# Toxic Air Contaminant Emissions Inventory and Dispersion Modeling Report for the Colton Rail Yard, Bloomington, California 

prepared for:

## Union Pacific Railroad Company

October 2007
prepared by:


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## SUMMARY

In accordance with the 2005 California Air Resources Board (CARB)/Railroad Statewide Agreement (MOU), Union Pacific Railroad Company (UPRR) has prepared a facilitywide emission inventory for the Colton Rail Yard (Yard) in Bloomington, California. The inventory quantifies emissions of specified toxic air contaminants (TACs) (including Diesel particulate matter [DPM]) from stationary, mobile, and portable sources at the Yard. The inventory was prepared in accordance with CARB's Rail Yard Emission Inventory Methodology guidelines (July 2006) and UPRR's Emission Inventory Protocol (May 2006).

The Colton Yard is a locomotive servicing facility. Activities at Colton include receiving inbound trains, building and departing outbound trains, locomotive refueling, locomotive servicing, and sand tower operations. Facilities and equipment include a locomotive shop, a service track, a locomotive wash, a sand tower, Diesel fuel storage tanks, various oil storage tanks, and a wastewater treatment plant.

Emission sources at the Yard include, but are not limited to, locomotives, heavy-heavyduty (HHD) Diesel-fueled delivery trucks, heavy equipment, fuel storage tanks, and an emergency generator. Emissions were calculated on a source-specific and facility-wide basis for the 2005 baseline year.

An air dispersion modeling analysis was also conducted for the Yard. The purpose of the analysis was to estimate ground-level concentrations of DPM and other TACs, emitted from Yard operations, at receptor locations near the Yard. Emission sources included in the modeling analysis were locomotives and Diesel-fueled heavy equipment. The air dispersion modeling was conducted using the AERMOD Gaussian plume dispersion model and meteorological data from the Ontario International Airport. The meteorological data were processed using the AERMET program. The modeling analysis was conducted in accordance with the Health Risk Assessment Guidance for Rail Yard and Intermodal Facilities (July 2006) and UPRR's Modeling Protocol (August 2006).

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# Toxic Air Contaminant Emission Inventory and Air Dispersion Modeling Report <br> for the <br> Colton Rail Yard Bloomington, California 

## PART I. INTRODUCTION

In accordance with the 2005 California Air Resources Board (CARB)/Railroad Statewide Agreement (MOU), Union Pacific Railroad Company (UPRR) has prepared a facilitywide emission inventory for the Colton Rail Yard ${ }^{1}$ (Yard) in Bloomington, California.. The inventory quantifies emissions of specified toxic air contaminants (TACs) (including Diesel particulate matter [DPM]) from stationary, mobile, and portable sources at the Yard. The inventory was prepared in accordance with CARB's Rail Yard Emission Inventory Methodology guidelines (July 2006) and UPRR's Emission Inventory Protocol (May 2006).

An air dispersion modeling analysis was also conducted for the Yard. The purpose of the analysis was to estimate ground-level concentrations of DPM and other TACs, emitted from Yard operations, at receptor locations near the Yard. Emission sources included in the modeling analysis were locomotives and Diesel-fueled heavy equipment. The air dispersion modeling was conducted using the AERMOD Gaussian plume dispersion model and meteorological data from the Ontario International Airport. The meteorological data were processed using the AERMET program. The modeling analysis was conducted in accordance with the Health Risk Assessment Guidance for Rail Yard and Intermodal Facilities (July 2006) and UPRR's Modeling Protocol (August 2006).

[^0]
## PART II. FACILITY DESCRIPTION

A. Facility Name and Address<br>Union Pacific Railroad Company<br>Colton Rail Yard<br>19100 Slover Avenue<br>Bloomington, CA 92316<br>\section*{B. Facility Contact Information}<br>Brock Nelson<br>Director of Environmental Operations - West<br>Union Pacific Railroad Company<br>10031 Foothills Boulevard<br>Roseville, CA 95747<br>Phone: (916) 789-6370<br>Fax: (402) 233-3162<br>banelson@up.com<br>\section*{C. Main Purpose of the Facility}

The Colton Yard is a classification yard. The primary function of a classification yard is to "break" arriving trains into sections based on their final destinations, and to build new trains that then depart for the desired destinations. This is accomplished by pushing the connected cars of an arriving train from the Receiving Yard over a "hump" (a raised section of track). Cars are decoupled at the top of the hump and gravity allows the cars roll into the "bowl." The bowl is a large area with a number of parallel tracks. A computer controls switching each car into the appropriate track within the bowl. Yard switcher locomotives build new trains by pulling sections of cars out of the bowl, connecting them to others with the same destination(s), and moving them to the Departure Yard, thereby creating a new outbound train.

There is also a locomotive service facility at the Yard that performs both basic service and scheduled and unscheduled maintenance and load testing. In 2005, all service and maintenance was performed at the service track, while a new locomotive shop facility was constructed at the east end of the Yard.

## D. Types of Operations Performed at the Facilities

Activities at the Colton Yard include receiving inbound trains, building and departing outbound trains, locomotive refueling, locomotive servicing, locomotive maintenance, locomotive washing, and sand tower operations. There are a number of tanks at the facility that are used to store liquid petroleum products such as Diesel fuel, gasoline, lubricating oils, and recovered oil.

Within the Yard, the primary locomotive activities are associated with arriving and departing trains and servicing the locomotives that power these trains. Arriving and departing trains' locomotives are fueled in the locomotive service area after arrival, and are sent back into the Yard or to other yards after service. A locomotive maintenance shop also performs periodic and unscheduled maintenance on locomotives.

Facilities and equipment at the Colton Yard include a locomotive shop, ${ }^{2}$ a locomotive service track, a locomotive wash area, a wheel shop, ${ }^{3}$ a sand tower, a railcar repair shop, Diesel fuel storage tanks, various oil storage tanks, and a wastewater treatment plant.

## E. Facility Operating Schedule

The Colton Yard operates 24 hours per day, 365 days per year.

## F. General Land Use Surrounding the Facility

The Colton Yard covers a narrow area approximately $2 \frac{1}{4}$ miles in length (tracks and train pushback areas extend both east and west of the main Yard) and $1 / 3$ mile in width, at the widest part. The Yard is located adjacent to and directly south of the I-10 freeway. Land use north of the Yard includes commercial, industrial, and residential areas. There are several truck distribution centers just north of the I-10. The nearest residential area is

[^1]located at the west end of the Yard, just north of the I-10, approximately 500 feet from the Yard boundary. Land use to the south of the Yard includes residential and industrial areas. There are a number of truck distribution centers and a bulk fuel storage plant in this area. The nearest residential area is located at the west end of the Yard about 350 feet from the Yard's southern boundary. Bloomington Junior High School is located south of the Yard, just east of Cedar Avenue. Land uses to the east and west include commercial and residential areas. There are also a number of schools in these areas. The location of specific receptors is further discussed in Part IX.

Figure 1

## Location Map


$\underset{0.0}{0.0} \underset{0.5}{0.5} \underset{1.0}{0.5} \underset{1.5}{1.5} \mathrm{~km}$

Figure 2
Colton Rail Yard Layout

## PART IV. COVERED SOURCES

This emission inventory quantifies toxic air contaminant (TAC) emissions from the stationary, mobile, and portable sources located or operating at the Colton Yard. Sources include, but are not limited to, locomotives, yard trucks of various vehicle weight classes, heavy-heavy duty (HHD) Diesel-fueled delivery trucks, Diesel-fueled heavy equipment, various storage tanks, a wastewater treatment plant, and an emergency generator. Sitespecific equipment inventories are included in Part V below.

Per the UPRR Emission Inventory Protocol, stationary point sources that are exempt from local air district rules have been identified, but not included in the detailed emission inventory. Also, de minimis sources, based on weighted risk, have been identified in the inventory, but have not been further discussed or included in the modeling analysis.
De minimis sources are the individual sources that represent less than $3 \%$ of the facilitytotal weighted-average site health risk (determined separately for cancer risk and noncancer chronic health hazard). Total exclusions for all de minimis sources did not exceed $10 \%$ of the facility-total weighted average site cancer risk or chronic health hazard.

De minimis sources are further discussed in Part VIII of this report.

## PART V. SITE-SPECIFIC INVENTORIES

As discussed in Part IV above, there are a number of mobile, stationary, and portable emissions sources operating at the Colton Rail Yard. The mobile sources include locomotives, heavy-heavy duty (HHD) Diesel-fueled delivery trucks, and heavy equipment. The stationary emission sources include storage tanks, a sand tower, a wastewater treatment plant, heaters, and an emergency generator. Portable equipment operating at the Yard includes welders, air compressors, steam cleaners, and pressure washers. Each source group is further discussed below.

## A. Locomotives

Locomotive activities at the Yard fall into several categories. "Road power" (locomotives used on inbound and outbound freight and passenger trains) activities include hauling through trains on the main line; pulling arriving trains into the Receiving Yard and departing trains out of the Departure Yard; and moving locomotives to and from the Service Track and Ready Track. Operations within the Yard include the use of 12 medium-horsepower switcher locomotives: two sets of three locomotives push inbound trains over the Hump into the Bowl; and three sets of two locomotives work the east end of the Bowl and the Departure Yard to build new outbound trains. Locomotive servicing and maintenance activities are performed on both road power and switcher locomotives, and include idling associated with refueling, sanding, oiling, and waiting to move to outbound trains. Additional periods of idling and operation at higher throttle settings occur during load test events that follow specific maintenance tasks.

Table 1 provides the number of locomotives in operation (arrivals, departures, and through traffic) at the Yard during 2005 by locomotive model group and type of train, including both working and non-working units. Through trains, including both freight trains and Amtrak passenger trains, as well as through power moves, ${ }^{4}$ use the main line

[^2]passing by the facility. All terminating trains arrive in the Receiving Yard. All originating trains depart from the Departure Yard.

| Table 1 <br> Locomotive Models (Road Power) Identified at Colton Rail Yard |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Train Type ${ }^{\text {a }}$ |  |  |  |  |
| Locomotive <br> Model <br> Group | Through Trains | Freight Trains | Local Trains | Power Moves Through | Power Moves In Yard |
| Switch ${ }^{\text {b }}$ | 2 | 65 | 64 | 0 | 22 |
| GP3x | 15 | 227 | 177 | 0 | 75 |
| GP4x | 1450 | 5607 | 1889 | 76 | 1079 |
| GP50 | 160 | 364 | 13 | 3 | 43 |
| GP60 | 972 | 12328 | 6337 | 48 | 5105 |
| SD7x | 8116 | 10284 | 154 | 94 | 900 |
| SD90 | 131 | 232 | 20 | 5 | 51 |
| Dash7 | 6 | 132 | 0 | 0 | 3 |
| Dash8 | 1908 | 3493 | 72 | 29 | 475 |
| Dash9 | 4191 | 13149 | 269 | 60 | 988 |
| C60A | 38 | 70 | 0 | 1 | 11 |
| Unknown | 162 | 463 | 62 | 4 | 56 |
| Total | 17151 | 46414 | 9057 | 320 | 8808 |

Notes:
a. Includes all locomotives identified on an arriving, a departing, or a through train, including both working and non-working units.
b. Does not include switcher locomotives used for Yard operations.

## B. Diesel-Fueled Trucks (Yard Trucks)

UPRR operates a variety of on-road Diesel-fueled trucks (Yard trucks) that are used for various activities in and around the Yard. Table 2 shows the equipment specifications for the Diesel-fueled Yard trucks.

| Equipment Specifications for Diesel-Fueled Yard Trucks <br> Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment ID | Make | Model | Model Year | Vehicle Class |
| 69496 | Chevy | CK 3500 | 1998 | LDT |
| 69499 | Chevy | CK 3500 | 1998 | LDT |
| $1915-73119$ | Ford | F-450 | 2003 | LHDT1 |
| 9007 E | Ford | F-800 | 1992 | MHD |
| 9009 E | Ford | F-800 | 1992 | MHD |
| 9031 E | Ford | F-800 | 1992 | MHD |
| 9018 E | Ford | F-800 | 1992 | MHD |
| Unknown | International | Unknown | 1987 | HHD |
| 64274 | Ford | LT8000 | 1989 | HHD |
| $1915-9038 \mathrm{E}$ | Ford | LT9000 | 1997 | HHD |
|  |  |  |  |  |
| Notes: <br> a. Vehicle specifications provided by UPRR personnel. |  |  |  |  |
|  |  |  |  |  |

## C. HHD Diesel-Fueled Delivery Trucks

A variety of HHD Diesel-fueled trucks operate at Colton each day. The HHD trucks deliver Diesel fuel, gasoline, various oils, sand, and soap to the Yard. The trucks are owned by independent operators. Therefore, a fleet distribution is not available. For emission calculations, the EMFAC 2007 model default fleet distribution for HHD Dieselfueled trucks operating in Los Angeles County was used.

## D. Heavy Equipment

Diesel-fueled heavy equipment is used in Yard operations at Colton. The heavy equipment is used for non-cargo-related activities at the Yard, such as locomotive maintenance, handling of parts and Company material, derailments, etc. Table 3 provides detailed information for the heavy equipment used at Colton.

| Table 3 <br> Equipment Specifications for Heavy Equipment <br> Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment Type | Make/Model | Model <br> Year | Rating <br> $(\mathrm{hp})$ | No. of <br> Units |
| Rail Cleaner | Unknown | 2003 | 125 | 1 |
| Rerailer | Cline | 1987 | 183 | 1 |
| Crane | Lorain LRT-250 | 1997 | 145 | 1 |
| Forklift | Toyota 6EDU45 | 1999 | 79 | 1 |
| Total |  |  |  | $\mathbf{4}$ |

## E. Tanks

There are a number of tanks at the Colton Yard that are used to store liquid petroleum and other products such as Diesel fuel, gasoline, lubricating oils, recovered oil, and soap. Table 4 provides detailed information for all storage tanks located at the facility.

As shown in Table 4, all storage tanks at the facility, except the four gasoline storage tanks (tanks 1172, 1187, 1189, and 1498) are exempt from South Coast Air Quality Management District (SCAQMD) permitting requirements per Rule 219(m). Since these storage tanks are exempt from local air district rules, the emissions from these tanks are not included in the inventory or the dispersion modeling analysis, consistent with the UPRR inventory protocol.

| Table 4 Storage Tank Specifications Colton Rail Yard |  |  |  |
| :---: | :---: | :---: | :---: |
| Tank No. | Tank Location | Material Stored | Tank Capacity (gallons) |
| $1149^{\text {a }}$ | Service Track | Lube Oil | 1,000 |
| $1151{ }^{\text {a }}$ | Service Track | Lube Oil | 15,700 |
| $1152^{\text {a }}$ | Service Track | Lube Oil | 15,700 |
| $1153^{\text {a }}$ | Service Track | Diesel | 15,700 |
| $1154^{\text {a }}$ | Service Track | Diesel | 15,700 |
| $1155^{\text {a }}$ | Service Track | Journal Box Oil | 7,500 |
| $1156^{\text {a }}$ | Service Track | Journal Box Oil | 7,500 |
| $1157^{\text {a }}$ | One Spot | Used Oil | 400 |
| $1158^{\text {a }}$ | WWTP | Stormwater | 275,000 |
| $1159^{\text {a }}$ | WWTP | Stormwater | 275,000 |
| $1160^{\text {a }}$ | WWTP | Used Oil | 2,000 |
| $1161{ }^{\text {a }}$ | WWTP | Sludge | 5,000 |
| $1168^{\text {a }}$ | Locomotive Wash | Used Oil | 25,000 |
| $1169^{\text {a }}$ | Locomotive Servicing | Used Oil | 25,000 |
| 1172 | Locomotive Servicing | Gasoline | 500 |
| $1174{ }^{\text {a }}$ | Locomotive Wash | Soap | 2,500 |
| $1175^{\text {a }}$ | Locomotive Wash | Soap Mix Tank | 350 |
| $1176{ }^{\text {a }}$ | Locomotive Wash | Soap Mix Tank | 350 |
| $1177^{\text {a }}$ | Locomotive Wash | Recycled Water | 20,000 |
| $1178{ }^{\text {a }}$ | Locomotive Wash | Water | 10,000 |
| $1179{ }^{\text {a }}$ | MOW Compound | Used Oil | 500 |
| $1180^{\text {a }}$ | Locomotive Servicing | Radiator Fluid | 7,500 |
| 1187 | One Spot | Gasoline | 500 |
| 1189 | Departure Yard/Trim Tower | Gasoline | 500 |
| 1498 | One Spot | Gasoline | 500 |
| Notes: <br> a. Exempt from permitting requirements per SCAQMD Rule 219(m). |  |  |  |

## F. Sand Tower

Locomotives use sand for traction and braking. The sand tower system located at the Colton Yard consists of a storage system and a transfer system to dispense sand into locomotives. The storage system includes a pneumatic delivery system and a storage silo. The transfer system includes a pneumatic transfer system, an elevated receiving silo, and a moving hopper and gantry system. The system is equipped with a baghouse for emissions control.

## G. Wastewater Treatment Plant

The Colton Yard also has a wastewater treatment plant (WWTP). Equipment at the WWTP includes oil/water separators, pumps, and storage tanks. Operation of the oil/water separators results in fugitive emissions of VOC.

## H. Emergency Generator

An emergency generator is located in the bowl area of the Colton Yard to provide emergency lighting when electrical service from the local power provider is disrupted. The generator is a 50 horsepower, Diesel-fueled unit.

## I. Boilers and Heaters

There are two natural gas-fired boilers and one natural gas-fired heater at the Colton Yard. Equipment specifications for the boilers and heater are shown in Table 5.

Rule 219(b)(2) exempts from permitting requirements boilers and process heaters that have a maximum heat input rate of $2 \mathrm{MMBtu} / \mathrm{hr}$ or less and are equipped to be heated exclusively with natural gas, methanol, or liquefied petroleum gas or any combination thereof that does not include an internal combustion engine. As shown in Table 5, the heater and boiler located at the locomotive wash area are exempt from permitting per Rule 219(b)(2). Since these units are exempt from local air district rules, the emissions from these units are not included in this inventory or in the dispersion modeling analysis, consistent with the UPRR inventory protocol.

| Table 5 <br> Equipment Specifications for Heater and Boilers <br> Colton Rail Yard |  |  |  |
| :---: | :---: | :---: | :---: |
| Unit Type | Location | Fuel Type | Rating <br> (MMBtu/hr) |
| Heater ${ }^{\mathrm{a}}$ | Locomotive Wash | Natural Gas | 0.14 |
| Boiler ${ }^{\text {a }}$ | Locomotive Wash | Natural Gas | 1.995 |
| Boiler $^{\mathrm{b}}$ |  |  |  |
| Locomotive Shop |  |  |  |
| Notes: <br> a. Exempt from permitting requirements per SCAQMD Rule 219(b)(2). <br> b. Unit was installed in 2006. Since the unit did not operate in 2005, emissions from this unit are not <br> included in the inventory or dispersion modeling analysis. |  |  |  |

The boiler at the locomotive shop is not exempt from permitting requirements per Rule 219. However, this unit was not installed until 2006 and therefore did not operate in 2005. Since the unit did not operate in 2005, emissions from this unit are not included in the emission inventory or dispersion modeling analysis for the Yard.

