} &= \left(\frac{69,000 \; gal \; diesel}{\textit{year}}\right) * \left(\frac{134.47 \; \textit{MJ}}{1 \; gal \; diesel}\right) * \left(\frac{1 \; kg}{119.99 \; \textit{MJ}}\right) * \left(\frac{1}{1.9}\right) \\ &= 40,700 \; \frac{\textit{kg hydrogen}}{\textit{year}} \end{aligned}$$

Step 2: Determine the GHG emissions that are attributed to the baseline diesel-fueled locomotive using Formula 1 and the variables identified above.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right)*\left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\ or\ \frac{MJ}{kWh}\right)$$

$$*\left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\ or\ \frac{kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{base} = \left(\frac{102.01\ g\ CO2e}{MJ}\right)*\left(\frac{134.47\ MJ}{gal\ diesel}\right)*\left(\frac{138,000\ gal\ diesel}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 1,893\ \frac{metric\ tons\ CO2e}{year}$$

Step 3: Determine the GHG emissions that are attributed to the advanced technology locomotive. Use Formula 1, the result from Step 1, and the variables identified above to calculate the GHG emissions for electricity and hydrogen separately, then add together.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right)*\left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\ or\ \frac{MJ}{kWh}\right)$$

$$*\left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\ or\ \frac{kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{electricity} = \left(\frac{105.16\ g\ CO2e}{MJ}\right)*\left(\frac{3.60\ MJ}{kWh}\right)*\left(\frac{560,000\ kWh}{year}\right)*\left(\frac{metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 212\frac{metric\ tons\ CO2e}{year}$$

$$GHG\ EF_{hydrogen} = \left(\frac{88.33\ g\ CO2e}{MJ}\right) * \left(\frac{119.99\ MJ}{kg}\right) * \left(\frac{40,700\ kg}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 431\frac{metric\ tons\ CO2e}{year}$$

$$GHG\ EF_{ATV} = \left(212\frac{metric\ tons\ CO2e}{year}\right) + \left(431\frac{metric\ tons\ CO2e}{year}\right)$$

$$= 643\frac{metric\ tons\ CO2e}{year}$$

Step 4: Determine the GHG emission reductions that are associated with the proposed project. Use Formula 4, populated by results from Step 2 and Step 3 above, to give the GHG emission benefit from the proposed project.

Formula 4:

$$Project\ GHG\ ER_{annual}\left(\frac{metric\ tons\ CO2e}{year}\right) = GHG\ EF_{base} - GHG\ EF_{ATV}$$

Where:

- GHG ER_{annual} is the annual GHG emission reductions that are associated with the proposed project;
- GHG EF_{base} is the GHG emission factor associated with the base case vehicle or equipment that the advanced technology vehicle or equipment is compared against; and
- GHG ERATV is the GHG emission factor that is associated with the proposed advanced technology vehicle.

$$Project\ GHG\ ER_{annual} = \left(1,893 \frac{metric\ tons\ CO2e}{year}\right) - \left(643 \frac{metric\ tons\ CO2e}{year}\right)$$
$$= 1,250 \frac{metric\ tons\ CO2e}{year}$$

Step 5: Determine the annual criteria pollutant emission reductions that are associated with the proposed project. The baseline locomotive is using a 1,500 hp diesel engine that is certified to the Tier 4 emissions standard, therefore, using emission values from Table IV-12b and fuel consumption rate factors from Table IV-19, the result of Step 1 above to populate Formula 13. The locomotive will be used 100% of the time in California. There are no criteria pollutant emissions associated with the use of the battery-electric locomotive with the fuel cell range extender in a tank-to-wheel analysis.

For a Tier 4 locomotive engine at 1,500 hp, Table IV-12b gives criteria pollutant emissions per bhp-hr and Table IV-19 gives the fuel consumption rate factor. Therefore:

NOx = 1.22
$$\frac{g \ NOx}{bhp-hr}$$
; ROG = 0.15 $\frac{g \ ROG}{bhp-hr}$; PM10 = 0.026 $\frac{g \ PM10}{bhp-hr}$

Formula 13:

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

$$Annual\ ER_{NOx} = \left(1.22 \frac{g\ NOx}{bhp-hr}\right) * \left(15.2 \frac{bhp-hr}{gal\ diesel}\right) * \left(138,000 \frac{gal\ diesel}{year}\right) * (1) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 2.821 \frac{tons\ NOx}{year}$$

$$Annual\ ER_{ROG} = \left(0.15 \frac{g\ ROG}{bhp-hr}\right) * \left(15.2 \frac{bhp-hr}{gal\ diesel}\right) * \left(138,000 \frac{gal\ diesel}{year}\right) * (1) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 0.347 \frac{tons\ ROG}{year}$$

$$Annual\ ER_{PM10} = \left(0.026 \frac{g\ PM10}{bhp-hr}\right) * \left(15.2 \frac{bhp-hr}{gal\ diesel}\right) * \left(138,000 \frac{gal\ diesel}{year}\right) * (1) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 0.060 \frac{tons\ PM10}{year}$$

Step 6: Determine the weighted annual surplus emission reductions that are associated with the proposed project. Use the results from Step 5 above, along with the realization that the proposed battery-electric locomotive with a fuel cell range extender will not produce any criteria pollutant emissions in a tank-to-wheel scenario, to populate Formula 11.

Formula 11:

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

$$WER = \left(2.821 \frac{tons\ NOx}{year}\right) + \left(0.347 \frac{tons\ ROG}{year}\right) + \left(20 * 0.060 \frac{tons\ PM}{year}\right)$$
$$= 4.368 \frac{tons}{year}$$

Step 7: Determine the incremental cost of the proposed technology using Formula 10 and the equipment costs for the baseline locomotive and the battery-electric locomotive with a fuel cell range extender given at the start of this example. Cost-effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Baseline Equipment:

Locomotive cost at Project : \$1,500,000

Locomotive cost two years after project: \$1,500,000

Advanced Technology:

Locomotive cost at project: \$3,500,000

Locomotive cost two years after project: \$2,500,000

Formula 10:

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

Incremental Cost_{2 years} = \$3,500,000 - \$1,500,000 = \$2,000,000

Incremental Cost_{10 years} = \$2,500,000 - \$1,500,000 = \$1,000,000

Step 8: Determine the GHG emission reduction cost-effectiveness for the proposed project using Formula 5 and the results from Step 4 and Step 7.

Formula 5:

$$Cost\ Effectiveness\ \left(\frac{\$}{metric\ ton\ CO2e}\right) = \frac{CRF\ *\ incremental\ cost}{Project\ GHG\ ER_{annual}}$$

Where, for the purposes of this Solicitation:

- CRF is the Capital Recovery Factor;
- CRF₂ = 0.508, per Moyer Table D-25 (2-year life);
- CRF₁₀ = 0.106, per Moyer Table D-25 (10-year life); and
- Incremental cost is the difference between the cost of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

$$GHG\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$2,000,000)}{\left(1,250\frac{metric\ tons\ CO2e}{year}\right)}$$

= \$813 per metric ton CO2e reduced

$$GHG\ Cost\ Effectiveness_{10\ years} = \frac{(0.106*\$1,000,000)}{\left(1,250\ \frac{metric\ tons\ CO2e}{year}\right)}$$

= \$85 per metric ton CO2e reduced

Step 9: Determine the criteria pollutant cost-effectiveness for the proposed technology. Use the results from Step 6 and Step 7 to populate Formula 8.

Formula 8:

WER Cost Effectiveness_{2 years} =
$$\frac{(0.508 * $2,000,000)}{\left(4.368 \frac{tons WER}{year}\right)}$$

= \$233,000 per ton weighted criteria pollutants reduced

WER Cost Effectiveness_{10 years} =
$$\frac{(0.106 * \$1,000,000)}{\left(4.368 \frac{tons WER}{year}\right)}$$

= \$24,300 per ton weighted criteria pollutants reduced

D. Example D: Logistic Strategy for Container Movement Technology

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a piece of cargo handling equipment utilizing advanced logistic technology will have the same energy requirements as a diesel counterpart without the logistic technology and will be used the same number of hours. The logistic strategy is only functional while loading and unloading ocean going vessels and, therefore, will only be engaged half of the time during the cargo handling equipment's operation.

Baseline Vehicle:

- Top handler with off-road diesel engine: Tier 4 final certification, 300 hp
- Diesel usage: 7.5 gallons per hour
- Operation: 2,500 hours per year, 18,750 gallons of diesel consumed per year
- Top handler cost at project : \$550,000
- Top handler cost two years after project: \$550,000

Advanced Technology:

- Top handler with off-road diesel engine: Tier 4 final certification, 300 hp
- Operation: 2,500 hours per year
 - o 50% of operation is loading and unloading ocean going vessels
- Logistic system provides a 5% increase in fuel economy while loading and unloading ocean going vessels
- Top handler with logistic technology cost at project : \$590,000
- Top handler with logistic technology two years after project: \$575,000

Variables Used in Calculation:

Carbon Intensity

From Table II-2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$Cl_{diesel} = \frac{102.01 g CO2e}{MJ}$$
 Table Pathway Identifier ULSD001

Energy Density

From Table II-1: Fuel Energy Density

ED = Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel}$$

Energy Efficiency Ratio

From Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

EER = Energy Efficiency Ratio (unit less)

Step 1: Calculate the amount of diesel needed to operate the advanced technology vehicle. Use Formula 7 and the baseline information above.

Formula 7:

$$Fuel\ Usage_{ATV}\left(\frac{gal}{year}\right) =\ fuel\ usage *\left(1 - \frac{(X*Y\%\ improvement)}{100\%}\right)$$

Where:

- X is the fraction of the time the advanced operational efficiency technology or logistic strategy is enabled and providing emission reductions. If the advanced operational efficiency technology or logistic strategy is always engaged and providing emission reductions assume that X is equal to 1; and
- Y is the percentage fuel economy improvement that is gained by having the advanced operational efficiency technology or logistic strategy efficiency improvement over the baseline engine.

$$\begin{aligned} &Fuel\ Usage_{ATV}\left(\frac{gal}{year}\right) = \left(\frac{18,750\ gal\ diesel}{year}\right)*\left(1 - \frac{(0.5*5\%\ improvement)}{100\%}\right) \\ &= 18,280\frac{gal\ diesel}{year} \end{aligned}$$

Step 2: Determine the GHG emissions that are attributed to the baseline vehicle using Formula 1 and the variables identified above.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right)*\left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\ or\ \frac{MJ}{kWh}\right)$$

$$*\left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\ or\ \frac{kWh}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{base} = \left(\frac{102.01\ g\ CO2e}{MJ}\right)*\left(\frac{134.47\ MJ}{gal\ diesel}\right)*\left(\frac{18,750\ gal\ diesel}{year}\right)*\left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 257\frac{metric\ tons\ CO2e}{year}$$

Step 3: Determine the GHG emissions that are attributed to the advanced technology vehicle using Formula 1, the result from Step 1 and the variables identified above.