## J. Portable Equipment and Steam Cleaners

A variety of portable equipment is used at the Yard. Equipment specifications for the welders and miscellaneous portable equipment are shown in Table 6.

Internal combustion engines with a rated capacity of 50 brake horsepower or less are exempt from permitting requirements by SCAQMD Rule 219(b)(1). As shown in Table 6, all welders and miscellaneous portable equipment operated at the Yards have a rated capacity of less than 50 hp , and therefore are exempt from permitting requirements. Since these units are exempt from local air district rules, the emissions from these units are not included in this inventory or in the dispersion modeling analysis, consistent with the UPRR inventory protocol.

| Table 6 <br> Portable Equipment Specifications Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment Location | Equipment Type | Number of Units | Fuel Type | Rated Capacity (hp) |
| Receiving Yard | Welder ${ }^{\text {a }}$ | 1 | Gasoline | 16 |
| Receiving Yard | Welder ${ }^{\text {a }}$ | 1 | Gasoline | 12.5 |
| Receiving Yard | Welder ${ }^{\text {a }}$ | 1 | Gasoline | 13 |
| One Spot | Welder ${ }^{\text {a }}$ | 5 | Gasoline | 13 |
| One Spot | Welder ${ }^{\text {a }}$ | 2 | Gasoline | 10 |
| Departure Yard | Welder ${ }^{\text {a }}$ | 1 | Gasoline | 12.5 |
| Departure Yard | Welder ${ }^{\text {a }}$ | 2 | Gasoline | 13 |
| Service Track | Welder ${ }^{\text {a }}$ | 3 | Gasoline | 13 |
| One Spot | Air Compressor ${ }^{\text {b }}$ | 1 | Gasoline | 8 |
| One Spot | Air Compressor ${ }^{\text {b }}$ | 1 | Gasoline | 11 |
| Bridge Department | Air Compressor ${ }^{\text {b }}$ | 1 | Diesel | 42 |
| Service Track | Pressure Washer ${ }^{\text {c }}$ | 4 | Propane | $0.325^{\text {d }}$ |
| Notes: <br> a. Exempt from permitting requirements per SCAQMD Rule 219(e)(8) and Rule 219(b)(1). <br> b. Exempt from permitting requirements per SCAQMD Rule 219(b)(1). <br> c. Exempt from permitting requirements per SCAQMD Rule 219(b)(2). <br> d. Rating for these units is in MMBtu/hr. |  |  |  |  |

Combustion equipment with a maximum rating of $2 \mathrm{MMBtu} / \mathrm{hr}$ or less that are equipped to be fired exclusively with natural gas, methanol, or liquefied petroleum gas are exempt from permitting requirements per SCAQMD Rule 219(b)(2). As shown in Table 6, the propane-fueled pressure washers have a rated capacity of less than $2 \mathrm{MMBtu} / \mathrm{hr}$ and are fired exclusively with natural gas. Therefore, these units are exempt from permitting requirements. Since these units are exempt from local air district rules, the emissions from these units are not included in this inventory or in the dispersion modeling analysis, consistent with the UPRR inventory protocol.

In addition to the portable equipment listed in Table 6, two portable steam cleaners are used at the Yard. Equipment specifications for steam cleaners are shown in Table 7.

| Table 7 <br> Equipment Specifications for Steam Cleaners Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment Location | Make | $\begin{gathered} \hline \text { Emission } \\ \text { Unit } \\ \hline \end{gathered}$ | Fuel Type | Rating (MMBtu/hr or hp ) |
| Locomotive | Hydroblaster | Pump | Electric | NA |
| Shop ${ }^{\text {a }}$ |  | Heater | Propane | 0.36 |
| Wheel Shop ${ }^{\text {a }}$ | Hydroblaster | Pump | Electric | NA |
|  |  | Heater | Propane | 0.36 |

Notes:
a. Exempt from permitting requirements per SCAQMD Rule 219(d)(5) and Rule 219(b)(2).
b. Prior to completion of the locomotive shop and the wheel shop, steam cleaning would have been done at the Service Track.

SCAQMD Rule 219(d)(5) exempts equipment that is used exclusively for steam cleaning from permitting requirements, provided that the equipment is also exempt per Rule 219(b)(2). Rule 219(b)(2) exempts from permitting requirements boilers and process heaters that have a maximum heat input rate of $2 \mathrm{MMBtu} / \mathrm{hr}$ or less and are equipped to be heated exclusively with natural gas, methanol, or liquefied petroleum gas or any combination thereof that does not include an internal combustion engine. As shown in Table 7, the steam-cleaning units at the Colton Yard are exempt from permitting per Rule 219(d)(5). Since these units are exempt from local air district rules, the emissions from these units are not included in this inventory or in the dispersion modeling analysis, consistent with the UPRR inventory protocol.

## PART VI. $\quad$ ACTIVITY DATA

Emissions from mobile sources are based on the number and type of equipment, equipment size, load factor, and operation during the 2005 baseline year. Since fuel consumption data were not available, the default load factors, from the OFFROAD2007 model, and operating data were used for emission calculations. Emissions from stationary and portable sources were based on the number and type of equipment, equipment size, and operation during the 2005 baseline year. For sources where operating data weren't available, an average operating mode (AOM) was developed based on employee interviews.

## A. Locomotives

Locomotive emissions were based on the number, model distribution, and operating conditions (idling, throttle notch, and speeds of movements, etc). Table 8 summarizes the activity data for locomotives operating on trains at the Colton Yard, including the number of trains and number of working locomotives per consist, as well as their idle and operating time, and speed on arrival or departure. In general, arriving trains enter the Receiving Yard and stop while the railcars are detached from the locomotive. After the railcars have been detached, the locomotives move to the Service Track for refueling and service, and then to the Ready Track. On departure, locomotive consists move from the Ready Track to the appropriate end of an outbound train in the Departure Yard. The train departs after completion of the Federal Railroad Administration (FRA) mandated safety inspections (e.g., air pressure and brakes) and the arrival of the train crew. Most terminating and originating freight trains follow the main line at the east or west end of the Yard. A fraction of these trains arrive from or depart toward Palmdale to the north, and were identified by their train symbols. Emission calculations and modeling assigned these specific trains to routes in the Yard that use the main line leg at the east end of the Yard that turns to the north toward Palmdale.

In some cases, trains that are nominally "through" trains (arriving and departing under the same train symbol and date) add or drop cars or locomotives at the Colton Yard, or stop
for a crew change at Cedar Avenue (east end of the Receiving Yard). These trains are counted separately, as the idling period is shorter prior to departure, and the locomotive consist is not disconnected nor moved to the service track. The data showed that nonlocal (line haul) freight trains arriving from and departing to the east used predominately newer high-horsepower SD-70 and Dash 9 locomotives, while both locals and freight trains arriving from and departing to the west used a mix of older medium- and highhorsepower and newer high-horsepower locomotives. Therefore, these two separate groups were assigned different locomotive model distributions in the emission calculations.

Power moves are groups of locomotives, with no attached railcars, that are moved between yards to provide road power for departing trains or to move malfunctioning locomotives to service areas. Although power moves may have as many as 10 or more locomotives, typically only one or two locomotives are actually operating. For emission calculations, power moves were assumed to have 1.5 operating locomotives (except for power moves involving just one locomotive). ${ }^{5}$ In addition to road power, two threelocomotive "hump sets" and three two-locomotive "trim sets" operate in the Yard to move sections of inbound trains, spot them in the appropriate areas for handling, and subsequently reconnect these sections and move them to the appropriate outbound train areas. All of the hump and trim set locomotives are medium-horsepower (GP-4x) units that operate approximately 23 hours per day in the Yard.

[^3]Table 8
Train Activity Summary ${ }^{\text {a }}$
Colton Rail Yard

| Train Type | East Bound |  | West Bound |  | Arrival/Departing Speed (mph) | $\begin{gathered} \hline \text { Idle } \\ \text { Time } \\ \text { (hrs) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | No. of Trains | Locomotives per Consist | No. of Trains | Locomotives per Consist |  |  |
| Through Trains - Mainline | 792 | 3.11 | 4,378 | 2.96 | 20 | 0.0 |
| Through Trains - In Yard | 95 | 3.11 | 178 | 2.96 | 10 | 0.5 |
| Through Trains - Crew Change | 149 | 3.11 | 4,017 | 2.96 | N/A | 0.167 |
| Freight Trains Arriving | 822 | 3.39 | 4,505 | 4.11 | 10 | 0.125 |
| Freight Trains Departing | 4,521 | 3.84 | 1,570 | 3.00 | 10 | 1.0 |
| Local Trains Arriving | 1,412 | 3.08 | 110 | 2.96 | 10 | 0.125 |
| Local Trains Departing | 24 | 2.46 | 1,213 | 2.96 | 10 | 1.0 |
| Power Moves Through | 14 | 3.21 | 49 | 4.39 | 20 | 0.0 |
| Power Moves Arriving | 546 | 3.62 | 1,071 | 2.52 | 10 | 0.0 |
| Power Moves Departing | 524 | 3.12 | 1,314 | 2.49 | 10 | 0.0 |

Notes:
a. Data reflect the number of operating locomotives; locomotives that are being transported, but are not under power, are not shown.
b. In addition to the activities described above, 12 switcher locomotives operate in the Yard. All switchers operate 23 hours per day.

A separate database provided information on each locomotive handled by the Service Track at the Yard. Based on detailed information on the reason and type of service or maintenance performed, separate counts of service and maintenance activities were developed, as detailed in Table 9. Routine service of locomotives involves idling and short movements in the service area associated with sanding, refueling, oiling, and other service activities prior to their movement to the Ready Track. Some locomotive service events occur elsewhere in the Yard, with little or no idling, as only simple service items and refueling are involved. Depending on the type of maintenance, load testing is performed prior to and/or after maintenance. The number of these test events was determined based on the service codes for each locomotive maintenance event in the database. The specific nature (duration and throttle setting) of such load testing events is described in Table 9.

| Table 9     <br>      <br> Locomotive Service and Shop Releases and Load Tests     <br> Colton Rail Yard     |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Number <br> of Events | Idling per <br> event (min) | Throttle Notch <br> 1 time (min) | Throttle Notch <br> 8 time (min) |
| Locomotive Service | 18,532 | 90 | 0 | 0 |
| Ready Track | 18,532 | 90 | 0 | 0 |
| Yard Service | 4,448 | 0 | 0 | 0 |
| Planned Maintenance Pre-Test | 661 | 2 | 0 | 8 |
| Planned Maintenance Post-Test | 661 | 10 | 10 | 10 |
| Quarterly Maintenance Test | 832 | 2 | 0 | 8 |
| Unscheduled Maintenance Diagnostic | 18 | 5 | 0 | 10 |
| Unscheduled Maintenance Post-Test | 1,048 | 10 | 10 | 10 |

## B. Diesel-Fueled Trucks (Yard Trucks)

Emissions from the on-road Diesel-fueled trucks operating at the Yard are based on the engine model year, annual vehicle miles traveled (VMT), and the amount of time spent idling. Table 10 summarizes the activity data for the on-road Diesel-fueled trucks operating at the Yard.

| Activity Data for Diesel-Fueled Yard Trucks <br> Colton Rail Yard |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment ID | Make/Model | Model <br> Year | Vehicle <br> Class | Annual <br> VMT $^{\text {a }}$ | Idling Time $^{\text {b }}$ |  |
| 69496 | Chevy CK 3500 | 1998 | LDT | 17,060 | 15 | 91 |
| 69499 | Chevy CK 3500 | 1998 | LDT | 20,042 | 15 | 91 |
| $1915-73119$ | Ford F-450 | 2003 | LHDT1 | 5,250 | 15 | 91 |
| 9007 E | Ford F-800 | 1992 | MHD | 3,353 | 15 | 91 |
| 9009 E | Ford F-800 | 1992 | MHD | 3,053 | 15 | 91 |
| 9031 E | Ford F-800 | 1992 | MHD | 9,929 | 15 | 91 |
| 9018 E | Ford F-800 | 1992 | MHD | 10,114 | 15 | 91 |
| Unknown | International | 1987 | HHD | 156 | 15 | 91 |
| 64274 | Ford LT8000 | 1989 | HHD | 18,197 | 15 | 91 |
| $1915-9038 \mathrm{E}$ | Ford LT9000 | 1997 | HHD | 16,001 | 15 | 91 |

Notes:
a. Annual VMT based on the current odometer reading and the age of the vehicle.
b. Idling time ( $\mathrm{min} /$ day) is an engineering estimate based on personal observation.

## C. HHD Diesel-Fueled Delivery Trucks

HHD Diesel-fueled trucks deliver Diesel fuel, gasoline, various oils, sand, and soap to the Yard. The annual number of delivery truck trips for liquid products was calculated based on the facility product throughput and a tanker truck capacity of 8,000 gallons per truck. The annual number of sand delivery truck trips was based on the annual sand throughput and a truck capacity of 20 tons per truck. The VMT per trip was estimated from aerial photos of the Yard. Activity data for the HHD delivery trucks are summarized in Table 11.

| Table 11Summary of HHD Delivery Truck Activity DataColton Rail Yard |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Delivery Type | Number of HHD Truck Trips ${ }^{\text {a,b }}$ | VMT per HHD Truck Trip (mi/trip) ${ }^{\text {c }}$ | Annual VMT (mi/yr) | Idling Time |  |
|  |  |  |  | $(\mathrm{min} / \text { trip })^{\text {d }}$ | (hr/yr) |
| Gasoline | 2 | 0.33 | 0.66 | 10 | 0.33 |
| Lube Oil | 57 | 0.58 | 33.06 | 10 | 9.50 |
| Used Oil | 24 | 0.58 | 13.92 | 10 | 4.00 |
| Soap | 18 | 0.71 | 12.78 | 10 | 3.00 |
| Sand | 195 | 0.58 | 113.10 | 30 | 97.50 |
| Notes: <br> a. Number of truck trips for liquid products based on the material throughput and a tanker truck volume of 8,000 gallons per truck. <br> b. Number of sand truck trips based on sand throughput and a truck capacity of 20 tons per truck. <br> c. VMT per trip estimated from aerial photos of the Yard. <br> d. Engineering estimate based on personal communication with UPRR staff. |  |  |  |  |  |

## D. Heavy Equipment

Emissions from heavy equipment operating at the Yard are based on the number and type of equipment, equipment model year, equipment size, and the annual hours of operation.

Activity data for heavy equipment are summarized in Table 12.

| Table 12 <br> Activity Data for Heavy Equipment <br> Colton Rail Yard |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment <br> Type | Make/Model | Model <br> Year | Rating <br> (hp) | No. of <br> Units | Hours of Operation <br> (hr/yr per unit) |
| Rail Cleaner | Unknown | 2003 | 125 | 1 | 5 |
| Rerailer | Cline | 1987 | 183 | 1 | $365^{\text {b }}$ |
| Crane | Lorain LRT-250 | 1997 | 145 | 1 | 260 |
| Forklift | Toyota 6EDU45 | 1999 | 79 | 1 | 312 |
| Notes: <br> a. Information provided by UPRR staff. <br> b. Items in italics are engineering estimates. |  |  |  |  |  |

## E. Tanks

Emissions from the non-exempt storage tanks Yards are based on the size of the tank, material stored, and annual throughput. Activity data for the non-exempt tanks are shown in Table 13.

| Table 13 <br> Activity Data for Non-Exempt Storage Tanks <br> Colton Rail Yard |  |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
| Tank | Tank Location | Material <br> Stored | Tank <br> Capacity <br> $(\mathrm{gal})$ | Tank <br> No. | Annual <br> $(\mathrm{ft})$ |
| 1172 | Locomotive Servicing | Gasoline | 500 | $5 \times 4.2$ | 500 |
| 1187 | One Spot | Gasoline | 500 | $5 \times 4.2$ | 3,440 |
| 1189 | Departure Yard/Trim Tower | Gasoline | 500 | $5 \times 4.2$ | 3,875 |
| 1498 | One Spot | Gasoline | 500 | $5 \times 4.2$ | 2,664 |
| Notes: <br> a. See Part V.E for a discussion of storage tank permitting exemptions. |  |  |  |  |  |

## F. Sand Tower

Emissions from the sand tower are based on the annual sand throughput. The 2005 sand throughput for the Colton Yard was 3,885 tons.

## G. Wastewater Treatment Plant

Emissions from the WWTP are based on the annual wastewater flow rate. In 2005, the wastewater flow rate at the Colton Yard was 8,636,710 gallons.

## H. Emergency Generator

Emissions from the emergency generator at the Yard are based on the rated capacity of the unit and the annual hours of operation. In 2005, the generator was operated 20 hours.

## PART VII. EMISSIONS

## A. Calculation Methodology and Emission Factors

Emission calculations were based on the site-specific equipment inventory, equipment activity data, and the source-specific emission factors. The calculation methodology and emission factors for each specific source type are further discussed below. Emissions were calculated in accordance with CARB Guidelines (July 2006) and the UPRR Emission Inventory Protocol (May 2006).

## 1. Locomotives

Emissions were calculated for UPRR-owned and -operated locomotives, as well as "foreign" locomotives ${ }^{6}$ operating in the rail yard, and through trains on the main line. Procedures for calculating emissions followed the methods described in Ireson et al. (2005). ${ }^{7}$ A copy of Ireson et al is contained in Appendix A-6.

Emissions from locomotive activities were calculated based on the number of working locomotives, ${ }^{8}$ time spent in each notch setting, and locomotive model-group distributions, with model groups defined by manufacturer and engine type. A separate calculation was performed for each type of locomotive activity, including line-haul locomotive operations, switcher locomotive operations, consist movements, locomotive refueling, and pre- and post-locomotive service and maintenance testing. Speed, movement duration, and throttle notch values were obtained from UPRR personnel for the Colton Yard for different types of activities. Movement durations were calculated from distance traveled and speed. Detailed counts of locomotive by model, tier, and train type are

[^4]shown in Appendix A-1 and A-2. Maps detailing the principal locomotive routes at the Yard are contained in Appendix A-5.

Notch-specific emission factors were assembled from a number of sources. These included emission factors presented in CARB's Roseville Rail Yard Study (October, 2004), as well as EPA certification data, and other testing performed by Southwest Research Institute on newer-technology locomotives.

For line haul operations, yard-specific average consist composition (number of units, number of units operating, model distribution, locomotive tier distribution, fraction equipped with auto start/stop technology ${ }^{9}$ ) was developed from UPRR data for different train types. Movement speed, duration, and notch estimates were developed for arriving, departing, through train, and in-yard movements. All road power movements within the Yard were assumed to be at 10 mph in throttle notches 1 and 2 ( $50 \%$ each). Idle duration was estimated based on UPRR operator estimates for units not equipped with auto start/stop. Units that were equipped with AESS/ZTR technology were assumed to idle for 30 minutes per extended idle event, with other locomotives idling for the remaining duration of the event. Numbers of arrivals and departures were developed from UPRR data. Emissions were calculated separately for through trains, intermodal train arrivals and departures, non-intermodal arrivals and departures, local trains, and power moves.

In addition to the line-haul locomotives discussed above, 12 "captive" switcher locomotives (i.e., locomotives dedicated to moving sections of rail cars within the Yard) operated within the facility boundaries during 2005. Two sets of three switcher locomotives (trim sets) push inbound trains over the Hump into the Bowl; and three sets of two switcher locomotives (hump sets) work the east end of the Bowl and the Departure Yard to build new outbound trains. Each switcher locomotive operates approximately 23 hours per day. Based on information from UPRR personnel, the trim sets were assumed

[^5]to operate on the full EPA switcher duty cycle, while the hump sets were assumed to be "pushing" in notch 2 (2 hours/day) and dynamic brake (11hours per day) through the Receiving Yard to the Hump, and returning to the west end of the Receiving Yard in notch 1 and 2 ( $50 \%$ each, 10 hours/day).

Data regarding the sulfur content of 2005 UPRR Diesel fuel deliveries within and outside of California were not available. To develop locomotive emission factors for different types of activities, estimates of fuel sulfur content were developed, and base case emission factors from the primary information sources (e.g., EPA certification data, with an assumed nominal fuel sulfur content of $3,000 \mathrm{ppm}$ ) were adjusted based on the estimated sulfur content of in-use fuels. Fuel sulfur content reportedly affects the emission rates for Diesel particulate matter from locomotives. The sulfur content in Diesel fuel varies with the type of fuel produced (e.g., California on-road fuel, 49-state off-road fuel, 49-state on-road fuel), the refinery configuration at which it is produced, the sulfur content of the crude oil being refined, and the extent to which it may be mixed with fuel from other sources during transport. As a result, it is extremely difficult to determine with precision the sulfur content of the fuel being used by any given locomotive at a specific time, and assumptions were made to estimate sulfur content for different types of activities.

To estimate the fuel sulfur content for UPRR locomotives in California during 2005, the following assumptions were made:

- "Captive" locomotives and consists in use on local trains (e.g., commuter rail) used only Diesel fuel produced in California.
- Trains arriving and terminating at California railyards (with the exception of local trains) used fuel produced outside of California, and arrive with remaining fuel in their tanks at $10 \%$ of capacity.
- On arrival, consists were refueled with California Diesel fuel, resulting in a 90:10 mixture of California and non-California fuel, and this mixture is representative of fuel on departing trains as well as trains undergoing load testing (if conducted at a specific yard).
- The average composition of fuel used in through trains bypassing a yard, and in trains both arriving and departing from a yard on the same day is $50 \%$ California fuel and $50 \%$ non-California fuel.

In 2005, Chevron was Union Pacific Railroad's principal supplier of Diesel fuel in California. Chevron's California refineries produced only one grade ("low sulfur Diesel," or LSD) in 2005. Quarterly average sulfur content for these refineries ranged from 59 ppm to 400 ppm , with an average of $221 \mathrm{ppm} .^{10}$ This value is assumed to be representative of California fuel used by UPRR. Non-California Diesel fuel for 2005 is assumed to have a sulfur content of $2,639 \mathrm{ppm}$. This is the estimated 49 -state average fuel sulfur content used by the U.S. Environmental Protection Agency in its 2004 regulatory impact analysis in support of regulation of nonroad Diesel engines (USEPA, 2004).

To develop emission inventories for locomotive activity, an initial collection of locomotive model- and notch-specific emissions data was adjusted based on sulfur content. Although there is no official guidance available for calculating this effect, a draft CARB document provides equations to calculate the effect of sulfur content on DPM emission rates at specific throttle settings, and for 2-stroke and 4-stroke engines (Wong, undated). These equations can be used to calculate adjustment factors for different fuels as described in Appendix A-7. The adjustment factors are linear in sulfur content, allowing emission rates for a specific mixture of California and non-California fuels to be calculated as a weighted average of the emission rates for each of the fuels. Adjustment factors were developed and used to prepare tables of emission factors for two different fuel sulfur levels: 221 ppm for locomotives operated on California fuel; and 2,639 ppm for locomotives operating on non-California fuel. These results are shown in Tables 14 and 15. Sample emission calculations are shown in Appendix A-3 and A-4. The calculations of sulfur adjustments and the Wong Technical Memo are shown in Appendix A-7.

[^6]Table 14

## Locomotive Diesel Particulate Matter Emission Factors (g/hr) Adjusted for Fuel Sulfur Content of 221 PPM <br> Colton Rail Yard

| Model Group | Tier | Throttle Setting |  |  |  |  |  |  |  |  |  | Source ${ }^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Idle | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |  |
| Switchers | N | 31.0 | 56.0 | 23.0 | 76.0 | 129.2 | 140.6 | 173.3 | 272.7 | 315.6 | 409.1 | CARB and ENVIRON |
| GP-3x | N | 38.0 | 72.0 | 31.0 | 110.0 | 174.1 | 187.5 | 230.2 | 369.1 | 423.5 | 555.1 | CARB and ENVIRON |
| GP-4x | N | 47.9 | 80.0 | 35.7 | 134.3 | 211.9 | 228.6 | 289.7 | 488.5 | 584.2 | 749.9 | CARB and ENVIRON |
| GP-50 | N | 26.0 | 64.1 | 51.3 | 142.5 | 282.3 | 275.2 | 339.6 | 587.7 | 663.5 | 847.2 | CARB and ENVIRON |
| GP-60 | N | 48.6 | 98.5 | 48.7 | 131.7 | 266.3 | 264.8 | 323.5 | 571.6 | 680.2 | 859.8 | CARB and ENVIRON |
| GP-60 | 0 | 21.1 | 25.4 | 37.6 | 75.5 | 224.1 | 311.5 | 446.4 | 641.6 | 1029.9 | 1205.1 | KCS7332 |
| SD-7x | N | 24.0 | 4.8 | 41.0 | 65.7 | 146.8 | 215.0 | 276.8 | 331.8 | 434.7 | 538.0 | CARB and ENVIRON |
| SD-7x | 0 | 14.8 | 15.1 | 36.8 | 61.1 | 215.7 | 335.9 | 388.6 | 766.8 | 932.1 | 1009.6 | CARB and ENVIRON |
| SD-7x | 1 | 29.2 | 31.8 | 37.1 | 66.2 | 205.3 | 261.7 | 376.5 | 631.4 | 716.4 | 774.0 | NS2630 ${ }^{\text {c }}$ |
| SD-7x | 2 | 55.4 | 59.5 | 38.3 | 134.2 | 254.4 | 265.7 | 289.0 | 488.2 | 614.7 | 643.0 | UP8353 ${ }^{\text {c }}$ |
| SD-90 | 0 | 61.1 | 108.5 | 50.1 | 99.1 | 239.5 | 374.7 | 484.1 | 291.5 | 236.1 | 852.4 | EMD 16V265H |
| Dash 7 | N | 65.0 | 180.5 | 108.2 | 121.2 | 306.9 | 292.4 | 297.5 | 255.3 | 249.0 | 307.7 | CARB and ENVIRON |
| Dash 8 | 0 | 37.0 | 147.5 | 86.0 | 133.1 | 248.7 | 261.6 | 294.1 | 318.5 | 347.1 | 450.7 | CARB and ENVIRON |
| Dash 9 | N | 32.1 | 53.9 | 54.2 | 108.1 | 187.7 | 258.0 | 332.5 | 373.2 | 359.5 | 517.0 | SWRI 2000 |
| Dash 9 | 0 | 33.8 | 50.7 | 56.1 | 117.4 | 195.7 | 235.4 | 552.7 | 489.3 | 449.6 | 415.1 | Average of CARB \& CN2508 ${ }^{\text {a }}$ |
| Dash 9 | 1 | 16.9 | 88.4 | 62.1 | 140.2 | 259.5 | 342.2 | 380.4 | 443.5 | 402.7 | 570.0 | CSXT595 ${ }^{\text {b }}$ |
| Dash 9 | 2 | 7.7 | 42.0 | 69.3 | 145.8 | 259.8 | 325.7 | 363.6 | 356.7 | 379.7 | 445.1 | BNSF $7736{ }^{\text {b }}$ |
| C60-A | 0 | 71.0 | 83.9 | 68.6 | 78.6 | 237.2 | 208.9 | 247.7 | 265.5 | 168.6 | 265.7 | CARB and ENVIRON |

Notes:
a. USEPA Regulatory Support Document, "Locomotive Emissions Regulation," Appendix B, 12/17/97, as tabulated by CARB and ENVIRON.
b. Base emission rates provided by ENVIRON as part of the BNSF analyses for the Railyard MOU (Personal communication from Chris Lindhjem to R. Ireson, 2006) based on data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to C. Lindhjem, 2006).
c. SwRI final report "Emissions Measurments - Locomotives" by Steve Fritz, August 1995.
d. Manufacturers' emissions test data as tabulated by CARB.
e. Base SD-70 emission rates taken from data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to R. Ireson, 2006).
f. Average of manufacturer's emissions test data as tabulated by CARB and data from the AAR/SwRI Exhaust Plume Study, tabulated and calculated by ENVIRON.

Table 15
Locomotive Diesel Particulate Matter Emission Factors (g/hr) Adjusted for Fuel Sulfur Content of 2,639 PPM

Colton Rail Yard

| Model Group | Tier | Throttle Setting |  |  |  |  |  |  |  |  |  | Source ${ }^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Idle | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |  |
| Switchers | N | 31.0 | 56.0 | 23.0 | 76.0 | 136.9 | 156.6 | 197.4 | 303.4 | 341.2 | 442.9 | CARB and ENVIRON |
| GP-3x | N | 38.0 | 72.0 | 31.0 | 110.0 | 184.5 | 208.8 | 262.2 | 410.8 | 457.9 | 601.1 | CARB and ENVIRON |
| GP-4x | N | 47.9 | 80.0 | 35.7 | 134.3 | 224.5 | 254.6 | 330.0 | 543.7 | 631.6 | 812.1 | CARB and ENVIRON |
| GP-50 | N | 26.0 | 64.1 | 51.3 | 142.5 | 299.0 | 306.5 | 386.9 | 653.9 | 717.3 | 917.4 | CARB and ENVIRON |
| GP-60 | N | 48.6 | 98.5 | 48.7 | 131.7 | 282.1 | 294.9 | 368.5 | 636.1 | 735.4 | 931.0 | CARB and ENVIRON |
| GP-60 | 0 | 21.1 | 25.4 | 37.6 | 75.5 | 237.4 | 346.9 | 508.5 | 714.0 | 1113.4 | 1304.9 | KCS7332 |
| SD-7x | N | 24.0 | 4.8 | 41.0 | 65.7 | 155.5 | 239.4 | 315.4 | 369.2 | 469.9 | 582.6 | CARB and ENVIRON |
| SD-7x | 0 | 14.8 | 15.1 | 36.8 | 61.1 | 228.5 | 374.1 | 442.7 | 853.3 | 1007.8 | 1093.2 | CARB and ENVIRON |
| SD-7x | 1 | 29.2 | 31.8 | 37.1 | 66.2 | 217.5 | 291.5 | 428.9 | 702.6 | 774.5 | 838.1 | NS2630 ${ }^{\text {c }}$ |
| SD-7x | 2 | 55.4 | 59.5 | 38.3 | 134.2 | 269.4 | 295.9 | 329.2 | 543.3 | 664.6 | 696.2 | UP8353 ${ }^{\text {c }}$ |
| SD-90 | 0 | 61.1 | 108.5 | 50.1 | 99.1 | 253.7 | 417.3 | 551.5 | 324.4 | 255.3 | 923.1 | EMD 16V265H |
| Dash 7 | N | 65.0 | 180.5 | 108.2 | 121.2 | 352.7 | 323.1 | 327.1 | 293.7 | 325.3 | 405.4 | CARB and ENVIRON |
| Dash 8 | 0 | 37.0 | 147.5 | 86.0 | 133.1 | 285.9 | 289.1 | 323.3 | 366.4 | 453.5 | 593.8 | CARB and ENVIRON |
| Dash 9 | N | 32.1 | 53.9 | 54.2 | 108.1 | 215.7 | 285.1 | 365.6 | 429.3 | 469.7 | 681.2 | SWRI 2000 |
| Dash 9 | 0 | 33.8 | 50.7 | 56.1 | 117.4 | 224.9 | 260.1 | 607.7 | 562.9 | 587.4 | 546.9 | Average of CARB \& CN2508 ${ }^{\text {a }}$ |
| Dash 9 | 1 | 16.9 | 88.4 | 62.1 | 140.2 | 298.2 | 378.1 | 418.3 | 510.2 | 526.2 | 751.1 | CSXT595 ${ }^{\text {b }}$ |
| Dash 9 | 2 | 7.7 | 42.0 | 69.3 | 145.8 | 298.5 | 359.9 | 399.8 | 410.4 | 496.1 | 586.4 | BNSF $7736{ }^{\text {b }}$ |
| C60-A | 0 | 71.0 | 83.9 | 68.6 | 78.6 | 272.6 | 230.8 | 272.3 | 305.4 | 220.3 | 350.1 | CARB and ENVIRON |

Notes:

1. USEPA Regulatory Support Document, "Locomotive Emissions Regulation," Appendix B, 12/17/97, as tabulated by CARB and ENVIRON.
2. Base emission rates provided by ENVIRON as part of the BNSF analyses for the Railyard MOU (Personal communication from Chris Lindhjem to R. Ireson, 2006) based on data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to C. Lindhjem, 2006).
3. SwRI final report "Emissions Measurments - Locomotives" by Steve Fritz, August 1995.
4. Manufacturers' emissions test data as tabulated by CARB.
5. Base SD-70 emission rates taken from data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to R. Ireson, 2006).
6. Average of manufacturer's emissions test data as tabulated by CARB and data from the AAR/SwRI Exhaust Plume Study, tabulated and calculated by ENVIRON.

## 2. Diesel-Fueled Trucks (Yard Trucks)

Emission estimates for the Diesel-fueled Yard trucks are based on the vehicle class, vehicle model year, annual VMT within the Yard, and amount of time the vehicles spend idling. Vehicle-specific emission factors, calculated using the EMFAC2007 model, are shown in Table 16. Per CARB guidelines, the emissions from idling and traveling modes have been separated because different source treatments (point or volume sources) will be used in the air dispersion modeling analysis for these modes. Detailed emission factor derivation calculations and EMFAC2007 output are contained in Appendix B.

## 3. HHD Diesel-Fueled Delivery Trucks

Emission factors for the HHD Diesel-fueled delivery trucks were obtained from CARB's EMFAC2007 model. Per CARB guidelines, the emissions from idling and traveling modes have been separated because different source treatments (point or volume sources) will be used in the air dispersion modeling analysis for these modes. A fleet average emission factor for traveling exhaust emissions was calculated using the EMFAC2007 model with the BURDEN output option. Since the fleet distribution is not known, the EMFAC2007 default distribution for Los Angeles County was used. Idling emission factors were calculated using the EMFAC2007 model with the EMFAC output option. The emission factors for the HHD Diesel-fueled trucks are shown in Table 17. Detailed emission factor derivation calculations and the EMFAC2007 output are contained in Appendix C.

## 4. Heavy Equipment

Emission factors for heavy equipment were calculated using OFFROAD2007 model. The emission factors for heavy equipment are shown in Table 18. Detailed emission factor derivation calculations and OFFROAD2007 output are contained in Appendix D.

## Table 16

## Emission Factors for Diesel-Fueled Yard Trucks

Colton Rail Yard

| Owner/ID | Make/Model | Model Year | Vehicle Class | Traveling Emission Factors$(\mathrm{g} / \mathrm{mi})^{\mathrm{a}}$ |  |  |  |  | Idling Emissions Factors$(\mathrm{g} / \mathrm{hr})^{\mathrm{a}, \mathrm{~b}}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | ROG | CO | NOx | DPM | SOx | ROG | CO | NOx | DPM | SOx |
| 69496 | Chevy CK 3500 | 1998 | LDT | 0.12 | 1.13 | 1.60 | 0.06 | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 69499 | Chevy CK 3500 | 1998 | LDT | 0.12 | 1.13 | 1.60 | 0.06 | 0.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1915-73119 | Ford F-450 | 2003 | LHDT1 | 0.33 | 1.70 | 6.70 | 0.08 | 0.04 | 3.17 | 26.30 | 75.05 | 0.75 | 0.34 |
| 9007 E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 0.16 | 3.17 | 26.30 | 75.05 | 1.40 | 0.34 |
| 9009 E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 0.16 | 3.17 | 26.30 | 75.05 | 1.40 | 0.34 |
| 9031E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 0.16 | 3.17 | 26.30 | 75.05 | 1.40 | 0.34 |
| 9018E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 0.16 | 3.17 | 26.30 | 75.05 | 1.40 | 0.34 |
| Unknown | International | 1987 | HHD | 12.31 | 41.26 | 31.86 | 5.72 | 0.22 | 22.84 | 61.55 | 82.94 | 4.28 | 0.55 |
| 64274 | Ford LT8000 | 1989 | HHD | 12.06 | 40.31 | 31.60 | 5.42 | 0.24 | 19.45 | 58.49 | 85.53 | 3.43 | 0.55 |
| 1915-9038E | Ford LT9000 | 1997 | HHD | 6.92 | 16.99 | 31.05 | 2.26 | 0.24 | 12.41 | 49.53 | 110.27 | 1.93 | 0.55 |

Notes:
a. Emission factors calculated using the EMFAC2007 model with the BURDEN output options.
b. Idling emission factors calculated using the EMFAC2007 model with the EMFAC output option.
c. See Table 2 for vehicle specifications.
d. Diesel $\mathrm{PM}_{10}$ (DPM) is a TAC.