Formula 1:

$$\begin{aligned} \textit{GHG EF}\left(\frac{\textit{metric tons CO2e}}{\textit{year}}\right) &= \textit{CI} * \textit{fuel energy density} * \textit{fuel usage} * \frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}} \\ &= \left(\frac{\textit{gram CO2e}}{\textit{MJ}}\right) * \left(\frac{\textit{MJ}}{\textit{gal}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kg}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{scf}} \, \textit{or} \, \frac{\textit{MJ}}{\textit{kWh}}\right) \\ &\quad * \left(\frac{\textit{gal}}{\textit{year}} \, \textit{or} \, \frac{\textit{kg}}{\textit{year}} \, \textit{or} \, \frac{\textit{scf}}{\textit{year}} \, \textit{or} \, \frac{\textit{kWh}}{\textit{year}}\right) * \left(\frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}}\right) \\ &\quad \textit{GHG EF}_{\textit{ATV}} = \left(\frac{102.01 \, \textit{g CO2e}}{\textit{MJ}}\right) * \left(\frac{134.47 \, \textit{MJ}}{\textit{gal diesel}}\right) * \left(\frac{18,280 \, \textit{gal diesel}}{\textit{year}}\right) * \left(\frac{1 \, \textit{metric ton CO2e}}{1,000,000 \, \textit{grams}}\right) \end{aligned}$$

$$GHG\ EF_{ATV} = \left(\frac{102.01\ g\ CO2e}{MJ}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \left(\frac{18,280\ gat\ ateset}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$= 251 \frac{metric\ tons\ CO2e}{year}$$

Step 4: Determine the GHG emission reductions that are associated with the proposed project. Use Formula 4, populated by results from Step 3 and Step 4 above, to give the GHG emission benefit from the proposed project.

Formula 4:

$$Project\ GHG\ ER_{annual}\left(\frac{metric\ tons\ CO2e}{year}\right) = GHG\ EF_{base} - GHG\ EF_{ATV}$$

Where:

- GHG ER_{annual} is the annual GHG emission reductions that are associated with the proposed project;
- GHG EF_{base} is the GHG emission factor associated with the base case vehicle or equipment that the advanced technology vehicle or equipment is compared against; and
- GHG ERATV is the GHG emission factor that is associated with the proposed advanced technology vehicle.

$$Project\ GHG\ ER_{annual} = \left(257 \frac{metric\ tons\ CO2e}{year}\right) - \left(251 \frac{metric\ tons\ CO2e}{year}\right)$$

$$= 6 \frac{metric\ tons\ CO2e}{year}$$

Step 5: Determine the annual criteria pollutant emissions that are associated with the baseline vehicle. The baseline vehicle is using a 300 hp diesel engine that is certified to the Tier 4 Final emissions standard, therefore, using emission values from Table IV-7 and fuel consumption rate factors from Table IV-19, populate Formula 13. The vehicle will be used 100% of the time in California.

For a Tier 4 Final off-road engine at 300 hp, Table IV-7 gives criteria pollutant emissions per bhp-hr and Table-24 gives the fuel consumption rate factors. Therefore:

NOx =
$$0.26 \frac{g \, NOx}{bhv-hr}$$
; ROG = $0.05 \frac{g \, ROG}{bhv-hr}$; PM10 = $0.009 \frac{g \, PM10}{bhv-hr}$

Formula 13:

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

$$Annual\ ER_{NOx} = \left(0.26 \frac{g\ NOx}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal\ diesel}\right) * \left(18,750 \frac{gal\ diesel}{year}\right) * \left(1\right) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 0.099 \frac{tons\ NOx}{year}$$

$$Annual\ ER_{ROG} = \left(0.05 \frac{g\ ROG}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal\ diesel}\right) * \left(18,750 \frac{gal\ diesel}{year}\right) * \left(1\right) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 0.019 \frac{tons\ ROG}{year}$$

$$Annual\ ER_{PM10} = \left(0.009 \frac{g\ PM10}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal\ diesel}\right) * \left(18,750 \frac{gal\ diesel}{year}\right) * \left(1\right) * \left(\frac{1\ ton}{907,200\ grams}\right)$$

$$= 0.003 \frac{tons\ PM10}{year}$$

Step 6: Determine the annual criteria pollutant emissions that are associated with the advanced technology vehicle. The vehicle is using a 300 hp diesel engine that is certified to the Tier 4 Final emissions standard, therefore, using emission values from Table IV-7, fuel consumption rate factors from Table IV-19, and the result of Step 2 above to populate Formula 13. The vehicle will be used 100% of the time in California.

Formula 13:

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

$$Annual \ ER_{NOx} = \left(0.26 \frac{g \ NOx}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal}\right) * \left(18,280 \frac{gal}{year}\right) * (1) * \left(\frac{1 \ ton}{907,200 \ grams}\right)$$

$$= 0.097 \frac{tons \ NOx}{year}$$

$$Annual \ ER_{ROG} = \left(0.05 \frac{g \ ROG}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal}\right) * \left(18,280 \frac{gal}{year}\right) * (1) * \left(\frac{1 \ ton}{907,200 \ grams}\right)$$

$$= 0.019 \frac{tons \ ROG}{year}$$

$$Annual \ ER_{PM10} = \left(0.009 \frac{g \ PM10}{bhp-hr}\right) * \left(18.5 \frac{bhp-hr}{gal}\right) * \left(18,280 \frac{gal}{year}\right) * (1) * \left(\frac{1 \ ton}{907,200 \ grams}\right)$$

$$= 0.003 \frac{tons \ PM10}{year}$$

Step 7: Determine the weighted annual emissions reductions that are associated with the proposed project. Using the results from Step 5 and Step 6 above, populate Formula 11.

Formula 11:

Annual Weighted Surplus Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

$$\begin{aligned} WER &= \left(0.099 - 0.097 \frac{tons\ NOx}{year}\right) + \left(0.019 - 0.019 \frac{tons\ ROG}{year}\right) + \left(20*\left(0.003 - 0.003\right) \frac{tons\ PM}{year}\right) \\ &= 0.002\ \frac{tons}{year} \end{aligned}$$

Step 8: Determine the incremental cost of the proposed technology using Formula 10 and the equipment costs for the baseline and advanced technology vehicle given at the start of this example. Cost-effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Baseline Equipment:

- Top handler cost at project : \$550,000
- Top handler cost two years after project: \$550,000

Advanced Technology:

- Top handler with logistic technology cost at project: \$590,000
- Top handler with logistic technology two years after project: \$575,000

Formula 10:

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Technology (\$)

Incremental Cost_{2 years} = \$590,000 - \$550,000 = \$40,000

Incremental Cost_{10 years} = \$575,000 - \$550,000 = \$25,000

Step 9: Determine the GHG emission reduction cost-effectiveness for the proposed project using Formula 5 and the results from Step 4 and Step 8.

Formula 5:

$$Cost\ Effectiveness\ \left(\frac{\$}{metric\ ton\ CO2e}\right) = \frac{CRF\ *\ incremental\ cost}{Project\ GHG\ ER_{annual}}$$

Where, for the purposes of this Solicitation:

- CRF is the Capital Recovery Factor;
- CRF₂ = 0.508, per Moyer Table D-25 (2-year life);
- CRF₁₀ = 0.106, per Moyer Table D-25 (10-year life); and
- Incremental cost is the difference between the cost of the baseline vehicle or equipment and the advanced technology vehicle or equipment.

$$GHG\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$40,000)}{\left(6\frac{metric\ tons\ CO2e}{year}\right)}$$

= \$3,390 per metric ton CO2e reduced

$$GHG\ Cost\ Effectiveness_{10\ years} = \frac{(0.106*\$25,000)}{\left(6\frac{metric\ tons\ CO2e}{year}\right)}$$

= \$442 per metric ton CO2e reduced

Step 10: Determine the criteria pollutant cost-effectiveness for the proposed technology. Use the results from Step 7 and Step 8 to populate Formula 8.

Formula 8:

$$WER\ Cost\ Effectiveness_{2\ years} = \frac{(0.508*\$40,000)}{\left(0.002\ \frac{tons\ WER}{year}\right)}$$

= \$10,200,000 per ton weighted criteria pollutants reduced

WER Cost Effectiveness_{10 years} =
$$\frac{(0.106 * $25,000)}{\left(0.002 \frac{tons WER}{year}\right)}$$

E. Example E: Fuel Cell Regional Haul Truck

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a fuel cell on-road regional haul truck will have the same energy requirements as a diesel counterpart and will be used the same number of miles. The proposed truck in this example will not be plugged in to the electrical grid to charge on-board battery packs, but will use the on-board fuel cell. Further, it is assumed that this project will use hydrogen that is produced from natural gas and compressed for use in the project.

Baseline vehicle:

 2017 diesel fueled regional haul truck with a heavy duty 2017 on-road diesel engine

- Usage 5 miles per gallon, 175 miles per day, 210 days per year
- On-road truck cost at project: \$100,000
- On-road truck cost two years after project : \$100,000

Advanced Technology:

- Hydrogen fuel cell on-road truck
- Hydrogen fuel cell on-road truck cost at project: \$750,000
- Hydrogen fuel cell on-road truck cost two years after project: \$500,000

Variables Used in Calculation:

Carbon Intensity

From Table ORATD App D2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$Cl_{diesel} = \frac{102.01 g CO2e}{MI}$$
 Table Pathway Identifier ULSD001

$$CI_{hydrogen} = \frac{88.33 g CO2e}{MJ}$$
 Pathway Identifier HYGN005

Energy Density

From Table ORATD App D1: Fuel Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel} \qquad \qquad \mathsf{ED}_{\mathsf{hydrogen}} = \frac{119.99 \, MJ}{kg \, H2}$$

Energy Efficiency Ratio

From Table ORATD App D3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

Step 1: Calculate the baseline vehicle's annual fuel usage using Formula 1a:

Formula 1a:

$$Fuel\ Usage_{baseline} = \left(\frac{gallon}{mile}\right) * \left(\frac{miles}{day}\right) * \left(\frac{days}{year}\right)$$

$$Fuel\ Usage_{baseline} = \left(\frac{1\ gallon}{5\ miles}\right) * \left(\frac{175\ miles}{day}\right) * \left(\frac{210\ days}{year}\right) = \frac{7,350\ gallons\ diesel}{year}$$

Step 2: Convert the diesel used per year from the baseline vehicle to the amount of hydrogen needed to do the same work. Using Formula 3 and the variable identified above.

Formula 3:

$$Fuel\ Usage_{ATV} = \left(\frac{X\ gal\ Diesel}{vr}\right) * \left(ED\ \frac{MJ}{1\ gal\ diesel}\right) * \left(ED\ \frac{NF\ unit}{MJ}\right) * \left(\frac{1}{EER}\right)$$

Where:

- X is the number of gallons diesel fuel used as a basis for the conversion;
- ED is the Energy Density of the replacement fuel (see Table ORATD App D1: Fuel Energy Density);
- **EER** is the Energy Economy Ratio value for fuels relative to diesel fuel (see Table ORATD App D3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications);
- NF is the new fuel that is proposed to be used as a diesel replacement; and
- Unit is the units associated with the replacement fuel:

Electricity: kWhHydrogen: kg

o CNG: scf

$$Fuel\ Usage_{ATV} = \left(\frac{7,350\ gal\ Diesel}{yr}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \left(\frac{1\ kg\ H2}{119.99\ MJ}\right) * \left(\frac{1}{1.9}\right) = 4,335\frac{kg\ H2}{year}$$

Step 3: Determine the GHG emissions that are attributed to the baseline on-road truck. Using Formula 1 and the variables identified above.