| Table 17 <br> Emission Factors for HHD Diesel-Fueled Delivery Trucks ${ }^{\text {a }}$ Colton Rail Yard |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Mode | Fleet Average Emission Factors |  |  |  |  |
|  | ROG | CO | NOx | $\mathrm{DPM}^{\text {d }}$ | SOx |
| Traveling (g/mi) ${ }^{\text {b }}$ | 6.40 | 17.23 | 28.68 | 2.47 | 0.2 |
| Idling (g/hr) ${ }^{\text {c }}$ | 16.16 | 52.99 | 100.38 | 2.85 | 0.5 |
| Notes: <br> a. See Part V for vehicle specifications. <br> b. Emission factors calculated using the EMFAC2007 model with the BURDEN output option. The default fleet distribution for Los Angeles County was used. <br> c. Emission factors calculated using the EMFAC2007 model with the EMFAC output option. The default fleet distribution for Los Angeles County was used. <br> d. Diesel $\mathrm{PM}_{10}(\mathrm{DPM})$ is a TAC. |  |  |  |  |  |


| Table 18 <br> Emission Factors for Heavy Equipment Colton Rail Yard |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equipment | Make/Model | Model Year | Emission Factors (g/hp-hr) ${ }^{\text {a }}$ |  |  |  |  |
| Type |  |  | ROG ${ }^{\text {b }}$ | CO | NOx | DPM | SOx |
| Rail Cleaner | Unknown | 2003 | 0.52 | 2.96 | 5.32 | 0.25 | 0.06 |
| Rerailer | Cline | 1987 | 1.64 | 5.52 | 13.04 | 0.77 | 0.06 |
| Crane | Lorain LRT-250 | 1997 | 1.27 | 3.55 | 8.35 | 0.58 | 0.06 |
| Forklift | Toyota 6EDU45 | 1999 | 1.85 | 4.60 | 8.36 | 1.06 | 0.06 |
| Notes: <br> a. Emission factors from the OFFROAD2007 model. <br> b. Evaporative emissions for these sources are negligible. |  |  |  |  |  |  |  |

## 5. Tanks

VOC emissions from the non-exempt storage tanks were calculated using USEPA's TANKS program. CARB's speciation database was used to determine the fraction of each TAC in the total VOC emissions from each gasoline storage tank. All TACs listed in the most recent version of the Emission Inventory Criteria and Guidelines Report for the Air Toxics "Hot Spots" Program were included. The TAC emission factors for gasoline storage are shown in Table 19. The TANKS output and the relevant sections of CARB's speciation database are included in Appendix E.

| Table 19 <br> TAC Emission Factors for Gasoline Storage Tank Colton Rail Yard |  |  |
| :---: | :---: | :---: |
| CAS | Chemical Name ${ }^{\text {b }}$ | Organic Fraction of VOC (by weight) ${ }^{\text {a }}$ |
| 540841 | 2,2,4-trimethylpentane | 0.0129 |
| 71432 | Benzene | 0.0036 |
| 110827 | Cyclohexane | 0.0103 |
| 100414 | Ethylbenzene | 0.0012 |
| 78784 | Isopentane | 0.3734 |
| 98828 | Isopropylbenzene (cumene) | 0.0001 |
| 108383 | m-Xylene | 0.0034 |
| 110543 | n-Hexane | 0.0154 |
| 95476 | o-Xylene | 0.0013 |
| 106423 | p-Xylene | 0.0011 |
| 108883 | Toluene | 0.0170 |
| Total |  | 0.44 |
| Notes: <br> a. The organic fraction information is from CARB's speciation database. Data are from the "Headspace vapors 1996 SSD etoh $2.0 \%$ (MTBE phaseout)" option. <br> b. Emissions were calculated only for chemicals that were in both CARB's speciation database and the AB2588 list. |  |  |

## 6. Sand Tower

Emission factors for the sand tower operations are from USEPA's AP-42 document. The sand transfer system consists of two parts: pneumatic transfer and gravity transfer. The pneumatic transfer system is similar to those used to unload cement at concrete batch plants. The gravity feed system is similar to the sand and aggregate transfer operations at concrete batch plants. Therefore, emissions will be calculated using the AP-42 emission factors for concrete batch plants. As previously discussed, the system is equipped with a baghouse; therefore, emission factors for a controlled system were used. These emission factors are shown in Table 20.

\left.| Emission Factors for Sand Tower Operations |  |  |
| :--- | :---: | :---: |
| Colton Rail Yard |  |  |$\right]$. Emission Factors (lb/ton)

Notes:
a. There are no TAC emissions from this source.
b. Emission factor from AP-42, Table 11.12-5, 6/06. Factor for controlled pneumatic cement unloading to elevated storage silo was used. The unit is equipped with a fabric filter.
c. Emission factor from AP-42, Table 11.12-5, 6/06. Factor for sand transfer was used.

## 7. Wastewater Treatment Plant

Emission factors for the WWTP are from the Comprehensive Air Emission Inventory and Regulatory Analysis Report for the Colton Yard (Trinity Consultants, May 30, 2003). Emission rates were calculated by Trinity Consultants using USEPA's WATER9 program. The emission rates are shown in Table 21.

| Emission Factors for the Wastewater Treatment Plant <br> Colton Rail Yard |  |
| :--- | :---: |
| Pollutant | Emission Rate $(\mathrm{grams} / \mathrm{sec})^{\mathrm{a}}$ |
| Benzene | $3.16 \times 10^{-6}$ |
| Bromomethane | $1.21 \times 10^{-5}$ |
| Chloroform | $6.18 \times 10^{-6}$ |
| Ethylbenzene | $1.96 \times 10^{-5}$ |
| Methylene Chloride | $1.08 \times 10^{-4}$ |
| Toluene | $4.34 \times 10^{-5}$ |
| Xylene | $7.80 \times 10^{-5}$ |
| Total | $\mathbf{2 . 7 0 \times 1 0} \mathbf{1 0}$ |
| Notes: <br> a. Emission rates from Comprehensive Air Emission <br> Yard, Trinity Consultants, May 30, 2003. |  |

## 8. Emergency Generator

Emission factors for the emergency generator are from AP-42, Table 3.3.-1 (10/96). The emission factors are shown in Table 22.

| Table 22 <br> Emission Factors for the Diesel-Fueled Emergency Generator Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Emission Factors (g/hp-hr) ${ }^{\text {a }}$ |  |  |  |  |
| ROG | CO | NOx | $\mathrm{DPM}^{\text {b }}$ | SOx |
| 1.14 | 3.03 | 14.06 | 1.00 | 0.93 |
| Notes: <br> a. Emission factors from AP-42, Table 3.3-1, 10/96. <br> b. Diesel $\mathrm{PM}_{10}(\mathrm{DPM})$ is a TAC. |  |  |  |  |

## B. TAC Emissions by Source Type

TAC emission calculations for each source type were based on the site-specific equipment inventory (shown in Part V of this report), equipment activity data (shown in Part VI of this report), and the source-specific emission factors shown in Part VII.A above. As discussed above, there are no TAC emissions from the sand tower. Detailed emission calculations for each source group are contained in Appendix F.

## 1. Locomotives

Emissions from locomotive operations were based on the emission factors shown in Tables 14 and 15 , the number of events, the number of locomotives per consist, duration, and duty cycle of different types of activity. Table 23 shows the duty cycles assumed for different types of activities.

For locomotive models and tiers for which specific emission factors were not available, the emissions for the next lower tier were used, or the next higher tier if no lower tier data were available. Emission factors for the "average locomotive" for different types of activity were developed from the emission factors and the actual locomotive model and technology distributions for that activity. Separate distributions were developed for the following types of activity: through trains (including through power moves); westbound

| Locomotive Duty Cycles <br> Colton Rail Yard |  |
| :--- | :---: |
| Activity | Duty Cycle |
| Through Train Movement | $\mathrm{N} 2-100 \%$ |
| Movements within the Yard | $\mathrm{N} 1-50 \%, \mathrm{~N} 2-50 \%$ |
| Hump Set Pushing | $\mathrm{N} 2-2 \mathrm{hrs} /$ day, DB ${ }^{\text {a }}-11 \mathrm{hrs} / \mathrm{day}$ |
| Hump Set Movement from Hump to <br> West End of the Receiving Yard | $\mathrm{N} 1-50 \%, \mathrm{~N} 2-50 \%$ |
| Trim Set Operations | USEPA Switch Duty Cycle ${ }^{\text {b }}$ |
| Notes: <br> a. DB (Dynamic braking) is a throttle setting available on medium- and high-horsepower locomotives in <br> which the coils on the traction motors are energized to effectively turn them into electrical generators, <br> similat to downshifting to provide engine braking in a car. The electricity generated is dissipated by <br> resistance grids on top of the locomotives. The track through the Receiving Yard to the Hump at Colton <br> has a slight downgrade, and braking is needed to maintain the slow speeds necessary for safe decoupling <br> and routing of individual cars into the Bowl. <br> b. USEPA (1998) Regulatory Support Document |  |

terminating freight trains and eastbound originating freight trains; eastbound terminating freight trains, westbound originating freight trains, and local trains; arriving and departing power moves; hump and trim sets (yard operations); locomotives in the Service Track; and locomotives undergoing load tests. Table 24 shows the DPM emission estimates for the different types of activities.

| Table 24 <br> DPM Emissions from Locomotives <br> Colton Rail Yard |  |
| :--- | :---: |
| Activity | DPM Emissions (tpy) |
| Through Trains and Power Moves | 0.51 |
| Freight Trains | 2.45 |
| Local Trains | 0.47 |
| Power Moves in Yard | 0.14 |
| Hump Operations | 4.74 |
| Trim Operations | 5.28 |
| Crew Changes | 0.07 |
| Service Movements | 0.06 |
| Service Idling | 2.14 |
| Load Testing | 0.44 |
| Total | $\mathbf{1 6 . 3 0}$ |
| Notes: <br> a. See Table 1 for equipment specifications. <br> b. See Tables 8 and 9 for activity data. <br> c. <br> d. See Tables 14 and 15 for emission factors. |  |
| d. Emissions from Yard operations are based on 12 switcher locomotives operating 23 hours per day each. |  |
| The switcher specific duty cycles are discussed in Part VII.A.1. |  |
| e. See Appendices A-3 and A-4 for detailed emission calculations. The calculations of sulfur adjustments |  |
| are shown in Appendix A-7. |  |

## 2. Diesel-Fueled Trucks (Yard Trucks)

Emission estimates for Diesel-fueled Yard trucks are based on vehicle class, vehicle model year, annual VMT within the Yard, and amount of time the vehicles spend idling.

Table 25 shows the DPM emission estimates for Diesel-fueled Yard trucks operating at Colton in 2005.

| DPM Emissions from Diesel-Fueled Yard Trucks <br> Colton Rail Yard |  |  |  |
| :--- | :---: | :---: | :---: |
| Pollutant | Emissions (tpy) |  |  |
|  | Traveling Mode | Idling Mode | Total |
|  | 0.19 | 0.002 | 0.19 |
| Notes: |  |  |  |
| a. See Table 2 for equipment specifications. |  |  |  |
| b. See Table 10 for activity data. |  |  |  |
| c. See Table 16 for emission factors. |  |  |  |

## 3. HHD Diesel-Fueled Delivery Trucks

DPM emission estimates for the HHD Diesel-fueled delivery trucks are based on the number of truck trips, the annual VMT within the Yard, and the amount of idling time. Table 26 shows the DPM emission estimates for the Diesel-fueled HHD trucks operating at the Yard in 2005.

| Table 26 <br> DPM Emissions from HHD Diesel-Fueled Delivery Trucks Colton Rail Yard |  |  |  |
| :---: | :---: | :---: | :---: |
|  | DPM Emissions (tpy) ${ }^{\text {a }}$ |  |  |
| Pollutant | Traveling Mode | Idling Mode | Total |
| DPM | 0.000 | 0.000 | 0.000 |
| Notes: <br> a. Due to the small number of deliveries and limited VMT, emissions from HHD Diesel-fueled delivery trucks are negligible. <br> b. See Part V for equipment specifications. <br> c. See Table 11 for activity data. <br> d. See Table 17 for emission factors. |  |  |  |

## 4. Heavy Equipment

Emission estimates for the heavy equipment are based on the number and type of equipment, the equipment model, and the hours of operation. Table 27 shows the DPM emission estimates for the Diesel-fueled heavy equipment operating at Colton in 2005.

| Table 27 <br> DPM Emissions from Heavy Equipment <br> Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment <br> Type | Make/Model | Model <br> Year | No of <br> Units | DPM Emissions <br> (tpy) |
| Rail Cleaner | Unknown | 2003 | 1 | 0.00 |
| Rerailer | Cline | 1987 | 1 | 0.03 |
| Crane | Lorain LRT-250 | 1997 | 1 | 0.01 |
| Forklift | Toyota 6EDU45 | 1999 | 1 | 0.01 |
| Total |  | $\mathbf{4}$ | $\mathbf{0 . 0 5}$ |  |
| Notes: <br> a. See Table 3 for equipment specifications. <br> b. See Table 12 for activity data. <br> c. See Table 18 for emission factors. |  |  |  |  |

## 5. Tanks

TAC emissions from the gasoline storage tanks were calculated using USEPA's TANKS program and CARB's speciation database. The TAC emissions for each gasoline storage tank at Colton are shown in Table 28.

## 6. Sand Tower

As previously discussed, there are no TAC emissions from the sand tower operations. $\mathrm{PM}_{10}$ emission estimates from the sand tower are shown in Appendix F.

## 7. Wastewater Treatment Plant

TAC emission estimates for the WWTP are based on emission rates from the Comprehensive Air Emission Inventory and Regulatory Analysis Report for the Colton Yard (Trinity Consultants, May 30, 2003) and the annual wastewater flow rate. Table 29 shows the TAC emissions from Colton WWTP during 2005.

| Table 28 <br> TAC Emissions from Gasoline Storage Tanks Colton Rail Yard |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CAS | Chemical Name | TAC Emissions (tpy) |  |  |  |  |
|  |  | Tank 1172 | Tank 1187 | Tank 1189 | Tank 1498 | Total |
| 540841 | 2,2,4-trimethylpentane | $1.29 \times 10^{-3}$ | $1.52 \times 10^{-3}$ | $1.55 \times 10^{-3}$ | $1.46 \times 10^{-3}$ | $5.81 \times 10^{-3}$ |
| 71432 | Benzene | $3.59 \times 10^{-4}$ | $4.22 \times 10^{-4}$ | $4.31 \times 10^{-4}$ | $4.05 \times 10^{-4}$ | $1.62 \times 10^{-3}$ |
| 110827 | Cyclohexane | $1.02 \times 10^{-3}$ | $1.20 \times 10^{-3}$ | $1.23 \times 10^{-3}$ | $1.16 \times 10^{-3}$ | $4.62 \times 10^{-3}$ |
| 100414 | Ethylbenzene | $1.18 \times 10^{-4}$ | $1.38 \times 10^{-4}$ | $1.41 \times 10^{-4}$ | $1.33 \times 10^{-4}$ | $5.30 \times 10^{-4}$ |
| 78784 | Isopentane | $3.72 \times 10^{-2}$ | $4.37 \times 10^{-2}$ | $4.47 \times 10^{-2}$ | $4.20 \times 10^{-2}$ | $1.68 \times 10^{-1}$ |
| 98828 | Isopropylbenzene (cumene) | $1.10 \times 10^{-5}$ | $1.29 \times 10^{-5}$ | $1.32 \times 10^{-5}$ | $1.24 \times 10^{-5}$ | $4.94 \times 10^{-5}$ |
| 108383 | m-Xylene | $3.42 \times 10^{-4}$ | $4.02 \times 10^{-4}$ | $4.11 \times 10^{-4}$ | $3.86 \times 10^{-4}$ | $1.54 \times 10^{-3}$ |
| 110543 | n-Hexane | $1.54 \times 10^{-3}$ | $1.80 \times 10^{-3}$ | $1.84 \times 10^{-3}$ | $1.73 \times 10^{-3}$ | $6.92 \times 10^{-3}$ |
| 95476 | o-Xylene | $1.28 \times 10^{-4}$ | $1.50 \times 10^{-4}$ | $1.53 \times 10^{-4}$ | $1.44 \times 10^{-4}$ | $5.75 \times 10^{-4}$ |
| 106423 | p-Xylene | $1.07 \times 10^{-4}$ | $1.25 \times 10^{-4}$ | $1.28 \times 10^{-4}$ | $1.20 \times 10^{-4}$ | $4.80 \times 10^{-4}$ |
| 108883 | Toluene | $1.70 \times 10^{-3}$ | $1.99 \times 10^{-3}$ | $2.04 \times 10^{-3}$ | $1.91 \times 10^{-3}$ | $7.64 \times 10^{-3}$ |
| Total |  | $4.38 \times 10^{-2}$ | $5.15 \times 10^{-2}$ | $5.26 \times 10^{-2}$ | $4.95 \times 10^{-2}$ | $1.97 \times 10^{-1}$ |
| Notes: <br> a. See Table 4 for equipment specifications. <br> b. See Table 13 for activity data. <br> c. See Table 19 for emission factors. |  |  |  |  |  |  |


| Table 29 <br> TAC Emissions from the Wastewater Treatment Plant <br> Colton Rail Yard |  |
| :--- | :---: |
| Pollutant | Emissions (tpy) |
| Benzene | $1.68 \times 10^{-4}$ |
| Bromomethane | $6.41 \times 10^{-4}$ |
| Chloroform | $3.28 \times 10^{-4}$ |
| Ethylbenzene | $1.04 \times 10^{-3}$ |
| Methylene Chloride | $5.72 \times 10^{-3}$ |
| Toluene | $2.31 \times 10^{-3}$ |
| Xylene | $4.14 \times 10^{-3}$ |
| Total | $\mathbf{1 . 4 3 \times 1 0 ^ { - 2 }}$ |
| Notes: <br> a. See Part V for equipment description. <br> b. See Part VI for activity data. <br> c. See Table 21 for emission factors. |  |

## 8. Emergency Generator

Emission estimates for the emergency generator are based on the size of the unit and the hours of operation. Table 30 shows the DPM emission estimates for the Diesel-fueled emergency generator operating at the Yard in 2005.

| Table 30 <br> DPM Emissions from the Emergency Generator <br> Colton Rail Yard |  |
| :--- | :---: |
| Equipment Type/Location |  |
| Emergency Generator - Bowl Area |  |
| Notes: |  |
| a. See Part V for equipment specifications. |  |
| b. See Part VI for activity data. |  |
| c. See Table 22 for emissions (tpy/yr) factors. |  |

## C. Facility Total Emissions

Facility-wide DPM emissions are shown in Table 31. Facility-wide TAC emissions, excluding DPM, are shown in Table 32.

| Table 31 <br> Facility-Wide Diesel Particulate Emissions Colton Rail Yard |  |
| :---: | :---: |
| Source | Emissions (tpy) |
| Locomotives ${ }^{\text {a }}$ | 16.30 |
| Diesel-Fueled Yard Trucks ${ }^{\text {b }}$ | 0.19 |
| HHD Diesel-Fueled Delivery Trucks ${ }^{\text {c }}$ | 0.00 |
| Heavy Equipment ${ }^{\text {d }}$ | 0.05 |
| Emergency Generator ${ }^{\text {e }}$ | 0.001 |
| Total | 16.54 |
| Notes: <br> a. See Table 24. <br> b. See Table 25. <br> c. See Table 26. <br> d. See Table 27. <br> e. See Table 30. |  |

Table 32
Facility-Wide TAC Emissions (excluding DPM) Colton Rail Yard

| CAS | Chemical Name | Emissions (tpy) $_{$$}$ |  |  |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $5.81 \times 10^{-3}$ | - | $5.81 \times 10^{-3}$ |  |  |  |  |
| 71432 | Benzene | $1.62 \times 10^{-3}$ | $1.68 \times 10^{-4}$ | $1.78 \times 10^{-3}$ |  |  |  |  |
|  | Bromomethane | - | $6.41 \times 10^{-4}$ | $6.41 \times 10^{-4}$ |  |  |  |  |
| 67663 | Chloroform | - | $3.28 \times 10^{-4}$ | $3.28 \times 10^{-4}$ |  |  |  |  |
| 110827 | Cyclohexane | $4.62 \times 10^{-3}$ | - | $4.62 \times 10^{-3}$ |  |  |  |  |
| 100414 | Ethylbenzene | $5.30 \times 10^{-4}$ | $1.04 \times 10^{-3}$ | $1.57 \times 10^{-3}$ |  |  |  |  |
| 78784 | Isopentane | $1.68 \times 10^{-1}$ | - | $1.68 \times 10^{-1}$ |  |  |  |  |
| 98828 | Isopropylbenzene (cumene) | $4.94 \times 10^{-5}$ | - | $4.94 \times 10^{-5}$ |  |  |  |  |
|  | Methylene Chloride | - | $5.72 \times 10^{-3}$ | $5.72 \times 10^{-3}$ |  |  |  |  |
| 108383 | m-Xylene | $1.54 \times 10^{-4}$ | - | $1.54 \times 10^{-3}$ |  |  |  |  |
| 110543 | n-Hexane | $6.92 \times 10^{-3}$ | - | $6.92 \times 10^{-3}$ |  |  |  |  |
| 95476 | o-Xylene | $5.75 \times 10^{-4}$ | - | $5.75 \times 10^{-4}$ |  |  |  |  |
| 106423 | p-Xylene | $4.80 \times 10^{-4}$ | - | $4.8 \times 10^{-4}$ |  |  |  |  |
| 108883 | Toluene | $7.64 \times 10^{-3}$ | $2.31 \times 10^{-3}$ | $9.95 \times 10^{-3}$ |  |  |  |  |
| 1330207 | Xylene (total) | - | $4.14 \times 10^{-3}$ | $4.14 \times 10^{-3}$ |  |  |  |  |
| Total |  |  |  |  |  | $\mathbf{1 . 9 7 \times 1 0 ^ { - 1 }}$ | $\mathbf{1 . 4 3 \times 1 0 ^ { - 2 }}$ | $2.12 \times 10^{-1}$ |

Notes:
a. See Table 28.
b. See Table 29.

## PART VIII. RISK SCREENING CALCULATIONS

As discussed in Part IV of this report and agreed upon with the CARB, de minimis sources, based on weighted health risk, were identified in the inventory, but were not included in the modeling analysis. De minimis sources are the individual source categories that represent less than $3 \%$ of the facility-total weighted-average site health impacts (determined separately for cancer risk and non-cancer chronic health hazard). Total exclusions for all de minimis sources did not exceed $10 \%$ of the facility-total weighted-average site health impacts.

The OEHHA unit risk factor for each pollutant was multiplied by the annual emissions of that pollutant to generate a risk index value for each source. Each source-specific risk index was divided by the facility total risk index to get the fractional contribution to the total risk for each source. The cancer risk, the non-cancer health hazard index, and the fractional contribution to the cancer risk and non-cancer chronic health hazard for each source are summarized in Table 33. Detailed cancer risk and non-cancer health hazard index calculations are in Appendix G.

| Table 33 <br> Summary of Weighted Risk by Source Category Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Cancer Risk |  | Non-Cancer Chronic Health Hazard |  |
| Source | Risk Index Value | Percent of Total Risk | Health Hazard Index Value | Percent of Total Hazard |
| Locomotives | $4.89 \times 10^{-3}$ | 98.54 | $8.15 \times 10^{1}$ | 56.42 |
| Diesel-Fueled Yard Trucks | $5.72 \times 10^{-5}$ | 1.15 | $9.53 \times 10^{-1}$ | 0.66 |
| HHD Diesel-Fueled Delivery Trucks | $2.49 \times 10^{-7}$ | 0.01 | $4.15 \times 10^{-3}$ | 0.00 |
| Heavy Equipment | $1.44 \times 10^{-5}$ | 0.29 | $2.41 \times 10^{-1}$ | 0.17 |
| WWTP | $1.23 \times 10^{-8}$ | 0.00 | 8.06 | 5.58 |
| Sand Tower ${ }^{\text {a }}$ | 0.00 | 0.00 | 0.00 | 0.00 |
| Gasoline Storage Tanks | $4.69 \times 10^{-8}$ | 0.00 | $5.37 \times 10^{1}$ | 37.17 |
| Emergency Generator | $3.30 \times 10^{-7}$ | 0.01 | $5.50 \times 10^{-3}$ | 0.00 |
| Total | $4.96 \times 10^{-3}$ | 100 | $1.44 \times 10^{2}$ | 100 |
| Notes: <br> a. There are no TAC emissions from the sand | tower. |  |  |  |

Sources that represent less than 3\% each of the facility-total weighted-average cancer risk and non-cancer chronic health hazard, as shown in Table 33, are de minimis. Table 34 lists the de minimis sources for the Colton Yard.

| Table 34 <br> Summary of De Minimis Sources Colton Rail Yard |  |
| :---: | :---: |
| De Minimis Sources for Cancer Risk | De Minimis Sources for Non-Cancer Chronic Health Hazard |
| Diesel-Fueled Yard Trucks <br> HHD Diesel-Fueled Delivery Trucks <br> Heavy Equipment <br> WWTP <br> Sand Tower <br> Gasoline Storage Tanks <br> Emergency Generator | Diesel-Fueled Yard Trucks <br> HHD Diesel-Fueled Delivery Trucks <br> Heavy Equipment <br> Sand Tower <br> Emergency Generator |

Sources that are de minimis for both cancer risk and non-cancer chronic health hazard (i.e., yard trucks, delivery trucks, heavy equipment, and emergency generator) are not included in the dispersion modeling analysis. At the request of CARB, heavy equipment was included in the dispersion modeling analysis, notwithstanding its de minimis risk contribution.

## PART IX. $\underline{\text { AIR DISPERSION MODELING }}$

An air dispersion modeling analysis was conducted for the Colton Yard. The purpose of the analysis was to estimate ground-level concentrations of DPM and other TACs, emitted from Yard operations, at receptor locations near the Yard. Air dispersion modeling was conducted in accordance with the Health Risk Assessment Guidance for Rail Yard and Intermodal Facilities (July 2006) and UPRR's Modeling Protocol (August 2006). Each aspect of the modeling is further described below.

## A. Model Selection and Preparation

## 1. Modeled Sources and Source Treatment

As discussed in Part VIII, only sources that represent more than 3\% of the facility-total weighted-average site health impacts (determined separately for cancer risk and noncancer chronic health hazard) were included in the dispersion modeling analysis. At the request of CARB, heavy equipment was included as well, notwithstanding its de minimis risk contribution. Emissions from mobile sources, heavy equipment, and moving locomotives were simulated as a series of volume sources along their corresponding travel routes and work areas. Idling and load testing of locomotives were simulated as a series of point sources within the areas where these events occur. The elevation for each source was interpolated from a 50 m grid of USGS terrain elevations. Table 35 shows the sources that were included in the modeling analysis and treatment used for each source. Assumptions used to spatially allocate emissions from locomotive operations within the Yard are included in Appendix A-4. Assumptions used to spatially allocate emissions from non-locomotive sources are contained in Appendix H. Figures 3 through 5 show how each source was located in the Yard for the dispersion modeling analysis.

| Source Treatment for Air Dispersion Modeling <br> Colton Rail Yard |  |
| :--- | :---: |
| Source | Source Treatment |
| Gasoline Storage Tanks | Point |
| WWTP | Point |
| Locomotives (idling and load testing) | Point |
| Locomotives (traveling) | Volume |
| Heavy Equipment (idling) | Volume |
| Heavy Equipment (traveling) | Volume |
| Notes: <br> a. See Figures 3 through 5 for source locations. |  |

## 2. Model Selection

Selection of air dispersion models depends on many factors, including the type of emissions source (point, line, or volume) and type of terrain surrounding the emission source. The USEPA-approved guideline air dispersion model, AERMOD, was selected for this project. AERMOD is recommended by the USEPA as the preferred air dispersion model, and is the recommended model in the CARB's Health Risk Assessment Guidance for Rail Yard and Intermodal Facilities (July 2006).

AERMOD is a steady-state, ${ }^{11}$ multiple-source, Gaussian dispersion model designed for use with emission sources situated in terrain where ground elevations can exceed the release heights of the emission sources (i.e., complex terrain). ${ }^{12}$ AERMOD was used with meteorological data from the Ontario International Airport. AERMOD used these parameters to select the appropriate dispersion coefficients.

Standard AERMOD control parameters were used, including stack-tip downwash, nonscreening mode, non-flat terrain, and sequential meteorological data check. Following USEPA guidance, the stack-tip downwash option adjusted the effective stack height

[^7]Figure 3
Placement of Locomotive Movements in the Dispersion Modeling Analysis Colton Rail Yard

Figure 4
Placement of Locomotive Idling in the Dispersion Modeling Analysis Colton Rail Yard

Figure 5
Placement of Switcher Locomotive and Heavy Equipment Operations in the Dispersion Modeling Analysis

Colton Rail Yard
downward following the methods of Briggs (1972) for stack exit velocities less than 1.5 times the wind speed at stack top.

Two AERMET preprocessors (Stages 1 and 2, and Stage 3) were used to prepare meteorological data for use in AERMOD. Albedo and Bowen ratio ${ }^{13}$ were estimated in multiple wind direction sectors surrounding the Yard, while surface roughness from similar sectors around the meteorological monitoring site was used in the model. This separation was based on the fact that atmospheric turbulence induced by surface roughness around the meteorological monitoring tower affects the resulting wind speed profile used by AERMOD to represent conditions at the Yard, while the albedo and Bowen ratio around the Yard are more appropriate to characterize land use conditions surrounding the area being modeled.

As suggested by the USEPA (2000), for purposes of determining albedo and Bowen ratio the surface characteristics were specified in sectors no smaller than a 30-degree arc. Specifying surface characteristics in narrower sectors becomes less meaningful because of expected wind direction variability during an hour, as well as the encroachment of characteristics from the adjacent sectors with a one-hour travel time. Use of weightedaverage ${ }^{14}$ characteristics by surface area within a 30-degree (or wider) sector made it possible to have a unique portion of the surface significantly influence the properties of the sector that it occupies. The length of the upwind fetch for defining the nature of the turbulent characteristics of the atmosphere in each sector surrounding the source location was 3 kilometers as recommended by Irwin (1978) and USEPA's Guideline on Air Quality Models. ${ }^{15}$

[^8]
## 3. Modeling Inputs

Modeling was based on the annual average emissions for each source as discussed in Part VII B above. Diurnal and/or seasonal activity scalars were applied to locomotive activities. The following profiles were used in the modeling. See Appendix A-3 for the profiles used and Appendix I for a description of the methods used to develop them.

- A seasonal/diurnal activity profile was calculated for locomotive idling based on the number of arrivals and departures in each hour of the day and the number of arriving and departing trains in each season. Each hourly factor was based on the number of arrivals and departures in that hour and the number of departures in the following hour. This approach captures the idling times for consists prior to departure. These factors were applied to consist idling for arriving and departing trains.
- A seasonal/diurnal activity profile was calculated for in-yard locomotive movements of road power using the same approach as for idling. In this case, however, only the number of arriving and departing trains in a single hour was used for that hour's factor.
- A seasonal profile was used for switching operations based on the same seasonal profile developed for train activity. No diurnal profile was used as hump and trim sets operate throughout the day.
- A seasonal profile was applied to locomotive service and load test emissions based on monthly service release data.

The volume source release heights and vertical dispersion parameters $\left(\sigma_{z}\right)$ were those used by CARB for the Truck Stop Scenario in Appendix VII of the Diesel Risk Reduction Plan for mobile vehicles and equipment other than locomotives. For locomotives, the release height and $\sigma_{z}$ values used were those developed by CARB for daytime and nighttime locomotive movements in the Roseville Risk Assessment modeling. Stack parameters used to create the AERMOD input file for locomotive operations are shown in Table 36. Table 37 summarizes the modeling inputs used to create the AERMOD input file for each non-locomotive source at the Yard.

| Table 36 Locomotive Modeling Inputs Colton Rail Yard |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Source | Point/Idling Source Parameters |  |  |  | Volume Source Parameters |  |  |
|  | Stack Height (m) | Stack Diameter (m) | Exit Velocity (m/s) | $\begin{aligned} & \text { Temp } \\ & \left({ }^{\circ} \mathrm{K}\right) \\ & \hline \end{aligned}$ | $\begin{array}{r} \sigma_{\mathrm{z}} \\ (\mathrm{~m}) \\ \hline \end{array}$ | $\begin{gathered} \sigma_{\mathrm{y}}{ }^{\mathrm{a}} \\ (\mathrm{~m}) \\ \hline \end{gathered}$ | Release Height (m) |
| Locomotives (idling and load tests) ${ }^{\text {a }}$ |  |  |  |  |  |  |  |
| Road power at all yards-SD7x ${ }^{\text {b }}$ | 4.6 | 0.625 | 3.1 | 364 | - | - | - |
| Load tests - $\mathrm{N}^{\text {c }}$ | 4.6 | 0.625 | 8.0 | 420 | - | - | - |
| Load tests - $\mathrm{N} 8^{\text {c }}$ | 4.6 | 0.625 | 36.6 | 589 | - | - | - |
| Yard locomotives | 4.6 | 0.305 | 7.5 | 342 | - | - | - |
| Locomotives (traveling) ${ }^{\text {d }}$ |  |  |  |  |  |  |  |
| Day ${ }^{\text {e }}$ | - | - | - | - | 2.6 | 20-50 | 5.6 |
| Night ${ }^{\text {e }}$ | - | - | - | - | 6.79 | 20-50 | 14.6 |
| Notes: <br> a. Stack parameters for stationary locomotives were taken from the CARB Roseville modeling analysis. <br> b. Idling road power stack parameters are those of the most prevalent locomotive model (SD-7x). <br> c. Load test stack parameters are those of the most prevalent locomotive model (SD-7x). <br> d. All locomotive movements for road power and yard locomotives while working are the day and night volume source parameters for moving locomotives from the CARB Roseville modeling analysis. <br> e. Lateral dispersion coefficient $\left(\sigma_{y}\right)$ for moving locomotive volume sources was set to values between 20 and 50 m , depending on the spacing of sources in different areas of the Yard and proximity to Yard boundaries. |  |  |  |  |  |  |  |


| Table 37 <br> Non-Locomotive Modeling Inputs Colton Rail Yard |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Point/Idling Source Parameters |  |  |  | Volume Source Parameters |  |  |
| Source | Stack Height (m) | Stack Diameter $(\mathrm{m})$ | $\begin{gathered} \text { Exit Velocity } \\ (\mathrm{m} / \mathrm{s}) \end{gathered}$ | $\begin{aligned} & \text { Temp } \\ & \left({ }^{\circ} \mathrm{K}\right) \\ & \hline \hline \end{aligned}$ | $\begin{array}{r} \sigma_{\mathrm{z}} \\ (\mathrm{~m}) \\ \hline \hline \end{array}$ | $\begin{gathered} \sigma_{\mathrm{y}}{ }^{\mathrm{b}} \\ (\mathrm{~m}) \end{gathered}$ | Release Height (m) |
| Rerailer ${ }^{\text {a }}$ | - | - | - | - | 1.39 | 20-50 | 4.15 |
| Rail Cleaner ${ }^{\text {a }}$ | - | - | - | - | 1.39 | 20-50 | 4.15 |
| Forklifts ${ }^{\text {a }}$ |  |  |  |  | 1.39 | 20-50 | 4.15 |
| Notes: <br> a. Low-level sources treated as volume sources using the release height and vertical dispersion parameter $\left(\sigma_{z}\right)$ from the CARB Diesel Risk Reduction Plan (Sept. 13, 2000), Appendix VII, Table 2 (Truck stop scenario). <br> b. Low-level source lateral dispersion parameter $\left(\sigma_{y}\right)$ set to a value between 20 and 50 meters based on spacing between sources and proximity to the Yard. boundary. |  |  |  |  |  |  |  |

## 4. Meteorological Data Selection

The Yard does not monitor meteorological variables on site. Data from the Ontario International Airport were used for this project.

To the extent that airflow patterns are spatially variable due to elevated terrain and landsea effects near the coast, judgment was exercised to select the monitoring stations that are most representative of conditions at the Colton Yard.

Because rail yards, especially emissions from locomotives, tend to be aligned linearly along the main track routes, the directions of prevailing surface winds were important to achieve representativeness of model predictions in the near field. For longer transport distances (e.g., 1 to 10 km ), surface winds were still the primary consideration, with atmospheric stability also playing an important role. Due to the relatively low release heights and limited plume rise of rail yard sources, modeled concentrations are relatively insensitive to mixing heights, temperatures, and vertical temperature and wind profiles.

The selection of Ontario for surface winds data was largely dependent on the limited availability of data from other stations for the same years for which upper air data were available. There are four SCAQMD surface stations in the general vicinity of the Yard for which historical (1981) data are available, but only in a form useable in AERMOD's predecessor, ISCST3.

AERMET, the meteorological preprocessor for AERMOD, required at a minimum data from one surface National Weather Service (NWS) station, Ontario International Airport for the Yard, and one upper air NWS station, Miramar Marine Corps Air Station in San Diego. Missing hourly surface data from Ontario International Airport were replaced by the last previous values available in the same dataset.

Eleven years worth of meteorological data from Ontario, for years 1990 through 2000, were processed with AERMET to assure that an adequate number of years of acceptable data completeness and quality would be available for AERMOD modeling. It is expected
that year-to-year variability would not cause significant differences in the modeled health impacts, and hence there is no need to subject the full set of receptors to more than one year of meteorological data. The meteorological data from 1999 were selected for the rail yard dispersion modeling because it was one of the two years recorded after the anemometer height was adjusted, and it was the year with the most conservative (i.e., largest) distances of impact from a specified source.

## 5. Model Domain and Receptor Grids

A domain size of 20 km by 20 km and coarse receptor grid of $500 \mathrm{~m} \times 500 \mathrm{~m}$ were used for the modeling analysis. A fine grid of $50 \mathrm{~m} \times 50 \mathrm{~m}$ surrounding the Yard was used for modeling within 300 m of the fence line. A medium-fine grid of $100 \mathrm{~m} \times 100 \mathrm{~m}$ was used for receptors between 300 and 600 m of the fence line around the fine grid network, and a medium grid of $200 \mathrm{~m} \times 200 \mathrm{~m}$ was used for receptor distances between 600 and 1000 m .