Formula 1:

GHG EF = CI * fuel energy density * fuel usage *
$$\frac{1 \text{ metric ton CO2e}}{1,000,000 \text{ grams}}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right) * \left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\right) * \left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$GHG\ EF_{baseline} = \left(\frac{102.01\ g\ CO2e}{MJ}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \\ \left(\frac{7,350\ gallons\ diesel}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$=101\frac{metric\ tons\ CO2e}{year}$$

Step 4: Determine the GHG emissions (GHG EF_{ATV})that are attributed to the advanced technology fuel cell on-road truck. Using the result from Step 2, the variables identified above as inputs into Formula 1.

Formula 1:

$$GHG\ EF = CI * fuel\ energy\ density * fuel\ usage * \frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$= \left(\frac{gram\ CO2e}{MJ}\right) * \left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\right) * \left(\frac{gal}{year}\ or\ \frac{kg}{year}\ or\ \frac{scf}{year}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$\begin{aligned} GHG \ EF_{ATV} &= \left(\frac{88.33 \ g \ CO2e}{MJ}\right) * \left(\frac{120.00 \ MJ}{kg \ H2}\right) * \left(\frac{4,335 \ kg \ H2}{year}\right) * \left(\frac{1 \ metric \ ton \ CO2e}{1,000,000 \ grams}\right) \\ &= 46 \frac{metric \ tons \ CO2e}{year} \end{aligned}$$

Step 5: Determine the annual GHG emission reductions that are associated with the proposed project. Using Formula 4 above populated by results from Step 3 and Step 4 from the above example to give the annual GHG emission benefit from the proposed project.

Formula 4:

$$Project\ GHG\ ER_{annual} = \left(101 \frac{metric\ tons\ CO2e}{year}\right) - \left(46 \frac{metric\ tons\ CO2e}{year}\right)$$
$$= 55 \frac{metric\ tons\ CO2e}{year}$$

Step 6: Determine the annual criteria and toxic pollutant emission reductions that are associated with the proposed project. Since the baseline vehicle is using an on-road engine certified to the 2010 standard, inputs from Table D-1 and the result of Step1 above will be used to populate Formula C-9. Since there are not any criteria or toxic air contaminant pollutant emissions associated with the use of the advanced technology on-road truck, all the emissions associated with the baseline vehicle are considered to be the criteria and toxic air contaminant emission reductions for the proposed project.

For a 2010 on-road engine with EO Certification Standard of 0.20 g NOx/bhp-hr, Table D-1 gives emissions per gallon of diesel consumed. Therefore:

NOx = 3.44
$$\frac{g \ NOx}{gal \ diesel}$$
; ROG =0.18 $\frac{g \ ROG}{gal \ diesel}$; PM10 = 0.148 $\frac{g \ PM \ 10}{gal}$

Using Formula C-9:

Formula C-9: Estimated Annual Emissions based on Fuel using Emission Factors (tons/yr). All the emission reductions are taking place in CA.

Annual Emission Reductions =

Emission Factor (g/gal) * Activity (gal/yr) * ton/907,200g

Annual ER is the calculated annual emission reductions

Annual ER_{NOX} =
$$\left(\frac{3.44 \text{ g Nox}}{\text{gal diesel}}\right) * \left(\frac{7350 \text{ gal diesel}}{\text{year}}\right) * \left(\frac{1 \text{ ton}}{907,200 \text{ g}}\right) = 0.0279 \frac{\text{tons Nox}}{\text{year}}$$

Annual ER_{ROG} = $\left(\frac{0.18 \text{ g ROG}}{\text{gal diesel}}\right) * \left(\frac{7350 \text{ gal diesel}}{\text{year}}\right) * \left(\frac{1 \text{ ton}}{907,200 \text{ g}}\right) = 0.00146 \frac{\text{tons ROG}}{\text{year}}$

Annual ER_{PM10} = $\left(\frac{0.148 \text{ g Nox}}{\text{gal diesel}}\right) * \left(\frac{7350 \text{ gal diesel}}{\text{year}}\right) * \left(\frac{1 \text{ ton}}{907,200 \text{ g}}\right) = 0.00120 \frac{\text{tons PM}}{\text{year}}$

Step 7: Determine the weighted annual surplus emission reductions that are associated with the proposed project. Using the results from Step 6 above along with the realization that the proposed fuel cell on-road truck will not produce any criteria pollutant emissions in a tank-to-wheel scenario populate Formula C-5.

Formula C-5: Annual Weighted Surplus Emission Reductions (tons/yr)

Weighted Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

Therefore using the results from Step 6 above and Formula C-5:

WER is the Weighted Emission Reductions

WER =
$$(0.0279 \frac{tons\ NOx}{year}) + \left(0.00146 \frac{tons\ ROG}{year}\right) * 20 \left(0.00120 \frac{tons\ NOx}{year}\right) = 0.0534\ tons$$

Therefore, WER = $0.053 \frac{tons\ criteria\ pollutants\ reduced}{year}$

Step 8: Determine the Incremental cost of the proposed technology using Formula C-3 and the vehicle costs for the baseline vehicle and the fuel cell on-road truck given at the start of this example. Cost effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Baseline vehicle:

- On-Road truck cost at Project : \$100,000
- On-Road truck cost two years after project : \$100,000

Advanced Technology:

- Fuel cell on-road truck cost at project : \$750,000
- Fuel cell on-road truck cost two years after project: \$500,000

Formula C-3: Incremental Cost (\$)

Incremental Cost = Cost of New Technology (\$) – Cost of Baseline Diesel Technology (\$)

Incremental Cost_{2 years} = \$750,000 - \$100,000 = \$650,000Incremental Cost_{10 years} = \$500,000 - \$100,000 = \$400,000

Step 9: Determine the GHG emission reduction cost effectiveness for the proposed project using the results from Step 5, Step 8 and Formula 5

Formula 5:

$$Cost\ Effectiveness\ (\frac{\$}{metric\ ton}) = \left(\frac{\frac{\textit{CRF*(\$Advanced\ Technology\ Vehicle-\$Baseline\ Diesel\ Vehicle)}}{\frac{\textit{year}}{\textit{vear}}}\right)$$

Where, for the purposes of this solicitation:

- CRF is the Capital Recovery Factor:
 - o CRF₂ = 0.515 per Moyer Table G-3a (2-year life); and
 - \circ CRF₁₀ = 0.111 per Moyer Table G-3a (10-year life).

Therefore:

GHG C/E is the GHG Cost Effectiveness

GHG C/E 2 years =
$$(\frac{\frac{(0.508*\$650,000)}{year}}{\frac{55 \ metric \ tons \ CO2e}{year}}) = \frac{\$6004}{metric \ tons \ CO2e \ reduced}$$

GHG C/E 10 years = $(\frac{\frac{(0.106*\$400,000)}{year}}{\frac{55 \ metric \ tons \ CO2e}{year}}) = \frac{\$771}{metric \ tons \ CO2e \ reduced}$

Step 10: Determine the criteria pollutant cost effectiveness for the proposed technology. Use the results from Step 7 and Step 8 to populate Formula C-1.

Formula C-1: Cost-Effectiveness of Weighted Surplus Emission Reductions (\$/ton)

Cost-Effectiveness (\$/ton) = Annualized Cost (\$/year(yr))

Annual Weighted Surplus Emission Reductions (tons/yr)

Criteria Pollutant C/E_{2 years} =
$$(\frac{\frac{(0.508*\$650,000)}{year}}{\frac{0.053 \ tons \ WER}{year}}) = \frac{\$6.2 \ million}{tons \ criteria \ pollutants \ reduced}$$
Criteria Pollutant C/E_{10 years} = $(\frac{\frac{(0.106*\$400,000)}{year}}{\frac{0.053 \ tons \ WER}{year}}) = \frac{\$800,000}{tons \ criteria \ pollutants \ reduced}$

F. Example F: Fuel Cell Transportation Refrigeration Unit (TRU)

Potential GHG emission reductions are determined on a well-to-wheel basis, while criteria pollutant emission reductions are determined using a tank-to-wheel analysis. This example assumes that a TRU will have the same energy requirements as a diesel counterpart and will be used the same number of hours. The initial chill down of the trailer, TRU operations and any needed standby power are provided by the fuel cell. Further, it is assumed that this project will use hydrogen that is SB 1505 compliant and therefore has a 1/3 renewable component.

Baseline TRU:

- Off-Road diesel engine: Tier-4 final certification, 24 hp
- Diesel usage: 0.8 gal per hour, 40 hours per week, 1664 gal per year
- TRU cost at project: \$26,000
- TRU cost two years after project : \$26,000

Advanced Technology:

- Hydrogen fuel cell TRU
- TRU cost during project: \$45,000
- TRU cost two years after project: \$40,000

Variables Used in Calculation:

Carbon Intensity

From Table MSF App D2: Fuel Carbon Intensity Values

CI = Carbon Intensity

$$Cl_{diesel} = \frac{102.01 g CO2e}{MJ}$$
 Table Pathway Identifier ULSD001

From Table II-2: Fuel Carbon Intensity Values

$$CI_{hydrogen} = \frac{88.33 g CO2e}{MJ}$$
 Pathway Identifier HYGN005

Energy Density

From Table II-1: Fuel Energy Density

ED = Energy Density

$$\mathsf{ED}_{\mathsf{diesel}} = \frac{134.47 \, MJ}{gal \, diesel} \qquad \qquad \mathsf{ED}_{\mathsf{hydrogen}} = \frac{119.99 \, MJ}{kg \, H2}$$

Energy Efficiency Ratio

From Table II-3: EER Values for Fuels Used in Light- Medium- and Heavy-Duty Applications

EER = Energy Efficiency Ratio (unit less)

EER_{hydrogen} = 1.9

Step 1: Convert the diesel used per year to the amount of hydrogen needed to do the same work. Using Formula 3 and the variable identified above.

Formula 3:

$$= \left(\frac{X \ gal \ Diesel}{vr}\right) \left(ED \ \frac{MJ}{1 \ gal \ diesel}\right) * \left(ED \ \frac{NF \ unit}{MI}\right) * \left(\frac{1}{EER}\right)$$

Where:

X is the number of gallons diesel fuel used as a basis for the conversion;

NF is the new fuel that is proposed to be used as a diesel replacement;

ED is the Energy Density of the replacement fuel see Table MSF App D1: Fuel Energy Density; and

Unit is the units associated with the replacement fuel:

Electricity: kWh Hydrogen: kg CNG: scf

$$\frac{kg\ H2}{year} = \left(\frac{1664\ gal\ diesel}{year}\right) * \left(\frac{134.47\ MJ}{gal\ diesel}\right) * \left(\frac{1\ kg\ H2}{119.99\ MJ}\right) * \left(\frac{1}{1.9}\right) = 981\ \frac{kg\ H2}{year}$$

Step 2: Determine the GHG emissions that are attributed to the base case diesel fueled TRU. Using Formula 1 and the variables identified above.