All receptors were identified by UTM coordinates. United States Geological Survey (USGS) 7.5 Minute digital elevation model (DEM) data were used to identify terrain heights at each receptor. Figures 6 and 7 show the outline of the Yard, along with the coarse and fine receptor grids.

Sensitive receptors, consisting of hospitals, schools, day-care centers, and elder care facilities, within a 1-mile radius of the Yard, were identified. Table 38 lists the address, elevations, and UTM coordinates for each sensitive receptor. Figure 8 shows the outline of the Yard and the location of each sensitive receptor identified in Table 38.

| Table 38 Sensitive Receptor Locations ${ }^{\text {a }}$ Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Receptor | Address | Elevation (m) | $\begin{gathered} \hline \text { UTM-E } \\ (\mathrm{m}) \\ \hline \hline \end{gathered}$ | $\begin{gathered} \text { UTM-N } \\ (\mathrm{m}) \\ \hline \end{gathered}$ |
| Bloomington High School | 10750 Laurel Ave, Bloomington, CA 92316 | 323.7 | 461799 | 3768829 |
| Bloomington Middle School | 18829 Orange St, Bloomington, CA 92316 | 326.4 | 463706 | 3769419 |
| Citrus High School | 9820 Citrus Ave., Fontana, CA 92335 | 343.5 | 458274 | 3770556 |
| Colton Community Day School | 10435 Cedar Ave., Bloomington, CA 92316 | 329.2 | 463431 | 3769425 |
| Colton High School | 777 West Valley Blvd., Colton, CA 92324 | 306.9 | 469039 | 3769820 |
| Colton Middle School | 670 West Laurel St., Colton, CA 92324 | 321.0 | 469217 | 3771020 |
| Crestmore Elementary School | 18870 Jurupa Ave, Bloomington, CA 92316 | 307.2 | 463807 | 3767822 |
| Cypress Elementary School | 9751 Cypress Ave., Fontana, CA 92335 | 349.6 | 459139 | 3770700 |
| Ernest Garcia Elementary School | 1390 W. Randall Ave., Colton, CA 92324 | 338.6 | 467938 | 3771442 |
| Gerald A. Smith Elementary School | 9551 Linden Ave, Bloomington, CA 92316 | 349.9 | 463033 | 3771049 |
| Harry S. Truman Middle School | 16224 Mallory Dr., Fontana, CA 92334 | 344.7 | 458487 | 3770559 |
| Jurupa Hills Elementary School | 10755 Oleander Ave., Fontana, CA 92337 | 324.9 | 458780 | 3768832 |
| Mary B. Lewis Elementary School | 18040 San Bernardino Ave, Bloomington, CA 92316 | 350.5 | 462124 | 3770855 |
| Palmetto Elementary School | 9325 Palmetto Ave., Fontana, CA 92335 | 361.2 | 460618 | 3771454 |
| Paul Rogers Elementary School | 955 West Laurel St., Colton, CA 92324 | 327.1 | 468560 | 3771244 |
| Randall Pepper Elementary School | 16613 Randall Ave., Fontana, CA 92335 | 360.3 | 459306 | 3771456 |
| Ruth Grimes Elementary School | 1609 S Spruce Ave, Bloomington, CA 92316 | 332.2 | 464270 | 3770132 |
| Ruth O. Harris Middle School | 11150 Alder Ave., Bloomington, CA 92316 | 318.2 | 461391 | 3768017 |
| Samuel W. Simpson Elementary School | 1050 S Lilac Ave, Rialto, CA 92376 | 343.5 | 465023 | 3771246 |
| Slover Mountain High | 325 Hermosa Ave, Colton, CA 92324 | 318.8 | 468192 | 3770021 |
| Sycamore Hills Elementary School | 11036 Mahogany Dr., Fontana, CA 92337 | 322.5 | 460680 | 3768216 |
| Ulysses Grant Elementary School | 550 West Olive St., Colton, CA 92324 | 314.6 | 469420 | 3770611 |
| Walter Zimmerman Elementary School | 11050 Linden Ave, Bloomington, CA 92316 | 314.2 | 463001 | 3768224 |
| William G. Jehue Middle School | 1500 N Eucalyptus Ave, Colton, CA 92324 | 347.5 | 466847 | 3771442 |
| Woodrow Wilson Elementary School | 750 South Eighth St., Colton, CA 92324 | 288.0 | 469827 | 3768658 |
| Bell Daycare | 18302 Marygold Ave, Bloomington, CA 92316 | 344.7 | 462632 | 3770447 |
| Bloomington Christian Pre-School | 9904 Bloomington Ave, Bloomington, CA 92316 | 340.2 | 463805 | 3770438 |


| Table 38 <br> Sensitive Receptor Locations ${ }^{\text {a }}$ Colton Rail Yard |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Receptor | Address | Elevation (m) | $\begin{gathered} \hline \text { UTM-E } \\ (\mathrm{m}) \\ \hline \hline \end{gathered}$ | $\begin{gathered} \hline \text { UTM-N } \\ (\mathrm{m}) \\ \hline \hline \end{gathered}$ |
| Ezzell Family Child Care | 10701 Cedar Ave, Bloomington, CA 92316 | 324.3 | 463422 | 3769010 |
| Little Angels | 18584 Valley Blvd, Bloomington, CA 92316 | 337.4 | 463210 | 3770052 |
| Mulberry Child Care \& Preschl | 960 Bloomington Ave, Bloomington, CA 92316 | 341.7 | 464093 | 3770726 |
| Rialto Jack Simonson Center | 1243 S Riverside Ave, Rialto, CA 92376 | 338.0 | 465843 | 3770968 |
| Vision Family Daycare | 1844 De Anza Dr, Colton, CA 92324 | 336.2 | 467154 | 3770890 |
| Williams Family Child Care | 925 S Riverside Ave, Rialto, CA 92376 | 347.2 | 465842 | 3771594 |
| Arrowhead Regional Medical Center | 400 N Pepper Ave, Colton, CA 92324 | 326.1 | 467459 | 3770190 |
| Crestview Convalescent Hospital | 1471 S Riverside Ave, Rialto, CA 92376 | 331.0 | 465854 | 3770428 |
| Kaiser Foundation Clinic | 9961 Sierra Ave., Fontana, CA 92335 | 344.7 | 459995 | 3770193 |
| Notes: <br> a. UTM Coordinates are in Zone 11, NAD 83 |  |  |  |  |

Figure 6
Coarse Modeling Grid
Colton Rail Yard


Figure 7

## Fine Modeling Grid

## Colton Rail Yard



Figure 8

## Sensitive Receptors

## Colton Rail Yard



## 6. Dispersion Coefficients

Dispersion coefficients are used in air dispersion models to reflect the land use over which the pollutants are transported. The area surrounding the Yard was divided into sectors to characterize the albedo and Bowen ratio. The area surrounding the Ontario International Airport meteorological monitoring station was similarly divided into sectors to characterize surface roughness. These parameters were provided along with the meteorological data to the AERMET software. The resulting meteorological input file allows AERMOD to select appropriate dispersion coefficients during its simulation of air dispersion. AERMOD also provides an urban input option to use the overall size of the Standard Metropolitan Statistical Area that contains the emission source (i.e., the Yard) in accounting for the urban heat island effect on the nocturnal convective boundary layer height. If the option is not selected, AERMOD defaults to rural dispersion coefficients. If the urban option is selected, but no surface roughness is specified (not to be confused with the surface roughness parameters already specified for sectors around the meteorological monitoring station and input to AERMET), AERMOD assigns a default "urban" surface roughness of 1 meter. For the Colton Yard, AERMOD was run with the urban option. Based on CARB and USEPA guidance, ${ }^{16}$ namely "For urban areas adjacent to or near other urban areas, or part of urban corridors, the user should attempt to identify that part of the urban area that will contribute to the urban heat island plume affecting the source," the area encompassed by the county of Riverside was considered to determine the urban heat island effect on the nocturnal convective boundary layer height. Although the Colton Yard is located within San Bernardino County, the more densely populated areas upwind (to the southwest and south) of the Yard are in Riverside County, so the Riverside County population was assumed to be representative of conditions at the Yard. The population of this county is approximately $1,545,000,{ }^{17}$ and the surface roughness that characterizes this area was set to the URBANOPT default of 1 m . See Appendix J for additional discussion of this issue.

[^9]
## 7. Building Downwash

Building downwash effects were considered for the Yard. Stack-tip downwash adjusted the effective stack height downward following the methods of Briggs (1972) when the stack exit velocity was less than 1.5 times the wind speed at stack top. The locomotives are the only structures in the Yard of sufficiently large size and close enough proximity to the modeled emission sources (i.e., their own stacks) to be entered into the Building Profile Input Program (BPIP) with one set of dimensions for a "standard" locomotive ( 24.2 m . long x 4.0 m . wide x 4.6 m . high).
B. Modeling Results

The AERMOD input and output files have been provided to CARB in an electronic format.
C. Demographic Data

Demographic data files have been provided to CARB in an electronic format. See Appendix K for a description of the data.

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APPENDIX A

LOCOMOTIVE DATA

## APPENDIX A-1

LOCOMOTIVE MODEL, TIER, AND AUTO-START/STOP TECHNOLOGY FREQUENCY BY TRAIN TYPE
Locomotive Model，Tier，and Auto Start／Stop Technology Frequency by Train Type

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Locomotive Model，Tier，and Auto Start／Stop Technology Frequency by Train Type


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| 0 | 0 | $6 t$ | 0 | 0 | 0 | t | st | 0 | 0 | 0 | 0 | ${ }^{\text {sp／}}$ |  |
| 0 | $\dagger$ | st | 01 | 0 | 0 | L6 | S0t | 0 | $\dagger$ | 0 | 0 | $\mathrm{o}^{\mathbf{N}}$ | 0 －${ }^{\text {dem }}$ |
| 0 | 0 | $\tau$ | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 乙 | I | ${ }^{\mathbf{s} \boldsymbol{N}} \mathbf{N}$ |  |
| zI | 0 | 09 | IL | 0 | 2I | L | ャ9tI | $L$ | ¢91 | 9 | 0 | $\mathrm{o}^{\mathrm{N}}$ |  |
| имоияиの | V093 | ${ }_{6}{ }^{\text {Ssea }}$ | ${ }_{84 \mathrm{se}}{ }^{\text {a }}$ | L ¢seg $^{\text {a }}$ | 06GS | xLGS | 09d | 0 ¢d | $\mathrm{x} \downarrow \mathrm{d}$ ¢ | x£d | чวч！MS ILOI | ssav／lutz | Кอоןоичэд <br>  |

## APPENDIX A-2

## LOCOMOTIVE MODEL DISTRIBUTION BY TRAIN TYPE GROUPS



Dash 9



SD-7x
 0.00000
0.12653
0.00053
 0.00008 0.00000

0.00000 0.00000 | 8 |
| :--- |
| 6 |
| 6 | GP-4x

0.09673 0.00329 0.00000 0.00000
0.00000 8
8
0
0
0
0
0
0
EB Departing and WB Arriving Freight Trains

## Through Freight Trains and Through Power Moves

SD-50 0.00759 0.00000
0.00012 0.00000 0.00000 0.00000 0.00000 0.00000

GP-4x 0.07978 0.00000
0.00312 0.00312
0.00000 0.00000 0.00000 $\begin{array}{cccc}\text { Technology } & \text { ZTR/AESS } & \text { Switcher } & \text { GP-3x } \\ \text { Pre Tier } \mathbf{0} & \text { No } & 0.00000 & 0.00073\end{array}$ $\begin{array}{lll}\text { Pre Tier 0 } & \text { No } & 0.00000 \\ \text { Pre Tier 0 }\end{array}$ Pre Tier 0 Yes $\quad 0.00000$ 0.000000
0.000 0.00000 0.00000 $0.00000-0.00000$ 0.00000 0.00000

Technology ZTR/AESS Switcher GP-3x $\begin{array}{ccccc}\text { Technology } & \text { ZTR/AESS } & \text { Switcher } & \text { GP-3x } \\ \text { Pre Tier } 0 & \text { No } & 0.00008 & 0.00146\end{array}$ $\begin{array}{ll}\text { Pre Tier } 0 & \text { No } \\ \text { Pre Tier } 0 & \text { Yes }\end{array}$ $\begin{array}{cl}\text { Pre Tier } 0 & \text { Yes } \\ \text { Tier } 0 & \text { No }\end{array}$ $\begin{array}{ll}\text { No } & 0.00003 \\ \text { Yes } & 0.00006\end{array}$
es No
Yes No s
Dash 7
0.00031
0.00000
0.00000
0.00000
0.00000
0.00000
0.00000 0.00000

Dash 7
0.00032 0.00000 0.00000
0.00000 0.00000 O. 8.




| Technology ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pre Tier 0 | No | 0.0000 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Pre Tier 0 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 0 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 0 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Locomotives Serviced |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |  |
| Pre Tier 0 | No | 0.00335 | 0.01232 | 0.18261 | 0.00724 | 0.26657 | 0.00270 | 0.00546 | 0.00032 | 0.05224 | 0.03906 | 0.00011 |
| Pre Tier 0 | Yes | 0.00157 | 0.00416 | 0.00043 | 0.00000 | 0.00065 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00324 | 0.00000 |
| Tier 0 | No | 0.00059 | 0.00005 | 0.00643 | 0.00000 | 0.07099 | 0.08045 | 0.00157 | 0.00000 | 0.01194 | 0.04176 | 0.00140 |
| Tier 0 | Yes | 0.00108 | 0.00205 | 0.00059 | 0.00000 | 0.00205 | 0.00022 | 0.00000 | 0.00000 | 0.00000 | 0.02539 | 0.00000 |
| Tier 1 | No | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.01086 | 0.00000 | 0.00000 | 0.00000 | 0.00108 | 0.00000 |
| Tier 1 | Yes | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.07067 | 0.00000 | 0.00000 | 0.00000 | 0.06494 | 0.00000 |
| Tier 2 | No | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00454 | 0.00000 |
| Tier 2 | Yes | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00702 | 0.00000 | 0.00000 | 0.00000 | 0.01226 | 0.00000 |

Locomotive Model Distribution by Train Type Groups
 Dash 8
0.04458
0.00000
0.00703
0.00000
0.00000
0.00000
0.00000
0.00000 Dash 7
0.00024 0.00000 0.00000
0.00000 0.00000
0.00000 0.00000 0.00000
0.00000
SD-90
0.00351
0.00000
0.00061
0.00000
0.00000
0.00000
0.00000
0.00000

 | $\circ$ |
| :--- |
| 8 |
|  |
|  |
| 0 |



 | 28 |
| :--- |
| y |
| 4. |
| 0. |
| 0 | 0.00497 SD-50 GP-60

 0.00073
0.12780 0.12780

0.01175 0.00000 | 8 |
| :--- |
| 8 |
| 8 |
| . | $\circ$

8
$\circ$
$\circ$
0
$00000^{\circ} 0$
 0.00000

Yard Switchers

## Yard Switchers

Technology ZTR/AESS Switcher Pre Tier 0 Tier 0
Tier 0
Tier 1
Tier 1
Tier 2 Technology





| Appendix A2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Locomotive Model Distribution by Train Type Groups |  |  |  |  |
|  |  |  |  |  |
| GP-4x | SD-50 | GP-60 | SD-7x | SD-90 |
| 0.19794 | 0.00686 | 0.23741 | 0.00057 | 0.01030 |
| 0.00172 | 0.00000 | 0.00114 | 0.00000 | 0.00000 |
| 0.01030 | 0.00000 | 0.06293 | 0.08238 | 0.00286 |
| 0.00172 | 0.00000 | 0.00172 | 0.00000 | 0.00000 |
| 0.00000 | 0.00000 | 0.00000 | 0.00744 | 0.00000 |
| 0.00000 | 0.00000 | 0.00000 | 0.07666 | 0.00000 |
| 0.00000 | 0.00000 | 0.00000 | 0.00000 | 0.00000 |
| 0.00000 | 0.00000 | 0.00000 | 0.00915 | 0.00000 |





APPENDIX A-3

SAMPLE CALCULATIONS

| Description | Code | Events/Year | per Consist | Group | Working | Fuel |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Thru EB | 1 | 792 | 3.107 | 1 | 3.107 | 0.50 |
| Thru EB Setouts | 2 | 95 | 3.107 | 1 | 3.107 | 0.50 |
| Thru WB | 3 | 4378 | 2.957 | 1 | 2.957 | 0.50 |
| Thru WB Setouts | 4 | 178 | 2.957 | 1 | 2.957 | 0.50 |
| Freight Train EB Arrivals | 5 | 822 | 3.387 | 3 | 3.387 | 0.00 |
| Freight Train EB Departures | 6 | 4521 | 3.844 | 2 | 3.844 | 0.90 |
| Freight Train WB Arrivals | 7 | 4505 | 4.112 | 2 | 4.112 | 0.00 |
| Freight Train WB Departures | 8 | 1570 | 2.999 | 3 | 2.999 | 0.90 |
| Local Train EB Arrivals | 9 | 1412 | 3.075 | 3 | 3.075 | 1.00 |
| Local Train EB Departures | 10 | 24 | 2.458 | 3 | 2.458 | 1.00 |
| Local Train WB Arrivals | 11 | 110 | 2.964 | 3 | 2.964 | 1.00 |
| Local Train WB Departures | 12 | 1213 | 2.961 | 3 | 2.961 | 1.00 |
| Power Moves Thru EB Arrivals | 13 | 14 | 3.214 | 1 | 1.500 | 0.50 |
| Power Moves Thru EB Departures | 14 | 14 | 3.214 | 1 | 1.500 | 0.50 |
| Power Moves Thru WB Arrivals | 15 | 49 | 4.388 | 1 | 1.500 | 0.50 |
| Power Moves Thru WB Departures | 16 | 49 | 4.388 | 1 | 1.500 | 0.50 |
| Power Moves EB Arrivals | 17 | 546 | 3.617 | 4 | 1.500 | 0.00 |
| Power Moves EB Departures | 18 | 524 | 3.124 | 4 | 1.500 | 0.90 |
| Power Moves WB Arrivals | 19 | 1071 | 2.522 | 4 | 1.500 | 0.00 |
| Power Moves WB Departures | 20 | 1314 | 2.494 | 4 | 1.500 | 0.90 |
| Hump Set Return to Receiving Yard West End | 21 | 7300 | 3.000 | 5 | 3.000 | 1.00 |
| Hump Set Push Notch 2 | 22 | 1460 | 3.000 | 5 | 3.000 | 1.00 |
| Hump Set Push DB | 23 | 8030 | 3.000 | 5 | 3.000 | 1.00 |
| Trim Sets | 24 | 25185 | 2.000 | 5 | 2.000 | 1.00 |
| Consist Movements in Service Track | 25 | 5080 | 3.648 | 5 | 1.500 | 0.90 |
| Crew Changes on EB Thru | 26 | 149 | 3.107 | 1 | 3.107 | 0.50 |
| Crew Changes on WB Thru | 27 | 4017 | 2.957 | 1 | 2.957 | 0.50 |


| Consist Groups | Group ID | Emission Factors Weighted by Model/Tier/ZTR Fractions - DPM g/hr per Locomotive |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Idle-NonZTR | Idle-All | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |
| California Fuel ( 221 ppm S) |  |  |  |  |  |  |  |  |  |  |  |  |
| Thru Trains and Power Moves | 1 | 20.38 | 28.91 | 54.85 | 48.76 | 98.42 | 221.07 | 281.99 | 362.07 | 546.04 | 624.04 | 720.65 |
| Freight Train WB Arrival and EB Departure | 2 | 23.58 | 31.54 | 66.59 | 50.86 | 110.15 | 227.84 | 279.15 | 372.62 | 525.34 | 591.06 | 702.33 |
| Freight Train EB Arrival, WB Departure and Locals | 3 | 41.98 | 43.06 | 81.86 | 44.71 | 122.36 | 245.22 | 264.09 | 336.26 | 556.18 | 694.46 | 863.99 |
| Power Moves In Yard | 4 | 35.80 | 39.04 | 77.02 | 47.36 | 116.52 | 241.32 | 271.17 | 351.11 | 550.11 | 676.72 | 829.75 |
| Hump and Trim Sets | 5 | 47.94 | 47.94 | 80.04 | 35.70 | 134.30 | 211.93 | 228.61 | 289.68 | 488.55 | 584.17 | 749.94 |
| 47-State Fuel (2639 ppm S) |  |  |  |  |  |  |  |  |  |  |  |  |
| Thru Trains and Power Moves | 1 | 20.38 | 28.91 | 54.85 | 48.76 | 98.42 | 241.55 | 313.20 | 407.31 | 612.70 | 705.09 | 820.26 |
| Freight Train WB Arrival and EB Departure | 2 | 23.58 | 31.54 | 66.59 | 50.86 | 110.15 | 250.30 | 309.83 | 417.61 | 591.31 | 677.56 | 810.03 |
| Freight Train EB Arrival, WB Departure and Locals | 3 | 41.98 | 43.06 | 81.86 | 44.71 | 122.36 | 260.64 | 294.03 | 382.41 | 619.57 | 754.55 | 940.41 |
| Power Moves In Yard | 4 | 35.80 | 39.04 | 77.02 | 47.36 | 116.52 | 258.99 | 301.62 | 397.51 | 614.59 | 745.77 | 916.78 |
| Hump and Trim Sets | 5 | N/A -- Hump and trim sets operate on 100\% California Fuel |  |  |  |  |  |  |  |  |  |  |



## $\begin{array}{lc}\text { Consist Groups } & \text { Group ID } \\ \text { California Fuel (221 ppm S) } & \\ \text { Thru Trains and Power Moves } & 1 \\ \text { Freight Train WB Arrival and EB Departure } & 2 \\ \text { Freight Train EB Arrival, WB Departure and Locals } & 3 \\ \text { Power Moves In Yard } & 4 \\ \text { Hump and Trim Sets } & 5 \\ & \\ \text { 47-State Fuel (2639 ppm S) } & 1 \\ \text { Thru Trains and Power Moves } & 2 \\ \text { Freight Train WB Arrival and EB Departure } & 3 \\ \text { Freight Train EB Arrival, WB Departure and Locals } & 4 \\ \text { Power Moves In Yard } & 5\end{array}$



| Locomotive Model Distributions Thru Trains and Power Moves |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |
| Pre Tier 0 | No | 0.0000 | 0.0007 | 0.0798 | 0.0076 | 0.0451 | 0.0046 | 0.0059 | 0.0003 | 0.0939 | 0.0942 | 0.0004 |
| Pre Tier 0 | Yes | 0.0000 | 0.0001 | 0.0000 | 0.0000 | 0.0003 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0066 | 0.0000 |
| Tier 0 | No | 0.0000 | 0.0000 | 0.0031 | 0.0001 | 0.0113 | 0.2231 | 0.0014 | 0.0000 | 0.0151 | 0.0400 | 0.0019 |
| Tier 0 | Yes | 0.0001 | 0.0000 | 0.0000 | 0.0000 | 0.0006 | 0.0009 | 0.0000 | 0.0000 | 0.0000 | 0.0102 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0445 | 0.0000 | 0.0000 | 0.0000 | 0.0002 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.1808 | 0.0000 | 0.0000 | 0.0000 | 0.0287 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0295 | 0.0000 | 0.0000 | 0.0000 | 0.0690 | 0.0000 |
| Freight Train WB Arrival and EB Departure |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |
| Pre Tier 0 | No | 0.0001 | 0.0015 | 0.0967 | 0.0081 | 0.1422 | 0.0028 | 0.0042 | 0.0036 | 0.0735 | 0.0687 | 0.0001 |
| Pre Tier 0 | Yes | 0.0001 | 0.0005 | 0.0001 | 0.0000 | 0.0002 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0047 | 0.0000 |
| Tier 0 | No | 0.0000 | 0.0000 | 0.0033 | 0.0001 | 0.0353 | 0.1265 | 0.0007 | 0.0000 | 0.0139 | 0.0642 | 0.0014 |
| Tier 0 | Yes | 0.0001 | 0.0001 | 0.0000 | 0.0000 | 0.0016 | 0.0005 | 0.0000 | 0.0000 | 0.0000 | 0.0508 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0218 | 0.0000 | 0.0000 | 0.0000 | 0.0028 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.1091 | 0.0000 | 0.0000 | 0.0000 | 0.1230 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0093 | 0.0000 | 0.0000 | 0.0000 | 0.0285 | 0.0000 |


| Appendix A-3-Sample Calculations |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ireight Train EB Arrival, WB Departure and Locals |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |
| Pre Tier 0 | No | 0.0018 | 0.0076 | 0.1915 | 0.0015 | 0.5806 | 0.0003 | 0.0008 | 0.0003 | 0.0072 | 0.0081 | 0.0000 |
| Pre Tier 0 | Yes | 0.0020 | 0.0048 | 0.0001 | 0.0000 | 0.0008 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0003 | 0.0000 |
| Tier 0 | No | 0.0001 | 0.0001 | 0.0052 | 0.0000 | 0.1343 | 0.0107 | 0.0003 | 0.0000 | 0.0009 | 0.0069 | 0.0004 |
| Tier 0 | Yes | 0.0003 | 0.0005 | 0.0000 | 0.0000 | 0.0030 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0040 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0016 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0077 | 0.0000 | 0.0000 | 0.0000 | 0.0117 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0020 | 0.0000 | 0.0000 | 0.0000 | 0.0029 | 0.0000 |
| Power Moves In Yard |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |
| Pre Tier 0 | No | 0.0010 | 0.0045 | 0.1124 | 0.0039 | 0.4626 | 0.0019 | 0.0035 | 0.0002 | 0.0446 | 0.0268 | 0.0000 |
| Pre Tier 0 | Yes | 0.0006 | 0.0028 | 0.0002 | 0.0000 | 0.0007 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0027 | 0.0000 |
| Tier 0 | No | 0.0002 | 0.0001 | 0.0032 | 0.0000 | 0.1278 | 0.0422 | 0.0006 | 0.0000 | 0.0070 | 0.0221 | 0.0013 |
| Tier 0 | Yes | 0.0007 | 0.0002 | 0.0000 | 0.0000 | 0.0118 | 0.0007 | 0.0000 | 0.0000 | 0.0000 | 0.0155 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0074 | 0.0000 | 0.0000 | 0.0000 | 0.0005 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0428 | 0.0000 | 0.0000 | 0.0000 | 0.0338 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0050 | 0.0000 | 0.0000 | 0.0000 | 0.0087 | 0.0000 |
| Hump and Trim Sets |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |
| Pre Tier 0 | No | 0.0000 | 0.0000 | 1.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Pre Tier 0 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 0 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 0 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

## Appendix A-3-Sample Calculations

| Track Segment | Number | (mi) |
| :---: | :---: | :---: |
| Main Line 1 | 1 | 2.224 |
| Main Line 2 | 2 | 0.136 |
| Main Line 3 | 3 | 1.822 |
| Main Line 4 | 4 | 0.363 |
| Main Line 5 | 5 | 0.173 |
| Main Line 6 | 6 | 0.332 |
| Main Line 7 | 7 | 0.120 |
| Main Line 8 | 8 | 0.352 |
| Receiving Yard West End Entrance | 11 | 0.117 |
| Receiving Yard West End | 12 | 0.467 |
| Receiving Yard Middle | 13 | 0.934 |
| Receiving Yard East End | 14 | 0.467 |
| Receiving Yard East End Entrance | 15 | 0.241 |
| Receiving Yard to Hump | 16 | 0.363 |
| Hump to Service 1 | 17 | 0.221 |
| Hump to Service 2 | 18 | 0.113 |
| Hump to Service 3 | 19 | 0.315 |
| Hump to Service 4 | 20 | 0.075 |
| Service Track Entrance | 21 | 0.204 |
| Service Track | 22 | 0.246 |
| Service Track East End | 23 | 0.063 |
| Service Track to Ready Track East 1 | 24 | 0.076 |
| Service Track to Ready Track East 2 | 25 | 0.053 |
| Ready Track East | 26 | 0.154 |
| Ready Track West | 27 | 0.154 |
| Ready Track West Entrance | 28 | 0.087 |
| Service Track Wye East Entrance | 31 | 0.087 |
| Service Track Wye East Leg | 32 | 0.065 |
| Service Track Wye South Lead | 33 | 0.073 |
| Service Track Wye West Leg | 34 | 0.068 |
| Service Track Wye North Leg | 35 | 0.058 |
| Service Track Wye West Entrance | 36 | 0.114 |
| Service Track to Departure Yard | 41 | 0.244 |
| Departure Yard South - Middle | 42 | 0.326 |
| Departure Yard South - East End | 43 | 0.238 |
| Departure Yard South - East Entrance | 44 | 0.209 |
| Bowl to Departure Yard South | 45 | 0.224 |
| Departure Yard North - West End | 46 | 0.252 |
| Departure Yard North - Middle | 47 | 0.252 |
| Departure Yard North - East End | 48 | 0.291 |

## Appendix A-3-Sample Calculations

| Track Segment | Segment <br> Number | Length <br> (mi) |
| :--- | :---: | :---: |
| Departure Yard North - East Entrance | 49 | 0.205 |
| Bowl North 1 | 51 | 0.222 |
| Bowl North 2 | 52 | 0.230 |
| Bowl North 3 | 53 | 0.686 |
| Bowl South 1 | 54 | 0.160 |
| Bowl South 2 | 55 | 0.331 |
| Bowl South 3 | 56 | 0.658 |
| Main Line Leg to Palmdale 1 | 61 | 0.057 |
| Main Line Leg to Palmdale 2 | 62 | 0.040 |
| Main Line Leg to Palmdale 3 | 63 | 0.045 |
| Main Line Leg to Palmdale 4 | 64 | 0.050 |
| Cedar (Crew Change Location) | 71 | 0.172 |

* Note: Approximately $5 \%$ of consists for south bound trains use the "Y" to turn to be facing south








$\begin{array}{ccccccc}\text { Activity Code } & \begin{array}{c}\text { Segment } \\ \text { Number }\end{array} & \begin{array}{c}\text { Speed } \\ (\mathbf{m p h})\end{array} & \begin{array}{c}\text { Duty Cycle } \\ \text { Number }\end{array} & \begin{array}{c}\text { Non-ZTR Idle Time } \\ \text { (hrs) }\end{array} & \begin{array}{c}\text { ZTR Idle Time } \\ \text { (hrs) }\end{array} & \begin{array}{c}\text { Fraction of Segment } \\ \text { or Time Moving }\end{array} \\ 25 & -26 & 10 & 2 & 0.000 & 0.000 & 0.750 \\ 25 & -36 & 10 & 2 & 0.000 & 0.000 & 0.250 \\ 25 & -21 & 10 & 2 & 0.000 & 0.000 & 0.250 \\ 25 & -28 & 10 & 2 & 0.000 & 0.000 & 0.250 \\ 25 & -27 & 10 & 2 & 0.000 & 0.000 & 0.250 \\ 26 & 71 & 10 & 2 & 0.000 & 0.167 & 0.000 \\ 27 & 71 & 10 & 2 & 0.000 & 0.167 & 0.000\end{array}$

| \％ $0 \cdot 0$ | \％000 | \％000 | \％ 00 | \％000 | \％0＇0 | \％0 0 | \％0＇0 | \％0001 | \％00 | 9 |  |
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| \％0＇0 | \％00 | \％0＇0 | \％00 | \％00 | \％00 | \％0＇st | \％ 0 ＇st | $\% 00$ | \％000 | $\dagger$ |  |
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|  |  |  |  |  | szo 0 | $000^{\circ}$ | $000^{\circ}$ | $\varepsilon$ | t | $\dagger \tau$ | ＂ |
|  |  |  |  |  | SLO $0^{\circ}$ | $000^{\circ}$ | 0000 | $\varepsilon$ | $\varepsilon \downarrow$ | $\dagger \tau$ | ＂ |
|  |  |  |  |  | 0010 | $000^{\circ}$ | 0000 | $\varepsilon$ | てt | 七て | ＂ |
|  |  |  |  |  | 0010 | $000{ }^{\circ}$ | $000 \cdot 0$ | $\varepsilon$ | st | $\dagger \tau$ | ＂ |
|  |  |  |  |  | 0¢で0 | $000^{\circ}$ | 0000 | $\varepsilon$ | 95 | ヶて | ＂ |
|  |  |  |  |  | 0¢̧て0 | $000^{\circ}$ | $000^{\circ}$ | $\varepsilon$ | $\varepsilon \varsigma$ | $\dagger \tau$ |  |
|  |  |  |  |  | 1810 | $000^{\circ}$ | $000^{\circ}$ | 9 | 91 | $\varepsilon \tau$ | ＂ |
|  |  |  |  |  | 0zto | $000^{\circ}$ | $000^{\circ}$ | 9 | sı | $\varepsilon \tau$ | ＂ |
|  |  |  |  |  | £̇̇て | $000^{\circ}$ | 0000 | 9 | ¢ | $\varepsilon \tau$ | ＂ |
|  |  |  |  |  | 99t＇0 | $000^{\circ}$ | $000^{\circ}$ | 9 | $\varepsilon 1$ | $\varepsilon \tau$ |  |
|  |  |  |  |  | 008.0 | $000^{\circ}$ | $000 \cdot 0$ | ¢ | z1 | zz | － |
|  |  |  |  |  | $00 z^{\circ}$ | $000^{\circ}$ | $000{ }^{\circ}$ | $\varsigma$ | II | zz |  |
|  |  |  |  |  | 0 tr 0 | 0000 | $000^{\circ}$ | $\dagger$ | 91 | 12 | ． |
|  |  |  |  |  | E60 ${ }^{\circ}$ | $000^{\circ}$ | $000{ }^{\circ}$ | $\dagger$ | ¢ı | 12 | ＂ |
|  |  |  |  |  | 0810 | $000^{\circ}$ | $000^{\circ}$ | t | †1 | 12 | ＂ |
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|  |  |  |  |  | $08 \mathrm{I}^{\circ} 0$ | $000^{\circ}$ | $000^{\circ}$ | t | zI | 12 | －${ }^{\text {a }}$ |
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| Appendix A-3-Sample Calculations |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Emission Factors Weighted by Model/Tier/ZTR Fractions - DPM g/hr per Locomotive |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Locomotive Model Group | Group ID | Idle-NonZTR | Idle-All | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |  |
| California Fuel (221 ppm S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Service | 1 | 31.52 | 36.57 | 72.43 | 47.36 | 114.81 | 230.95 | 268.86 | 351.95 | 529.91 | 624.49 | 760.23 |  |
| LoadTest | 2 | 32.02 | 37.26 | 72.46 | 46.93 | 114.53 | 228.49 | 266.4 | 350.76 | 525.37 | 616.69 | 753.34 |  |
| 47-State Fuel (2639 ppm S) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Service | 1 | 31.52 | 36.57 | 72.43 | 47.36 | 114.81 | 249.95 | 298.82 | 396.91 | 593.63 | 697.91 | 852.37 |  |
| LoadTest | 2 | 32.02 | 37.26 | 72.46 | 46.93 | 114.53 | 247.18 | 296.1 | 395.6 | 588.49 | 689.06 | 844.16 |  |
| Note: Idle-NonZTR is the average per-locomotive idle emission rate for the fraction of locomotives not equipped with ZTR/Auto start-stop technology |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Service and Shop Activity |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Duration of Activity per Locomotive (minutes) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Activity | Number of Locomotives | Fraction of Calif. Fuel | $\begin{gathered} \text { Idle- } \\ \text { NonZTR } \end{gathered}$ | Idle-All | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |
| Service - Inbound \& Service | 18532 | 0.00 | 0 | 90 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Service - Post Service | 18532 | 0.90 | 60 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pre-Maintenance Load Test | 661 | 0.90 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Post-Maintenance Load Test | 661 | 0.90 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Quarterly Maintenance Load Test | 832 | 0.90 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Unscheduled Mtc Diagnostic Test | 18 | 0.90 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Unscheduled Mtc Post Test | 1048 | 0.90 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Locomotive Model Distributions |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Locomotives Serviced |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Technology | ZTR/AESS | Switcher | GP-3x | GP-4x | SD-50 | GP-60 | SD-7x | SD-90 | Dash 7 | Dash 8 | Dash 9 | C-60 |  |
| Pre Tier 0 | No | 0.0034 | 0.0123 | 0.1826 | 0.0072 | 0.2666 | 0.0027 | 0.0055 | 0.0003 | 0.0522 | 0.0391 | 0.0001 |  |
| Pre Tier 0 | Yes | 0.0016 | 0.0042 | 0.0004 | 0.0000 | 0.0007 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0032 | 0.0000 |  |
| Tier 0 | No | 0.0006 | 0.0001 | 0.0064 | 0.0000 | 0.0710 | 0.0805 | 0.0016 | 0.0000 | 0.0119 | 0.0418 | 0.0014 |  |
| Tier 0 | Yes | 0.0011 | 0.0021 | 0.0006 | 0.0000 | 0.0021 | 0.0002 | 0.0000 | 0.0000 | 0.0000 | 0.0254 | 0.0000 |  |
| Tier 1 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0109 | 0.0000 | 0.0000 | 0.0000 | 0.0011 | 0.0000 |  |
| Tier 1 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0707 | 0.0000 | 0.0000 | 0.0000 | 0.0649 | 0.0000 |  |
| Tier 2 | No | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0045 | 0.0000 |  |
| Tier 2 | Yes | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0070 | 0.0000 | 0.0000 | 0.0000 | 0.0123 | 0.0000 |  |













Example 1 -- WB Arriving Freight Trains

Departure Yard North - East Entrance
Departure Yard North - East End Departure Yard North - Middle
Departure Yard North - West End Bowl North 3
Bowl North 2 Bowl North 1
Receiving Yard to Hump Receiving Yard East End Entrance
Receiving Yard East End Receiving Yard Middle
 Receiving Yard West End Receiving Yard Middle
Receiving Yard East End Receiving Yard East End Entrance Receiving Yard to Hump Hump to Service 1
Hump to Service 2 Hump to Service 3
Hump to Service 4 Service Track Entrance


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No.
苞~~~
Emission Factors
Arriving IM Trains - CA Fuel
Arriving IM Trains - 47-State Fuel
CA Fuel Fraction Adjusted Rates
Duty Cycle Moving
Weighted g/hr emissions

APPENDIX A-4
METHODOLOGY FOR ESTIMATING LOCOMOTIVE EMISSIONS AND GENERATING AERMOD EMISSION INPUTS

## Appendix A-4

## Methodology for Estimating Locomotive Emissions and Generating AERMOD Emission Inputs

## Overview

This appendix describes the general procedures followed for developing locomotive emission inventories for the Union Pacific Railroad (UPRR) rail yards under the Memorandum of Understanding with the California Air Resources Board. It also describes the procedure by which the emission inputs are prepared for both locomotive and non-locomotive sources are used in AERMOD dispersion modeling.