Formula 1:

$$GHG\ EF = carbon\ intensity * \frac{fuel\ energy\ density}{efficiency} * \frac{1\ metric\ ton\ CO2e}{1,000,000\ grams} = \left(\frac{gram\ CO2e}{MJ}\right) * \left(\frac{MJ}{gal}\ or\ \frac{MJ}{kg}\ or\ \frac{MJ}{scf}\right) * \left(\frac{gal}{day}\ or\ \frac{kg}{day}\ or\ \frac{scf}{day}\right) * \left(\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}\right)$$

$$\mathsf{GHG}\;\mathsf{EF}_{\mathsf{base}} = \left(\frac{102.01\,g\,CO2e}{MJ}\right) * \left(\frac{134.47\,MJ}{gal\,\,diesel}\right) * \left(\frac{1664\,gal}{year}\right) * \left(\frac{1\,metric\,ton\,CO2e}{1,000,000\,grams}\right) = 23\,\frac{metric\,tonc\,CO2e}{year}$$

Step 3: Determine the GHG emissions that are attributed to the advanced technology TRU. Using Formula 1, the result from Step 1 and the variables identified above.

GHG EF_{adv tech} =
$$\left(\frac{88.33 \ g \ CO2e}{MJ}\right) * \left(\frac{119.99 \ MJ}{kg \ H2}\right) * \left(\frac{981 \ kg \ H2}{year}\right) * \left(\frac{1 \ metric \ ton}{1,000,000 \ grams}\right) = 10 \frac{metric \ tons \ CO2e}{year}$$

Step 4: Determine the GHG emission reductions that are associated with the proposed project. Using Formula 4, populated by results from Step 2 and Step 3 to give the GHG emission benefit from the proposed project.

Formula 4:

Project GHG ERannual = GHG EFbase - GHG EFadv tech

Project GHG ER annual =
$$\left(\frac{23 \ metric \ tons \ CO2e}{year}\right) - \left(\frac{10 \ metric \ tons \ CO2e}{year}\right) = 13 \ \frac{metric \ tons \ CO2e}{year}$$

Step 5: Determine the annual criteria pollutant emission reductions that are associated with the proposed project. The base case TRU is using a 24 hp, diesel engine that is certified to the Tier-4 final emissions standard, therefore, using emission values from Table D-12 and fuel consumption rate factors from Table D-24, the result of Step1 above to populate Formula C-8. The fuel cell TRU will be used 100% of the time in California. There are no criteria pollutant emissions associated with the use of the fuel cell TRU in a tank to wheel analysis.

For a Tier-4 final off-road engine at 24 hp, Table D-12 gives criteria pollutant emissions per bhp-hr, but only for diesel engines above 25 hp, for this calculation use the emission factor for a 25 hp diesel engine. The conversion factor from Table D-24, for the relevant engine power rating, allows for the conversion from gram per bhp-hr to gram per gallon of fuel consumed. Therefore:

NOx = 2.75
$$\frac{g \ NOx}{b/p-/rr}$$
; ROG = 0.09 $\frac{g \ ROG}{b/p-/rr}$; PM10 = 0.009 $\frac{g \ PM \ 10}{b/p-/rr}$

Formula C-8: Estimated Annual Emissions based on Fuel Consumed using Emission Factors or Converted Emission Standard (tons/yr)

Annual Emission Reductions =

Emission Factor or Converted Emission Standard (g/bhp-hr) * fuel consumption rate factor (bhp-hr/gallon (gal)) * Activity (gal/yr) * Percent Operation in CA * ton/907,200g

Annual ER is the annual emission reductions for a particular pollutant.

Annual ER_{NOX} =
$$\left(\frac{2.75g\,NOx}{b\,hp-hr}\right) * \left(\frac{18.5\,b\,hp-hr}{gal\,diesel}\right) * \left(\frac{1664\,gal\,diesel}{year}\right) * \left(1\right) * \left(\frac{1\,ton}{907,200\,g}\right) =$$

Annual ER_{NOX} = $0.093\,\frac{tons\,NOx}{year}$

Annual ER_{ROG} = $\left(\frac{0.09\,g\,ROG}{b\,hp-hr}\right) * \left(\frac{18.5\,b\,hp-hr}{gal\,diesel}\right) * \left(\frac{1664\,gal\,diesel}{year}\right) * \left(1\right) * \left(\frac{1\,ton}{907,200\,g}\right) =$

Annual ER_{ROG} = $0.0031\,\frac{tons\,ROG}{year}$

Annual ER_{PM} = $\left(\frac{0.009\,g\,PM}{b\,hp-hr}\right) * \left(\frac{18.5\,b\,hp-hr}{gal\,diesel}\right) * \left(\frac{1664\,gal\,diesel}{year}\right) * \left(1\right) * \left(\frac{1\,ton}{907,200\,g}\right) =$

Annual ER_{PM} = $0.00031\,\frac{tons\,PM}{year}$

Step 6: Determine the weighted annual surplus emission reductions that are associated with the proposed project. Using the results from Step 5 above along with the realization that the proposed fuel cell TRU will not produce any criteria pollutant emissions in a tank-to-wheel scenario populate Formula C-5.

Formula C-5: Annual Weighted Surplus Emission Reductions (tons/yr)

WER is the Weighted Emission Reductions

Weighted Emission Reductions =

NOx reductions (tons/yr) + ROG reductions (tons/yr) + [20 * (PM reductions (tons/yr)]

Therefore, using the results from Step 6 above and Formula C-5:

WER =
$$(0.093 \frac{tons\ NOx}{year}) + \left(0.0031 \frac{tons\ ROG}{year}\right) * 20 \left(0.00031 \frac{tons\ PM}{year}\right) = 0.10 \frac{tons\ PM}{year}$$
Therefore, WER = $0.10 \frac{tons\ criteria\ pollutants\ reduced}{year}$

Step 7: Determine the incremental cost of the proposed technology using Formula C-3, the equipment costs for the base case TRU and the fuel cell TRU given at the start of this example. Cost effectiveness is to be calculated for two scenarios; for two years during the project and for 10 years, two years after the completion of the project.

Step 8: Determine the GHG emission reduction cost effectiveness for the proposed project using the results from Step 4, Step 7 and Formula 5

Formula 5:

$$Cost\ Effectiveness\ (\frac{\$}{metric\ ton}) = \left(\frac{\frac{\$CRF*(\$Advanced\ Technology\ Vehicle-\$Baseline\ Diesel\ Vehicle}{\frac{year}{(\frac{metric\ ton\ emissions\ reduced}{year})}}\right)$$

For the purposes of this Solicitation:

CRF is the Capital Recover Factor for a specific useful life.

 $CRF_2 = 0.508$ per Moyer Table IV-24 (2-year life)

 $CRF_{10} = 0.106$ per Moyer Table IV-24 (10-year life)

Therefore:

GHG C/E is the GHG Cost Effectiveness

GHG C/E
$$_{2 \text{ years}} = \left(\frac{\underbrace{\frac{(0.508*\$19,000)}{year}}}{\underbrace{\frac{13 \text{ metric tons CO2e}}{year}}}\right) = \frac{\$742}{\text{metric tons CO2e reduced}}$$

GHG C/E 10 years =
$$\left(\frac{\left(\frac{(0.106*\$14,000)}{year}\right)}{\frac{13\ metric\ tons\ CO2e}{year}}\right) = \frac{\$114}{metric\ tons\ CO2e\ reduced}$$

Step 9: Determine the criteria pollutant cost effectiveness for the proposed technology. Use the results from Step 6 and Step 7 to populate Formula C-1.

Formula C-1: Cost-Effectiveness of Weighted Surplus Emission Reductions (\$/ton):

Criteria Pollutant C/E_{2 years} =
$$(\frac{\frac{(0.508*\$19,000)}{year}}{\frac{0.10\ tons\ WER}{year}}) = \frac{\$96,500}{tons\ criteria\ pollutants\ reduced}$$

Criteria Pollutant C/E_{10 years} = $(\frac{\frac{(0.106*\$14,000)}{year}}{\frac{0.10\ tons\ WER}{year}}) = \frac{\$14,800}{tons\ criteria\ pollutants\ reduced}$

G. Example G: Facility Efficiency Improvement

Potential GHG emission reductions are determined on a well-to-wheel basis. This example shows the emission reductions by increasing the efficiency at a freight facility by installing advanced technologies that reduce the electrical needs of a freight facility by 10%. Criteria pollutant emission reductions are determined on tank-to-wheel basis. Since this project is using electrically from the electrical grid there are no criteria pollution emission reductions.

Baseline technology:

- Business as Usual
- Facility uses 190.8 Kw/hr

Advanced Technology:

- 10% efficiency improvement thru the use of advanced strategies
- Advanced strategy cost during the project: \$175,000
- Advanced strategy cost two years after the project: \$150,000

Variables used in Calculation:

Energy Density

From Table II-1 Fuel Energy Density

$$ED_{electricity} = \frac{3.60 \, MJ}{KWh}$$

Carbon Intensity

$$Cl_{\text{electricy}} = \frac{105.15 \ g \ CO2e}{MJ}$$

Step 1: Determine the amount of electric used at the freight facility during one year without the use of advanced technologies reducing electrical load for the facility.

$$Annual\ Electrical\ usage = \frac{190.8\ Kw}{hr} \quad *\frac{8760\ hrs}{year} = \frac{1,671,408\ Kw}{yr}$$

Step 2: Calculate the baseline emissions from the freight facility.

Formula 1:

$$GHG\ EF\left(\frac{metric\ tons\ CO2e}{year}\right) = CI*fuel\ energy\ density*fuel\ usage*\frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$GHG\ EF = \frac{105.15\ g\ CO2e}{MJ} \ * \frac{3.60\ MJ}{KWh} \ * \frac{1,671,408\ Kw}{yr} \ * \frac{1\ metric\ ton\ CO2e}{1,000,000\ grams}$$

$$GHG\ EF = \frac{633\ metric\ tons\ CO2e}{Year}$$

Since the advanced technology, being deployed at the freight facility will reduce electrical load by 10% that gives a GHG emission reduction of:

Project GHG ER annual =
$$\left(\frac{633 \text{ metric tons CO2e}}{\text{year}}\right) * 10\% = 63 \frac{\text{metric tons CO2e}}{\text{year}}$$

For the purposes of this Solicitation:

CRF is the Capital Recover Factor for a specific useful life.

 $CRF_2 = 0.508$ per Moyer Table IV-24 (2-year life)

 $CRF_{10} = 0.106$ per Moyer Table IV-24 (10-year life)

Therefore:

GHG C/E is the GHG Cost Effectiveness

$$\text{GHG C/E 2 years} = \left(\frac{\underbrace{\frac{(0.508*\$175,000)}{year}}}{\underbrace{\frac{633 \ metric \ tons \ CO2e}{year}}} \right) = \frac{\$140}{metric \ tons \ CO2e \ reduced}$$

GHG C/E 10 years =
$$\left(\frac{\frac{\left(0.106*\$150,000\right)}{year}}{\frac{633\ metric\ tons\ CO2e}{year}}\right) = \frac{\$25}{metric\ tons\ CO2e\ reduced}$$

H. Example H: Project Wide Summation of Emission Reductions and Cost Effectiveness Determination:

This example shows the summation of the emission reductions and cost effectiveness from an entire project utilizing the example calculations for specific vehicle and equipment types and including reductions from the freight facility efficiency improvement project. The total project will have a one-to-one match and the total project cost is \$18,500,000 with a request for funding of \$9,000,000. The summation calculation will only be required for the time frame of the proposed project and not require a calculation for a period after the end of the project.

A proposed project wants to deploy:

10 Fuel Cell Regional Haul Trucks

Advanced Technology Trucks:

Hydrogen fuel cell on-road truck cost at project : \$750,000

Emission Reductions:

- 55 metric tons CO2e per truck
- o 0.053 tons WER per truck

• 75 Fuel Cell TRUs

Advanced Technology TRUs:

Hydrogen fuel cell TRU cost at project : \$45,000

Emission Reductions:

- 13 metric tons CO2e per TRU
- 0.10 tons WER per TRU

Facility Efficiency Improvement

Advanced Technology Strategy:

- 10% efficiency improvement thru the use of advanced strategies
- Advanced strategy cost during the project: \$175,000

Emission Reductions:

- 633 metric tons CO2e
- o 0.0 tons WER

Determination of the Total Cost of the Project:

Total Cost for Fuel Cell Trucks = 10 trucks * $\frac{\$750,000}{truck}$ = \$7,500,000

Total Cost for TRUs = 75 TRUs * $\frac{$45,000}{TRU}$ = \$3,375,000

Total Cost for Freight Facility Improvement = \$175,000

Fueling Infrastructure = \$7,000,000

Project Administration = \$450,000

Therefore the total project cost is = \$18,500,000

Determination of the total emission reductions from the project:

GHG Emission reduction from trucks =

10 trucks *
$$\frac{55 metric tons CO2e}{truck}$$
 = 550 metric tons CO2e

WER from Trucks =

10 trucks *
$$\frac{0.053 tons WER}{truck}$$
 = 0.53 tons WER

Emission reductions from TRUs =

75 TRUs *
$$\frac{13 metric tons CO2e}{truck}$$
 = 975 metric tons CO2e

WER from Trucks =

10 trucks *
$$\frac{0.10 \text{ tons WER}}{truck}$$
 = 1.0 tons WER

Emission reductions from Facility Efficiency Improvement =

633 metric tons CO2e for Facility Improvement

Therefore, the total emission reductions for the project can be determined:

550 metric tons CO2e from trucks +875 metric tons CO2e from TRUs +

633 metric tons CO2e from facility improvement =

= 2,058 metric tons CO2e for project

0.53 tons WER from trucks + 1.0 tons WER from TRU + 0 tons WER from facility improvement = 1.53 tons WER

:

CRF is the Capital Recover Factor for a specific useful life.

 $CRF_2 = 0.508$ per Moyer Table IV-24 (2-year life)

Therefore:

GHG C/E is the GHG Cost Effectiveness

GHG C/E
$$_{2 \text{ years}} = \left(\frac{\frac{(0.508*\$18,500,000)}{year}}{\frac{2058 \ metric \ tons \ CO2e}{year}}\right) = \frac{\$4570}{metric \ tons \ CO2e \ reduced}$$

Determine the criteria pollutant cost effectiveness for the proposed technology. Use the results from Step 6 and Step 7 to populate Formula C-1.

Formula C-1: Cost-Effectiveness of Weighted Surplus Emission Reductions (\$/ton):

Criteria Pollutant C/E_{2 years} =
$$(\frac{\frac{(0.508*\$118,500,000)}{year}}{\frac{1.53 \ tons \ WER}{year}}) = \frac{\$6,140,000}{tons \ criteria \ pollutants \ reduced}$$

V. EMISSION FACTORS FOR GHG REDUCTIONS

The following emission factors apply when calculating emission reductions and cost-effectiveness for Zero- and Near Zero-Emission Freight Facility Project applications:

Table II-1: Fuel Energy Density⁶

| Table II-1. I del Ellergy Delisity | | | |
|------------------------------------|-----------------|--|--|
| Fuel (units) | Energy Density | | |
| CARBOB (gal) | 119.53 (MJ/gal) | | |
| CaRFG (gal) | 115.83 (MJ/gal) | | |
| Diesel fuel (gal) | 134.47 (MJ/gal) | | |
| CNG (scf) | 1.04 (MJ/scf) | | |
| LNG (gal) | 78.83 (MJ/gal) | | |
| Electricity (KWh) | 3.60 (MJ/KWh) | | |
| Hydrogen (kg) | 119.99 (MJ/kg) | | |
| Denatured Ethanol (gal) | 81.51 (MJ/gal) | | |
| Biodiesel (gal) | 126.13 (MJ/gal) | | |
| Renewable Diesel (gal) | 129.65 (MJ/gal) | | |
| | | | |

⁶ CARB, 2015; LCFS Regulation, Table 3: Energy Densities of LCFS Fuels and Blendstocks. https://www.arb.ca.gov/regact/2015/lcfs2015/lcfsfinalregorder.pdf

Table II-2: Fuel Carbon Intensity Values^{7,8}

| Fuel | Pathway Identifier | Carbon Intensity Values (gCO₂e/MJ) |
|--|-----------------------|--|
| ULSD – based on the average crude oil supplied to California refineries and average California refinery efficiencies | ULSD001 | 102.01 |
| CaRFG (calculated) | | 98.47 |
| Fossil CNG | CNG400T | 78.37 |
| Fossil LNG | LNG401T | 94.42 |
| Biomethane CNG | CNG500T | 46.42 |
| Biomethane LNG | LNG501T | 64.63 |
| Biodiesel – any feedstock | BIOD202T | 102.01 |
| Renewable Diesel – any feedstock | RNWD302T | 102.01 |
| Ethanol – corn | ETH100T | 75.97 |
| Ethanol – any starch or sugar feedstock | ETH103T | 98.47 |
| Hydrogen – all sources | HYGN005 | 88.33 |
| Electricity – California average | ELC001 | 105.16 |
| Electricity – Solar based | | 0 |

⁷ CARB, 2018; CCI Quantification Methodology Emission Factor Database https://www.arb.ca.gov/cc/capandtrade/auctionproceeds/cci_emissionfactordatabase.xlsx accessed [March 20, 2018].

8 CARB, 2015; LCFS Regulation. https://www.arb.ca.gov/regact/2015/lcfs2015/lcfsfinalregorder.pdf

Table II-3: EER Values for Fuels Used in Light-, Medium-, and Heavy-Duty
Applications⁹

| Fuels Used as a Diesel Replacement for Heavy-Duty and Off-Road Applications | | | |
|---|-----|--|--|
| Fuel/Vehicle Combinations EER Value Relative to Diesel | | | |
| Diesel Fuel or Biomass Based Diesel Blends | 1.0 | | |
| CNG | 0.9 | | |
| LNG | 0.9 | | |
| Electricity / Battery Electric or Plug-in Hybrid Electric Vehicle or Equipment | 5.5 | | |
| Electricity / Fixed Guideway, Heavy Rail | 4.6 | | |
| H ₂ / Fuel Cell Vehicle or Equipment | 1.9 | | |

Table II-4: Low NOx Engine Emission Values⁹

| | Low-NOx Engine Incentives Emission Factors | | | | |
|---------------|--|-------------|----------|---------------------------------|--|
| Vehicle Class | (g/mi) | 2017 Diesel | 2017 CNG | 2017 Low NO _x RNG | |
| | GHG (CO ₂ e) | | 1,261 | 557 | |
| | ROG | | 0.0371 | 0.0371 | |
| MHD | NOx | | 0.8579 | 0.0858 | |
| | PM _{2.5} | | 0.0616 | 0.0616 | |
| | Diesel PM | | 0 | 0 | |
| | GHG (CO ₂ e) | 2,223 | 1,821 | 804 | |
| | ROG | 0.0789 | 0.0789 | 0.0789 | |
| HHD | NOx | 1.4310 | 1.4310 | 0.1431 | |
| | PM _{2.5} | 0.0408 | 0.0408 | 0.0408 | |
| | Diesel PM | 0.0055 | 0 | 0 | |

⁹ CARB, 2018; CCI Quantification Methodology Emission Factor Database https://www.arb.ca.gov/cc/capandtrade/auctionproceeds/cci_emissionfactordatabase.xlsx accessed [March 20, 2018].https://www.arb.ca.gov/cc/capandtrade/auctionproceeds/quantification.htm

VI. Tables for Calculating Criteria and Toxic Pollutant Emission Reductions

ON-ROAD TRUCK TABLES

Table IV-1
Diesel Heavy-Duty Engines
Converted Emission Standards for Fuel Based Usage Calculations

| Converted Ennicolon Standards for 1 doi 2 dood Souge Salediations | | | | | |
|---|-----------|--------|--------------------|-------|--|
| EO Certification Standards g/bhp-hr | | NOx | ROG ^(a) | PM10 | |
| | | g/ga | (b)(c)(d) | | |
| 6.0 NOx | 0.60 PM10 | 103.23 | 5.33 | 7.992 | |
| 5.0 NOx | 0.25 PM10 | 86.03 | 4.44 | 3.330 | |
| 5.0 NOx | 0.10 PM10 | 86.03 | 4.44 | 1.332 | |
| 4.0 NOx | 0.10 PM10 | 68.82 | 3.55 | 1.332 | |
| 2.5 NOx + NMHC | 0.10 PM10 | 40.86 | 2.11 | 1.332 | |
| 1.8 NOx + NMHC | 0.01 PM10 | 29.42 | 1.52 | 0.148 | |
| 1.5 NOx + NMHC | 0.01 PM10 | 24.52 | 1.27 | 0.148 | |
| 1.2 NOx + NMHC | 0.01 PM10 | 19.61 | 1.01 | 0.148 | |
| 0.84 NOx + NMHC | 0.01 PM10 | 13.73 | 0.71 | 0.148 | |
| 0.50 NOx | 0.01 PM10 | 8.60 | 0.44 | 0.148 | |
| 0.20 NOX | 0.01 PM10 | 3.44 | 0.18 | 0.148 | |

Table IV-2
Alternative Fuel Heavy-Duty Engines
Converted Emission Standards for Fuel Based Usage Calculations

| Converted Emission Clandards for Faci Based Csage Calculations | | | | |
|--|-----------|--------|--------------------|--------|
| EO Certification Standards g/bhp-hr | | NOx | ROG ^(a) | PM10 |
| | | g/ga | (b)(c)(d) | |
| 6.0 NOx | 0.60 PM10 | 111.00 | 35.14 | 11.100 |
| 5.0 NOx | 0.25 PM10 | 92.50 | 29.29 | 4.625 |
| 5.0 NOx | 0.10 PM10 | 92.50 | 29.29 | 1.850 |
| 4.0 NOx | 0.10 PM10 | 74.00 | 23.43 | 1.850 |
| 2.5 NOx + NMHC | 0.10 PM10 | 37.00 | 11.71 | 1.850 |
| 1.8 NOx + NMHC | 0.01 PM10 | 26.64 | 8.43 | 0.185 |
| 1.5 NOx + NMHC | 0.01 PM10 | 22.20 | 7.03 | 0.185 |
| 1.2 NOx + NMHC | 0.01 PM10 | 17.76 | 5.62 | 0.185 |
| 0.84 NOx + NMHC | 0.01 PM10 | 12.43 | 3.94 | 0.185 |
| 0.50 NOx | 0.01 PM10 | 9.25 | 2.93 | 0.185 |
| 0.20 NOX | 0.01 PM10 | 3.70 | 1.17 | 0.185 |

a - ROG = HC * 1.26639.

b - Fuel based emissions factors were calculated using fuel consumption rate factors from Table IV-19.

c - Fuel based factors are for engines less than 750 horsepower only.

d - Emission standards were converted where appropriate, using the NMHC and NOx fraction default values and the ultra low sulfur diesel fuel correction factors listed in Table D-25 and D-26 of the Moyer Guidelines, respectively.

Table IV-3
Heavy-Duty Vehicles
14,001-33,000 pounds (lbs) Gross Vehicle Weight Rating (GVWR)
Emission Factors for Mileage Based Calculations (g/mile)

| Emission ractors for whicage based calculations (g/mile) | | | |
|--|-------|-----------------------|-------|
| Madel Vee | | Diesel ^(b) | |
| Model Year | NOx | ROG ^(c) | PM10 |
| Pre-1987 | 14.52 | 0.75 | 0.695 |
| 1987-1990 | 14.31 | 0.59 | 0.755 |
| 1991-1993 | 10.70 | 0.26 | 0.409 |
| 1994-1997 | 10.51 | 0.20 | 0.226 |
| 1998-2002 | 10.33 | 0.20 | 0.249 |
| 2003-2006 | 6.84 | 0.13 | 0.157 |
| 2007-2009 | 4.01 | 0.11 | 0.017 |
| 2007+ (0.21-0.50 g/bhp-hr NOx) ^(d) | 1.73 | 0.10 | 0.017 |
| 2010+ (0.20 g/bhp-hr NOx or cleaner) | 0.74 | 0.09 | 0.017 |

Table IV-4 Heavy-Duty Vehicles Over 33,000 lbs GVWR

Emission Factors for Mileage Based Calculations (g/mile)^a

| Model Veer | | Diesel ^(b) | |
|--|-------|-----------------------|-------|
| Model Year | NOx | ROG ^(c) | PM10 |
| Pre-1987 | 21.37 | 1.09 | 1.247 |
| 1987-1990 | 21.07 | 0.86 | 1.355 |
| 1991-1993 | 18.24 | 0.56 | 0.562 |
| 1994-1997 | 17.92 | 0.42 | 0.365 |
| 1998-2002 | 17.61 | 0.43 | 0.403 |
| 2003-2006 | 11.64 | 0.27 | 0.254 |
| 2007-2009 | 6.62 | 0.23 | 0.028 |
| 2007+ (0.21-0.50 g/bhp-hr NOx) ^(d) | 2.88 | 0.20 | 0.028 |
| 2010+ (0.20 g/bhp-hr NOx or cleaner) | 1.27 | 0.19 | 0.028 |

a - EMFAC 2011 Zero-Mile Based Emission Factors.

b - Emission factors reflect the ultra low sulfur diesel fuel correction factors listed in Table D-26 of the Moyer Guidelines.

c - ROG = HC * 1.26639.

d - Use interpolated values assuming 1.2 g/bhp-hr NOx Standards for 2007-2009 Model Year Grouping and 0.2 g/bhp-hr NOx Standards for 2010+ Model Years.

OFF-ROAD PROJECTS AND NON-MOBILE AGRICULTURAL PROJECTS

Table IV-5
Off-Road Diesel Engines Default Load Factors

| Off-Road Diesei Engines Default Load Factors | | | | |
|--|----------------------------|-------------|--|--|
| Category | Equipment Type | Load Factor | | |
| Airport Ground Support | Aircraft Tug | 0.54 | | |
| | Air Conditioner | 0.75 | | |
| | Air Start Unit | 0.90 | | |
| | Baggage Tug | 0.37 | | |
| | Belt Loader | 0.34 | | |
| | Bobtail | 0.37 | | |
| | Cargo Loader | 0.34 | | |
| | Cargo Tractor | 0.36 | | |
| | Forklift | 0.20 | | |
| | Ground Power Unit | 0.75 | | |
| | Lift | 0.34 | | |
| | Passenger Stand | 0.40 | | |
| | Service Truck | 0.20 | | |
| | Other GSE | 0.34 | | |
| Construction | Air Compressors | 0.48 | | |
| | Bore/Drill Rigs | 0.50 | | |
| | Cement & Mortar Mixers | 0.56 | | |
| | Concrete/Industrial Saws | 0.73 | | |
| | Concrete/Trash Pump | 0.74 | | |
| | Cranes | 0.29 | | |
| | Crawler Tractors | 0.43 | | |
| | Crushing/Process Equipment | 0.78 | | |
| | Excavators | 0.38 | | |
| | Graders | 0.41 | | |

Table IV-5 (Continued)

| Off-Road Diesel Engines Default Load Factors Category | Equipment Type | Load Factor |
|---|--------------------------------|-------------|
| Construction | Off-Highway Tractors | 0.44 |
| | Off-Highway Trucks | 0.38 |
| | Pavers | 0.42 |
| | Other Paving | 0.36 |
| | Pressure Washer | 0.30 |
| | Rollers | 0.38 |
| | Rough Terrain Forklifts | 0.40 |
| | Rubber Tired Dozers | 0.40 |
| | Rubber Tired Loaders | 0.36 |
| | Scrapers | 0.48 |
| | Signal Boards | 0.78 |
| | Skid Steer Loaders | 0.37 |
| | Surfacing Equipment | 0.30 |
| | Tractors/Loaders/Backhoes | 0.37 |
| | Trenchers | 0.50 |
| | Welders | 0.45 |
| | Other Construction Equipment | 0.42 |
| Industrial | Aerial Lifts | 0.31 |
| | Forklifts | 0.20 |
| | Sweepers/Scrubbers | 0.46 |
| | Other General Industrial | 0.34 |
| | Other Material Handling | 0.40 |
| Cargo Handling | Container Handling Equipment | 0.59 |
| | Cranes | 0.43 |
| | Excavators | 0.57 |
| | Forklifts | 0.30 |
| | Other Cargo Handling Equipment | 0.51 |
| | Sweeper/Scrubber | 0.68 |
| | Tractors/Loaders/Backhoes | 0.55 |
| | Yard Trucks | 0.65 |
| Other | All | 0.43 |

Table IV-6 Uncontrolled Off-Road Diesel Engines Emission Factors (g/bhp-hr)

| Horsepower | Model Year | NOx | ROG | PM10 |
|------------|-------------|-------|------|-------|
| 25 – 49 | pre-1988 | 6.51 | 2.21 | 0.547 |
| | 1988 + | 6.42 | 2.17 | 0.547 |
| 50 – 119 | pre-1988 | 12.09 | 1.73 | 0.605 |
| | 1988 + | 8.14 | 1.19 | 0.497 |
| 120+ | pre-1970 | 13.02 | 1.59 | 0.554 |
| | 1970 – 1979 | 11.16 | 1.20 | 0.396 |
| | 1980 – 1987 | 10.23 | 1.06 | 0.396 |
| | 1988 + | 7.60 | 0.82 | 0.274 |

Table IV-7 Controlled Off-Road Diesel Engines Emission Factors (g/bhp-hr)^a

| Horsepower | Tier | NOx | ROG | PM10 |
|------------|------------------|------|------|-------|
| 25-49 | 1 | 5.26 | 1.32 | 0.400 |
| 25-49 | · | | | 0.480 |
| | 2 | 4.63 | 0.22 | 0.280 |
| | 4 Interim | 4.55 | 0.09 | 0.128 |
| 50.74 | 4 Final | 2.75 | 0.09 | 0.009 |
| 50-74 | 1 | 6.54 | 0.90 | 0.552 |
| | 2 | 4.75 | 0.17 | 0.192 |
| | 3 ^(b) | 2.74 | 0.09 | 0.192 |
| | 4 Interim | 2.74 | 0.09 | 0.112 |
| | 4 Final | 2.74 | 0.09 | 0.009 |
| 75-99 | 1 | 6.54 | 0.90 | 0.552 |
| | 2 | 4.75 | 0.17 | 0.192 |
| | 3 | 2.74 | 0.09 | 0.112 |
| | 4 Phase-Out | 2.74 | 0.09 | 0.009 |
| | 4 Phase-In/ | 2.14 | 0.08 | 0.009 |
| | Alternate NOx | | | |
| | 4 Final | 0.26 | 0.05 | 0.009 |
| 100-174 | 1 | 6.54 | 0.62 | 0.304 |
| | 2 | 4.17 | 0.15 | 0.128 |
| | 3 | 2.32 | 0.09 | 0.112 |
| | 4 Phase-Out | 2.32 | 0.09 | 0.009 |
| | 4 Phase-In/ | 2.15 | 0.08 | 0.009 |
| | Alternate NOx | | | |
| | 4 Final | 0.26 | 0.05 | 0.009 |
| 175-299 | 1 | 5.93 | 0.38 | 0.120 |
| | 2 | 4.15 | 0.12 | 0.088 |
| | 3 | 2.32 | 0.12 | 0.088 |
| | 4 Phase-Out | 2.32 | 0.12 | 0.009 |
| | 4 Phase-In/ | 1.29 | 0.08 | 0.009 |
| | Alternate NOx | | | |
| | 4 Final | 0.26 | 0.06 | 0.009 |

Table IV-7 (Continued) Controlled Off-Road Diesel Engines Emission Factors (g/bhp-hr)a

| Horsepower | Tier | NOx | ROG | PM10 |
|------------|------------------------------|------|------|-------|
| 300-750 | 1 | 5.93 | 0.29 | 0.120 |
| | 2 | 3.79 | 0.11 | 0.088 |
| | 3 | 2.32 | 0.09 | 0.088 |
| | 4 Phase-Out | 2.32 | 0.09 | 0.009 |
| | 4 Phase-In/ Alternate NOx | 1.29 | 0.06 | 0.009 |
| | 4 Final | 0.26 | 0.05 | 0.009 |
| 751+ | 1 | 5.93 | 0.29 | 0.120 |
| | 2 | 3.79 | 0.09 | 0.088 |
| | 4 Interim | 2.24 | 0.06 | 0.051 |
| | 4 Final | 2.24 | 0.05 | 0.017 |

Note: Engines that are participating in the "Tier 4 Early Introduction Incentive for Engine Manufacturers" program per California Code of Regulations, Title 13, section 2423(b)(6) are eligible for funding provided the engines are certified to the final Tier 4 emission standards. The CARB Executive Order indicates engines certified under this provision. The emission rates for these engines used to determine cost-effectiveness shall be equivalent to the emission factors associated with Tier 3 engines.

For equipment with baseline engines certified under the flexibility provisions per California Code of Regulations, Title 13, section 2423(d), baseline emission rates shall be determined by using the previous applicable emission standard or Tier for that engine model year and horsepower rating. The CARB Executive Order indicates engines certified under this provision.

a - Emission factors were converted using the ultra low sulfur diesel fuel correction factors listed in Table D-27 of the Moyer Guidelines.

b - Alternate compliance option.

LARGE SPARK IGNITION ENGINES (LSI)

Table IV-8
Off-Road LSI Equipment Default Load Factors

| Oπ-Road LSI Equipment Detault Load Factors | | | | | | |
|--|---------------------------|-------------|--|--|--|--|
| Category | Equipment Type | Load Factor | | | | |
| Airport Ground Support | A/C Tug | 0.80 | | | | |
| | Baggage Tug | 0.55 | | | | |
| | Belt Loader | 0.50 | | | | |
| | Bobtail | 0.55 | | | | |
| | Cargo Loader | 0.50 | | | | |
| | Forklift | 0.30 | | | | |
| | Ground Power Unit | 0.75 | | | | |
| | Lift | 0.50 | | | | |
| | Passenger Stand | 0.59 | | | | |
| | Other GSE | 0.50 | | | | |
| Construction | Air Compressors | 0.56 | | | | |
| | Asphalt Pavers | 0.66 | | | | |
| | Bore/Drill Rigs | 0.79 | | | | |
| | Concrete/Industrial Saws | 0.78 | | | | |
| | Concrete/Trash Pump | 0.69 | | | | |
| | Cranes | 0.47 | | | | |
| | Gas Compressor | 0.85 | | | | |
| | Paving Equipment | 0.59 | | | | |
| | Pressure Washer | 0.85 | | | | |
| | Rollers | 0.62 | | | | |
| | Rough Terrain Forklifts | 0.63 | | | | |
| | Rubber Tired Loaders | 0.54 | | | | |
| | Skid Steer Loaders | 0.58 | | | | |
| | Tractors/Loaders/Backhoes | 0.48 | | | | |

Table IV-8 (Continued) Off-Road LSI Equipment Default Load Factors

| Category | Equipment Type | Load Factor |
|--------------|--------------------|-------------|
| Construction | Trenchers | 0.66 |
| | Welders | 0.51 |
| | Other Construction | 0.48 |
| Industrial | Aerial Lifts | 0.46 |
| | Forklifts | 0.30 |
| | Sweepers/Scrubbers | 0.71 |
| | Other Industrial | 0.54 |

Table IV-9 Off-Road LSI Engines Emission Factors (g/bhp-hr)

| Harman III | | | | | | | |
|------------|----------|-------------------------------------|-------|------|-------|--|--|
| Horsepower | Fuel | Model Year | NOx | ROG | PM10 | | |
| 25 – 49 | Gasoline | Uncontrolled – pre-2004 | 8.01 | 3.81 | 0.060 | | |
| | | Controlled 2001-2006 | 1.33 | 0.72 | 0.060 | | |
| | | Controlled 2007-2009 ^(a) | 0.89 | 0.48 | 0.060 | | |
| | | Controlled 2010+ | 0.27 | 0.14 | 0.060 | | |
| | Alt Fuel | Uncontrolled – pre-2004 | 13.00 | 0.90 | 0.060 | | |
| | | Controlled 2001-2006 | 1.95 | 0.09 | 0.060 | | |
| | | Controlled 2007-2009 ^(a) | 1.30 | 0.06 | 0.060 | | |
| | | Controlled 2010+ | 0.39 | 0.02 | 0.060 | | |
| 50 – 120 | Gasoline | Uncontrolled – pre-2004 | 11.84 | 2.66 | 0.060 | | |
| | | Controlled 2001-2006 | 1.78 | 0.26 | 0.060 | | |
| _ | | Controlled 2007-2009 ^(a) | 1.19 | 0.18 | 0.060 | | |
| | | Controlled 2010+ | 0.36 | 0.05 | 0.060 | | |
| | Alt Fuel | Uncontrolled – pre-2004 | 10.51 | 1.02 | 0.060 | | |
| | | Controlled 2001-2006 | 1.58 | 0.11 | 0.060 | | |
| | | Controlled 2007-2009 ^(a) | 1.05 | 0.07 | 0.060 | | |
| | | Controlled 2010+ | 0.32 | 0.02 | 0.060 | | |
| >120 | Gasoline | Uncontrolled – pre-2004 | 12.94 | 1.63 | 0.060 | | |
| | | Controlled 2001-2006 | 1.94 | 0.16 | 0.060 | | |
| | | Controlled 2007-2009 ^(a) | 1.29 | 0.11 | 0.060 | | |
| | | Controlled 2010+ | 0.39 | 0.03 | 0.060 | | |
| | Alt Fuel | Uncontrolled – pre-2004 | 10.51 | 0.90 | 0.060 | | |
| | | Controlled 2001-2006 | 1.58 | 0.09 | 0.060 | | |
| | | Controlled 2007-2009 ^(a) | 1.05 | 0.06 | 0.060 | | |
| | | Controlled 2010+ | 0.32 | 0.02 | 0.060 | | |

a - Emission factors for federally certified engines used in preempt equipment.

Table IV-10 Emission Factors for Off-Road LSI Engine Retrofits Verified to Absolute Emission Number (g/bhp-hr)

Manufacturers of LSI retrofit systems may verify to a percent emission reduction or absolute emissions. If a retrofit system is verified to a percent reduction, the emission factors will be that verified percent of the appropriate emissions factors in Table IV-9. If a retrofit system is verified to an absolute emission number, use the following table for the emission factors.

| Fuel | Verified Value | NOx | ROG | PM10 |
|----------|----------------|------|------|-------|
| Gasoline | 3.0 g/bhp-hr | 1.78 | 0.26 | 0.060 |
| | 2.5 g/bhp-hr | 1.48 | 0.22 | 0.060 |
| | 2.0 g/bhp-hr | 1.19 | 0.18 | 0.060 |
| | 1.5 g/bhp-hr | 0.89 | 0.13 | 0.060 |
| | 1.0 g/bhp-hr | 0.59 | 0.09 | 0.060 |
| | 0.6 g/bhp-hr | 0.36 | 0.05 | 0.060 |
| | 0.5 g/bhp-hr | 0.30 | 0.04 | 0.060 |
| Alt Fuel | 3.0 g/bhp-hr | 1.58 | 0.10 | 0.060 |
| | 2.5 g/bhp-hr | 1.32 | 0.09 | 0.060 |
| | 2.0 g/bhp-hr | 1.05 | 0.07 | 0.060 |
| | 1.5 g/bhp-hr | 0.79 | 0.05 | 0.060 |
| | 1.0 g/bhp-hr | 0.53 | 0.03 | 0.060 |
| | 0.6 g/bhp-hr | 0.32 | 0.02 | 0.060 |
| | 0.5 g/bhp-hr | 0.26 | 0.02 | 0.060 |

Table IV-11
Off-Road LSI Engines Certified to Optional Standards
Emission Factors (g/bhp-hr)

| | | Emission Factors (g | <i>J</i> /D11p-111 <i>)</i> | | |
|------------|----------|---------------------|-----------------------------|------|-------|
| Horsepower | Fuel | Optional Standard | NOx | ROG | PM10 |
| 25-50 | Gasoline | 1.50 | 0.67 | 0.36 | 0.060 |
| | | 1.00 | 0.44 | 0.24 | 0.060 |
| | | 0.60 | 0.27 | 0.14 | 0.060 |
| | | 0.40 | 0.18 | 0.10 | 0.060 |
| | | 0.20 | 0.09 | 0.05 | 0.060 |
| | | 0.10 | 0.04 | 0.02 | 0.060 |
| | Alt Fuel | 1.50 | 0.98 | 0.05 | 0.060 |
| | | 1.00 | 0.65 | 0.03 | 0.060 |
| | | 0.60 | 0.39 | 0.02 | 0.060 |
| | | 0.40 | 0.26 | 0.01 | 0.060 |
| | | 0.20 | 0.13 | 0.01 | 0.060 |
| | | 0.10 | 0.07 | 0.00 | 0.060 |
| 50-120 | Gasoline | 1.50 | 0.89 | 0.13 | 0.060 |
| | | 1.00 | 0.59 | 0.09 | 0.060 |
| | | 0.60 | 0.36 | 0.05 | 0.060 |
| | | 0.40 | 0.24 | 0.04 | 0.060 |
| | | 0.20 | 0.12 | 0.02 | 0.060 |
| | | 0.10 | 0.06 | 0.01 | 0.060 |
| | Alt Fuel | 1.50 | 0.79 | 0.05 | 0.060 |
| | | 1.00 | 0.53 | 0.03 | 0.060 |
| | | 0.60 | 0.32 | 0.02 | 0.060 |
| | | 0.40 | 0.21 | 0.01 | 0.060 |
| | | 0.20 | 0.11 | 0.01 | 0.060 |
| | | 0.10 | 0.05 | 0.00 | 0.060 |
| >120 | Gasoline | 1.50 | 0.97 | 0.08 | 0.060 |
| | | 1.00 | 0.65 | 0.05 | 0.060 |
| | | 0.60 | 0.39 | 0.03 | 0.060 |
| | | 0.40 | 0.26 | 0.02 | 0.060 |
| | | 0.20 | 0.13 | 0.01 | 0.060 |
| | | 0.10 | 0.06 | 0.01 | 0.060 |
| | Alt Fuel | 1.50 | 0.79 | 0.05 | 0.060 |
| | | 1.00 | 0.53 | 0.03 | 0.060 |
| | | 0.60 | 0.32 | 0.02 | 0.060 |
| | | 0.40 | 0.21 | 0.01 | 0.060 |
| | | 0.20 | 0.11 | 0.01 | 0.060 |
| | | 0.10 | 0.05 | 0.00 | 0.060 |

LOCOMOTIVES

Table IV-12a Locomotive Emission Factors (g/bhp-hr) Based on 1998 Federal Standards

| Engine Model Year | Туре | NOx ^(a) | ROG ^(b) | PM10 ^(a) |
|----------------------|----------------------------|--------------------|--------------------|---------------------|
| Pre-1973 | Line-haul and Passenger | 12.22 | 0.51 | 0.275 |
| | Switcher | 16.36 | 1.06 | 0.378 |
| 1973-2001 Tier 0 | Line-haul and Passenger | 8.93 | 1.05 | 0.516 |
| | Switcher | 13.16 | 2.21 | 0.619 |
| 2002-2004 Tier 1 | Line-haul and Passenger | 6.96 | 0.58 | 0.387 |
| | Switcher | 10.34 | 1.26 | 0.464 |
| 2005-2011 Tier 2 | Line-haul and Passenger | 5.17 | 0.32 | 0.172 |
| | Switcher | 7.61 | 0.63 | 0.206 |

These factors are to be used for the project baseline emissions if the baseline locomotive is certified or required to be certified to the 1998 federal locomotive remanufacture standards and for the reduced emission locomotive if the project locomotive is remanufactured to these 1998 standards. Factors are based upon Regulatory Impact Analysis: Final United States Environmental Protection Agency (U.S. EPA) Locomotive Regulation (2008).

a - NOx and PM10 emission factors have been adjusted by a factor of 0.94 and 0.86, respectively, to account for use of California ultra-low sulfur diesel fuel.

b - ROG = HC * 1.053

Table IV-12b Locomotive Emission Factors (g/bhp-hr)

Based on 2008 Federal Standards

| Engine Model Year | Туре | NOx ^(a) | ROG ^(b) | PM10 ^(a) |
|----------------------|----------------------------|--------------------|--------------------|---------------------|
| 1973-2001 Tier 0+ | Line-haul and Passenger | 6.96 | 0.58 | 0.189 |
| | Switcher | 11.09 | 2.21 | 0.224 |
| 2002-2004 Tier 1+ | Line-haul and Passenger | 6.96 | 0.58 | 0.189 |
| | Switcher | 10.34 | 1.26 | 0.224 |
| 2005-2011 Tier 2+ | Line-haul and Passenger | 5.17 | 0.32 | 0.086 |
| | Switcher | 7.61 | 0.63 | 0.112 |
| 2011-2014 Tier 3 | Line-haul and Passenger | 5.17 | 0.32 | 0.086 |
| | Switcher | 4.70 | 0.63 | 0.086 |
| 2015 Tier 4 | Line-haul and Passenger | 1.22 | 0.15 | 0.026 |
| | Switcher | 1.22 | 0.15 | 0.026 |

These factors are to be used for the project baseline emissions if the baseline locomotive is certified or required to be certified to the new (2008) federal locomotive remanufacture standards, and for the reduced emission locomotive if the project locomotive is remanufactured to the new standards or meets Tier 3 standards. Factors are based upon Regulatory Impact Analysis: Final U.S. EPA Locomotive Regulation (2008).

a - NOx and PM10 emission factors have been adjusted by a factor of 0.94 and 0.86, respectively, to account for use of California ultra-low sulfur diesel fuel.

b - ROG = HC * 1.053

Table IV-13
Locomotive Idle-Limiting Device Emission Reduction Factors

| Туре | Factor |
|-----------|--------|
| Switchers | 0.90 |
| Line-Haul | 0.97 |
| Passenger | 0.97 |

Note: Factors based on assumption Idle Limiting Device (ILD) reduces locomotive engine idling by 50 percent. Multiply total baseline emissions by this factor to determine reduced emissions with ILD.

MARINE VESSELS

Table IV-14a
Uncontrolled Harbor Craft Propulsion Engine
Emission Factors (g/bhp-hr)

| Horsepower | Model Year | NOx | ROG | PM10 |
|------------|------------|-------|------|-------|
| 25-50 | All | 7.57 | 1.32 | 0.520 |
| 51-120 | pre-1997 | 14.27 | 1.04 | 0.575 |
| | 1997+ | 9.70 | 0.71 | 0.524 |
| 121-250 | pre-1971 | 15.36 | 0.95 | 0.527 |
| | 1971-1978 | 14.27 | 0.79 | 0.451 |
| | 1979-1983 | 13.17 | 0.72 | 0.376 |
| | 1984+ | 12.07 | 0.68 | 0.376 |
| 251+ | pre-1971 | 15.36 | 0.91 | 0.506 |
| | 1971-1978 | 14.27 | 0.76 | 0.431 |
| | 1979-1983 | 13.17 | 0.68 | 0.363 |
| | 1984-1994 | 12.07 | 0.65 | 0.363 |
| 251-750 | 1995+ | 8.97 | 0.49 | 0.260 |
| 751+ | 1995+ | 12.07 | 0.60 | 0.363 |

Table IV-14b
Controlled Harbor Craft Propulsion Engine
Emission Factors (g/bhp-hr)

| | illissioii i a | , , | , | |
|------------|----------------|------|------|-------|
| Horsepower | Tier | NOx | ROG | PM10 |
| 25-50 | 1 | 6.93 | 1.30 | 0.580 |
| | 2 | 5.04 | 1.30 | 0.240 |
| | 3 | 5.04 | 1.30 | 0.176 |
| 51-120 | 1 | 6.93 | 0.71 | 0.524 |
| | 2 | 5.04 | 0.71 | 0.240 |
| | 3 | 5.04 | 0.71 | 0.176 |
| 121-175 | 1 | 8.97 | 0.49 | 0.290 |
| | 2 | 4.84 | 0.49 | 0.176 |
| | 3 | 3.60 | 0.49 | 0.077 |
| 176-750 | 1 | 8.97 | 0.49 | 0.290 |
| | 2 | 4.84 | 0.49 | 0.120 |
| | 3 | 3.87 | 0.49 | 0.068 |
| 751-1900 | 1 | 8.97 | 0.49 | 0.290 |
| | 2 | 5.24 | 0.49 | 0.160 |
| | 3 | 3.87 | 0.49 | 0.068 |
| 1901 + | 1 | 8.97 | 0.49 | 0.290 |
| | 2 | 5.24 | 0.49 | 0.160 |
| | 3 | 4.14 | 0.49 | 0.085 |

Table IV-15a Uncontrolled Harbor Craft Auxiliary Engine Emission Factors (g/bhp-hr)

| Horsepower | Model Year | NOx | ROG | PM10 |
|------------|------------|-------|------|-------|
| 25-50 | all | 6.42 | 1.58 | 0.460 |
| 51-120 | pre-1997 | 12.09 | 1.23 | 0.508 |
| | 1997+ | 8.14 | 0.85 | 0.417 |
| 121-250 | pre-1971 | 13.02 | 1.13 | 0.466 |
| | 1971-1978 | 12.09 | 0.94 | 0.399 |
| | 1979-1983 | 11.16 | 0.86 | 0.333 |
| | 1984-1995 | 10.23 | 0.82 | 0.333 |
| | 1996+ | 7.75 | 0.59 | 0.255 |
| 251-750 | pre-1971 | 13.02 | 1.08 | 0.448 |
| | 1971-1978 | 12.09 | 0.90 | 0.381 |
| | 1979-1983 | 11.16 | 0.81 | 0.321 |
| | 1984-1994 | 10.23 | 0.77 | 0.321 |
| | 1995+ | 7.60 | 0.58 | 0.230 |
| 751 + | pre-1971 | 13.02 | 1.08 | 0.448 |
| | 1971-1978 | 12.09 | 0.90 | 0.381 |
| | 1979-1986 | 11.16 | 0.81 | 0.321 |
| | 1987-1998 | 10.23 | 0.72 | 0.321 |
| | 1999+ | 7.75 | 0.58 | 0.255 |

Table IV-15b
Controlled Harbor Craft Auxiliary Engine
Emission Factors (g/bhp-hr)

| Emission ractors (g/bnp-m) | | | | |
|----------------------------|------|------|------|-------|
| Horsepower | Tier | NOx | ROG | PM10 |
| 25-50 | 1 | 6.54 | 1.54 | 0.511 |
| | 2 | 5.04 | 1.54 | 0.240 |
| | 3 | 5.04 | 1.54 | 0.176 |
| 51-120 | 1 | 6.93 | 0.85 | 0.464 |
| | 2 | 5.04 | 0.85 | 0.240 |
| | 3 | 5.04 | 0.85 | 0.176 |
| 121-175 | 1 | 6.93 | 0.58 | 0.255 |
| | 2 | 4.84 | 0.58 | 0.176 |
| | 3 | 3.60 | 0.58 | 0.077 |
| 176-750 | 1 | 6.93 | 0.58 | 0.255 |
| | 2 | 4.84 | 0.58 | 0.120 |
| | 3 | 3.78 | 0.58 | 0.068 |
| 751-1900 | 1 | 6.93 | 0.58 | 0.255 |
| | 2 | 5.24 | 0.58 | 0.160 |
| | 3 | 3.87 | 0.58 | 0.068 |
| 1901 + | 1 | 6.93 | 0.58 | 0.255 |
| | 2 | 5.24 | 0.58 | 0.160 |
| | 3 | 4.14 | 0.58 | 0.085 |

Table IV-16 Harbor Craft Load Factors

| Vessel Type | Propulsion Engine | Auxiliary Engine |
|--------------------|-------------------|------------------|
| Charter Fishing | 0.52 | |
| Commercial Fishing | 0.27 | |
| Ferry/Excursion | 0.42 | |
| Pilot | 0.51 | 0.43 |
| Tow | 0.68 | |
| Work | 0.45 | |
| Other | 0.52 | |
| Barge/Dredge | 0.45 | 0.65 |
| Crew & Supply | 0.38 | 0.32 |
| Tug | 0.50 | 0.31 |

Table IV-17
Shore Power
Default Emission Rates Grams per kilowatt-hour (g/kWh)

| Pollutant | Emission Rate |
|--|---------------|
| NOx | 13.9 |
| ROG | 0.49 |
| PM10 (marine gas oil fuel with 0.11- 0.5 % sulfur content) | 0.38 |
| PM10 (marine gas oil fuel with <= 0.10 % sulfur content) | 0.25 |

Table IV-18
Shore Power
Default Power Requirements

| Default Fower Requirements | | | | | |
|----------------------------|--|------------------------|--|--|--|
| Ship Category | Ship Size / Type Default Twenty-foot Equivalent Unit (TEU) | Power Requirement (kW) | | | |
| Container Vessel | <1,000 | 1,000 | | | |
| | 1,000 – 1,999 | 1,300 | | | |
| | 2,000 – 2,999 | 1,600 | | | |
| | 3,000 – 3,999 | 1,900 | | | |
| | 4,000 – 4,999 | 2,200 | | | |
| | 5,000 – 5,999 | 2,300 | | | |
| | 6,000 – 6,999 | 2,500 | | | |
| | 7,000 – 7,999 | 2,900 | | | |
| | 8,000 – 9,999 | 3,300 | | | |
| | 10,000 – 12,000 | 3,700 | | | |
| Passenger Vessel | No Default Value – Use Actual Power Requirement ^(a) | | | | |
| Reefer | Break Bulk | 1,300 | | | |
| | Fully containerized | 3,300 | | | |

a - The average power requirement for passenger vessels is 7,400 kW (ARB Oceangoing Vessel Survey, 2005).

ALL ENGINES

Table IV-19
Fuel Consumption Rate Factors (bhp-hr/gal)

| Category | Horsepower/Application | Fuel Consumption Rate |
|------------------------------------|---|-----------------------|
| Non-Mobile Agricultural Engines | ALL | 17.5 |
| Locomotive | Line Haul and Passenger (Class I/II) | 20.8 |
| | Line Haul and Passenger (Class III) | 18.2 |
| | Switcher | 15.2 |
| Other | < 750 hp | 18.5 |
| | ≥ 750 hp | 20.8 |

Table IV-20 Shore Power Default Emission Rates (Grams per kilowatt-hour (g/kW-hr))

| Pollutant | Emission Rate |
|--|---------------|
| NOx | 13.09 |
| ROG | 0.49 |
| PM10 (marine gas oil fuel with 0.11- 0.5 % sulfur content) | 0.38 |
| PM10 (marine gas oil fuel with <= 0.10 % sulfur content) | 0.25 |

Table IV-21 Shore Power Default Power Requirements

| Ship Category | Ship Size / Type Default (Twenty-foot Equivalent Unit (TEU)) | Power Requirement (kW) |
|------------------|--|------------------------|
| Container Vessel | <1,000 | 1,000 |
| | 1,000 – 1,999 | 1,300 |
| | 2,000 – 2,999 | 1,600 |
| | 3,000 – 3,999 | 1,900 |
| | 4,000 – 4,999 | 2,200 |
| | 5,000 – 5,999 | 2,300 |
| | 6,000 - 6,999 | 2,500 |
| | 7,000 – 7,999 | 2,900 |
| | 8,000 – 9,999 | 3,300 |
| | 10,000 – 12,000 | 3,700 |
| Passenger Vessel | No Default Value – Use Actual Power Requirement ^(a) | |
| Reefer | Break Bulk | 1,300 |
| | Fully containerized | 3,300 |

^(a) The average power requirement for passenger vessels is 7,400 kW (ARB Oceangoing Vessel Survey, 2005).

Table IV-24
Capital Recovery Factor (CRF) for Various Project Lives
At a 1% Discount Rate

| Project Life | CRF |
|--------------|-------|
| 1 | 1.010 |
| 2 | 0.508 |
| 3 | 0.340 |
| 4 | 0.256 |
| 5 | 0.206 |
| 6 | 0.173 |
| 7 | 0.149 |
| 8 | 0.131 |
| 9 | 0.117 |
| 10 | 0.106 |
| 11 | 0.096 |
| 12 | 0.089 |
| 13 | 0.082 |
| 14 | 0.077 |
| 15 | 0.072 |
| 16 | 0.068 |
| 17 | 0.064 |
| 18 | 0.061 |
| 19 | 0.058 |
| 20 | 0.055 |