## EMISSION CALCULATIONS

This section describes the details of the development of activity inputs, emission factors, and emission estimates for locomotive operations. Separate procedures are followed for estimating activity associated with locomotives on trains, locomotive consist movements within a yard, service and shop activity (if occurring at a specific yard), and yard switching operations within a yard. Emission factors are developed for each of the types of locomotive activity based on the model and technology distribution of locomotives involved in each activity. Emission estimates are then developed for the activities and specific areas of a yard in which each activity occurs. The data used to calculate these emissions are included in the Appendix A-3 Excel workbook, which includes a "Sample Calculations" worksheet showing the linkages between the various activities, emission factors, and operating characteristics data.

## Train Activity

Train activity data for emissions calculations include a number of separate components:
-- The number of trains arriving, departing, or passing through a yard, broken down by type of train;

- The average composition of working locomotives in each consist ${ }^{1}$, including the fraction of locomotives of different models, emissions technology tier, and automatic idling control equipment ${ }^{2}$;
-- The identification of routes followed for different types of train activities; and

[^10]-- Identification of the speeds and throttle settings for different types of train activities in different locations.

The primary source of information for estimating train activity is a database identifying the arrival and departure of locomotives at a specific yard. This database identifies locomotives by their ID numbers and models, the status on the train (working or not working), and the specific train to which they are connected. From these data, the total numbers of trains of different types are identified based on train symbols, train dates, train origination and termination indicators, and dates and times of arrival and departure. For each type of train and activity, the average number of locomotives per consist is calculated along with the distribution of locomotive models, emission technology tiers, and automatic idling control equipment. A separate database of UPRR locomotives is consulted based on locomotive ID to determine the tier and date of any retrofits of automatic idling controls to complete the development of these model distributions. The activity data so derived are shown on the "Activities" worksheet in the Appendix A-3 Excel workbook, and the model and technology distributions are shown on the "Consist Emissions" worksheet.

The types of trains to be identified can vary from yard to yard. For all yards, through trains (which bypass the yard itself on mainline tracks adjacent to the yard) are identified. Depending on the yard, trains entering or departing from the yard can be of several types, including:
-- Intermodal trains;
-- Automobile trains;
-- "Manifest" or freight trains;

- Local trains; and
- Power moves.

Power moves are trains consisting only of locomotives that are either arriving at the yard to be serviced or used for departing trains, or departing from the yard to be serviced at another location or used for trains departing from another location. The routes followed by each type of train on arrival and departure are identified in consultation with UPRR yard personnel, along with estimates of average speeds and duty cycles (fraction of time spent at different throttle settings) for different areas.

Specific track subsections are identified by UTM coordinates digitized from georeferenced aerial photographs. The segments identified and their lengths are shown on the "Track Segments" worksheet of Appendix A-3. For each train type, direction, and route, a listing of track segments, segment lengths, and duty cycles is developed. Duty cycles are shown on the "Consist Emissions" worksheet of Appendix A-3, and the segment speeds, duty cycles, idling durations are shown on the "Movements and Yard Operations" worksheet. This listing, along with the number of locomotives per consist and number of trains of each type, allows the number of locomotive hours in each duty cycle to be calculated for each section of track. For arriving and departing trains, estimates of the duration of idling were developed in consultation with UPRR personnel.

These idling periods were divided into two parts: the assumed amount of time that all locomotives in a consist would idle on arrival or departure, and the amount of time that only locomotives not equipped with automatic idle controls would idle. Idling periods were assigned to a segment of the arrival or departure track one fifth of the length of the track at the appropriate end.

## Service and Shop Activity

If there is a service track and/or shop at a yard, locomotives (including both road power from trains as well as yard switchers) undergo a variety of activities at these locations. If present at a yard, details of the service and shop activity, model distributions, and emission factors are shown on the "Service and Shop" worksheet of Appendix A-3. Specific locomotive activities involve idling while awaiting or undergoing routine service (cleaning, refueling, oiling, sanding, and other minor maintenance), movement and idling between service and maintenance areas, and stationary load testing associated with specific types of maintenance events. A database of service events at individual yards identifies the number of service events during the year, the locomotive ID and model, and the nature of servicing performed. Routine servicing involves periods of idling prior to and during service, and additional idling prior to movement of consists to departing trains in the yard. Estimates of the duration of idling associated with servicing are developed in consultation with UPRR personnel. As was done for trains, these idling periods were separated into two parts: the average total duration of idling by all locomotives, and the average duration of additional idling by locomotives not equipped with automatic idling controls.

The database also specifically identifies load test events and the type of maintenance with which the load testing is associated. These types include planned maintenance at different intervals (e.g., quarterly, semiannual) as well as unscheduled maintenance that may involve both diagnostic load testing prior to maintenance and post-maintenance load testing. The duration of load test events in each throttle setting depends on the equipment available and types of maintenance performed at the yard. Estimates of these durations, as well as the identification of load testing activity by type of load test and the time and duration of any additional idling and movements, are developed in consultation with UPRR personnel.

A total number of events (servicing and load testing by location and type) are developed from these data, as are locomotive model and technology distributions for all locomotives serviced and for those specific locomotives undergoing load testing (if applicable). From these event counts and durations, the total number of hours of locomotive idling and higher throttle setting operation in different portions of the service areas are calculated for each of the two model distributions.

## Yard Switcher Activity

In each yard, there are routine jobs assigned to individual switchers or sets of switchers. These activities are generally not tracked from hour to hour, but they occur routinely within yard boundaries during specified work shifts. Similarly, the specific yard switcher
locomotive IDs assigned to these jobs are not routinely tracked, but these yard jobs are generally assigned to a specific model of low horsepower locomotive. From the assigned yard switcher jobs and shifts, and in consultation with UPRR personnel, an estimate of the hours per day of switcher operation in a yard are developed, along with the specific times of day when these activities occur (time of day assignments were made only if operation was less than 24 hour per day). Duty cycles for switching operation are also developed in consultation with local UPRR personnel. Depending on the type of activity and type of trains being handled in a yard, duty cycle estimates may vary. In the absence of more detailed information, the USEPA switcher duty cycle is assumed to be representative of each switcher's operation ${ }^{3}$. The total number of locomotive hours of operation for each model are calculated and assigned to the areas in which the units work. In some cases, yard jobs are assigned to specific areas within the yard and specific models of locomotives. In these cases, the switcher activities are assigned specifically to these areas of the yard.

## Emission Factor Development

The locomotive model and technology group distributions derived in the development of activity data are grouped by type or types of activity with consideration for the level and nature of the activity. For example, a single distribution is used for through trains of all types, including power moves, while consist model distributions for different types of trains within a yard may be treated as separate distributions if they are handled in different areas of a yard. As shown in Part VII of this report, model-group-specific emission factors by throttle setting were developed based on emission test data and sulfur content adjustment factors. From these emission factors and the locomotive model and technology distributions for different types of trains and activities, weighted average emission factors are calculated for the "average" locomotive for that train type or activity on a gram per hour basis. For each train type or activity, two separate idle emission rates are calculated. The first is the straight weighted average emission rate for all locomotives, while the second is the weighted average only for the fraction of locomotives without automatic idle controls. Mathematically,

$$
\bar{Q}(l)=\sum_{i=1}^{11} \sum_{j=1}^{4} \sum_{k=1}^{2} F(i, j, k) \cdot Q(i, j, l)
$$

for $l$ corresponding to idle through N 8 , and

$$
\bar{Q}\left(l^{*}\right)=\sum_{i=1}^{11} \sum_{j=1}^{4} F(i, j, 1) \cdot Q\left(i, j, l^{*}\right)
$$

[^11]for idling emission rate during periods when only locomotives without automatic idle controls are idling
where
\[

$$
\begin{aligned}
& \overline{\bar{Q}}(l)=\text { weighted average emission factor for throttle setting } l \\
& Q(i, j, l)=\text { the base } \mathrm{g} / \mathrm{hr} \text { emission factor of a particular model group/technology } \\
& \text { class and throttle setting } \\
& F(i, j, k)=\text { the fraction of locomotives of a particular model group/technology class } \\
& i=\text { model group index (Switcher, GP-3x, etc.) } \\
& j=\text { technology tier index (pre-Tier 0, Tier 0, Tier 1, Tier 2) } \\
& k=\text { automatic idle control status index (with or without) } \\
& l=\text { throttle setting (idle, N1, . ., N8) } \\
& l^{*}=\text { index for idle throttle of locomotives without automatic idle controls. }
\end{aligned}
$$
\]

Thus, for each defined locomotive model distribution, gram per hour emission factors are generated for each throttle setting.

## Emission Calculations - Locomotive Movements

From the train activity analysis, the following data are available for each segment of track: track length of segment $L(i)$; speed $V(i)$; movement duty cycle $\boldsymbol{D}(i)$ (a vector of fractions of time spent in each throttle setting); number of trains of each type $N(j)$; and number of working locomotives per consist for each train type $C(j)$. For each type of train $j$, there is a set of throttle-specific emission factors $Q_{j}(l)$ for the "average" locomotive used on that train type. If a particular type of train or consist movement can follow multiple paths within the yard, the activity is allocated to sequences of track segments representing each such path. Total annual emissions $q_{\text {tot }}(i)$ for each segment are then calculated as

$$
q_{t o t}(i)=\frac{L(i)}{V(i)} \cdot \sum_{j} N(j) \cdot C(j) \sum_{l} D(i, l) \cdot Q_{j}(l) .
$$

## Emission Calculations - Locomotive Idling

Locomotive idling is calculated in a similar manner for road power and locomotives in service. For each train type and for service events, activity data provide a number of annual events $N(i)$, duration of idling by locomotives with $\left(T_{\text {all }}(i)\right)$ and without $\left(T_{n Z T R}(i)\right)$ automatic idle control, and gram per hour emission rates for the "average" locomotive $Q_{\text {all }}(i)$, and the "average" locomotive excluding those with automatic idle controls $Q_{n Z T R}(i)$. Total annual emissions are calculated as

$$
q_{\text {idle }}=\sum_{i}-N(i) \cdot C(i) \cdot\left(T_{\text {all }}(i) \cdot Q_{\text {all }}(i)+T_{n Z T R}(i) \cdot Q_{n Z T R}(i)\right) .
$$

If a particular type of activity occurs at multiple locations within the yard (e.g., on multiple arrival or departure tracks), then the idling time is allocated to different segments of track as appropriate so that segment-specific emissions are obtained.

## Emission Calculations - Load Testing

Load testing emissions are calculated separately for each throttle setting (idle, N1, and N8) using the weighted average emission factors for the load-tested units, the number of load tests of different types, and the duration of testing in each throttle setting for each type of test.

## Emission Calculations - Yard Switcher Operations

Activity data provide the number and model group information for yard switchers, and the number of operating hours per day. Model-group-specific emission factors are multiplied by the duty cycle to generate weighted average gram per hour emissions for idling and for combined emissions from operation in notch 1 through notch 8. Emissions are calculated directly from the number of units, hours per day working, and duty cycle weighted emission factors for both idle and non-idle throttle settings during work shifts.

## AERMOD EMISSION INPUT PREPARATION

Emissions from both locomotives and from other emission sources in a yard are allocated to multiple individual point or volume sources in AERMOD inputs. In addition to each type of activity's emission rates, the locations of emissions, the release parameters, and other inputs (e.g., building downwash parameters, temporal variation in emissions, etc.) are required by AERMOD. Emission inputs are prepared sequentially for different types of activities and the areas within which they occur. The source elevation for each point or volume source is interpolated from a high-resolution terrain file.

## Locomotive Movements

For each type of locomotive movement, emissions calculated for each track segment are uniformly allocated to a series of evenly spaced volume sources along that track segment. The maximum spacing between sources is specified and the number of sources to be used for each segment is calculated from the segment length. The raw emission rate value in the AERMOD inputs ( $\mathrm{g} / \mathrm{sec}$ ) is based directly on the annual emission total for the segment divided by the number of sources on that segment. For locomotive movements, separate day and night release parameters are needed. Therefore, each source is duplicated (but with a different source ID and parameters) in the AERMOD inputs, with temporal profile inputs (EMISFACT HROFDY) that use day time parameters from 06001800 and night time parameters for 1800-0600.

## Locomotive Idling and Load Testing

Locomotive idling and load testing emissions are allocated to track segments in the same manner as locomotive movements, but as point, rather than volume, sources. Each source location may have up to three separate sources identified, with different stack parameters used for idle, notch 1 , and notch 8 . Building downwash inputs are assigned from a pre-prepared set of records for a typical locomotive's dimensions and the orientation of the track segment on which the emissions occur.

## Yard Switcher Operations

Yard switcher operations are allocated to areas within the yard based on the estimated time spent working in each area. As for locomotive movements, yard switcher emissions for a specific area are allocated uniformly to a number of volume sources on defined segments. Day and night operations are handled similarly to train and consist movements, with EMISFACT HROFDY records used to switch day and night volume source release parameters. Depending on their magnitude and distance from yard boundaries, the "working idling" emissions for yard switching may be added to the nonidle emissions from volume sources, or treated as a series of point sources, using stack parameters for the specific model group being used. If treated as point sources, building downwash inputs are prepared as for other locomotive idling and load testing.

## APPENDIX A-5

PRINCIPLE LOCOMOTIVE ROUTES

## Appendix A-5

## Principle Locomotive Routes

Through Trains, Through Power Moves, and Power Moves Arriving and Departing


Green $=$ Through trains and through power moves
Dashed blue = Power moves arriving and departing from Service Track
Terminating Trains and Power Moves from Receiving Yard to Service Track


Green $=$ Terminating EB and WB trains
Dashed blue $=$ Power moves to Service Track

## Originating Trains and Power Moves from Ready Track



Green $=$ Departing EB and WB trains
Dashed blue $=$ Power moves from Ready Track

## Hump Push and Return Movements and Movements in Service Track



Solid green $=$ Hump set push movement
Dashed light green $=$ Hump set return route
Light blue $=$ Movements through Service Track to Ready Track

Notes:

1. Vertical scale has been expanded for clarity.

APPENDIX A-6
IRESON ET AL

# Development of Detailed Railyard Emissions to Capture Activity, Technology and Operational Changes 

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#### Abstract

Railyard operations involve a variety of complex activities, including inbound and outbound train movements, classification (i.e., separating cars from inbound trains for redirection to multiple destinations, and building new trains), and servicing locomotives. Standard locomotive duty cycles provide long-term average activity patterns for locomotive operations, but they are not appropriate for the specialized activities that occur within railyards or at locations such as ports, and emission densities in such areas can be high relative to those of line haul activities. There are significant emission rate differences between locomotive models, and differences in the types of service for which specific models are used. Data for throttle-specific emissions, activity levels, and locomotive models and operating practices can be used to provide more accurate emissions estimates for such operations. Such data are needed to quantify actual emissions changes in these high activity areas. A calculation scheme has been developed to generate detailed emission inventories based on the types of data that are collected for managing rail operations. This scheme allows improved accuracy in emissions estimation, and also provides a more reliable basis for bottom-up tracking of emissions changes over time. Factors that can be addressed include: changes in the distribution of locomotive models and control technology levels (e.g., increasing fractions of Tier 0,1 , and 2 locomotives) for both line haul and local operations; actual in-yard idling duration and reductions associated with auto-start-stop technologies; fuel quality effects; and detailed operating practices for switching and train-building operations. By providing detailed disaggregation of activity and emissions data, the method also makes it possible to quantify and evaluate the effects of specific emission reduction alternatives.


## INTRODUCTION

Freight movement by rail is a key component of the U.S. transportation infrastructure. The combination of rail's low rolling resistance and the fuel-efficient turbocharged diesel engines used in modern locomotives make rail the most efficient mode of transport from both an emissions and economic perspective. Railyards located strategically through the nation's rail network are used to assemble and direct goods movement to their destinations. Railyards may handle dozens of trains per day, each powered by a "consist" of several locomotives. While in railyards, these locomotives are serviced and regrouped into new consists as needed for specific departing trains. In addition to train arrivals and departures and locomotive servicing, so-called "classification" yards separate rail cars in inbound trains into segments with different destinations, and build new trains with a common destination. This work is accomplished by switcher locomotives (typically of lower horsepower than the locomotives used for "line-haul" operations). Some railyards also have major locomotive repair facilities whose activities include load testing of locomotives prior to or after maintenance. Collectively, the locomotive operations associated with these activities can result in relatively high localized emission densities.

The Union Pacific Railroad (UPRR) is the largest railroad in North America, operating throughout the western two-thirds of the United States. It operates a number of railyards throughout its system, including the J. R. Davis Yard in Roseville, California. The Davis Yard is UPRR's largest classification yard in the western U.S. It is approximately one-quarter mile wide and four miles long, and is visited by over 40,000 locomotives per year. The California Air Resources Board (CARB) recently completed a detailed dispersion modeling study to estimate concentrations of diesel particulate matter in the vicinity of the railyard. ${ }^{1}$ UPRR cooperated closely with CARB in this study, including the identification, retrieval and analysis of data needed to assemble a detailed emission inventory for railyard operations. This effort produced the most detailed emission inventory for railyard operations to-date, including empirically developed train counts, locomotive model distributions, locomotive service and maintenance activities, and dedicated on-site switching operations. The results of this effort have been further adapted to allow UPRR to track the effect of locomotive fleet modernization, freight volume, and operational changes on emissions, and to identify opportunities for further emission reductions at the Davis Yard.

## RAILYARD ACTIVITY ESTIMATION

At state and national levels, locomotive emissions have been estimated using locomotive fleet population data and average locomotive emission factors, expressed in $\mathrm{g} / \mathrm{bhp}-\mathrm{hr}$, in conjunction with fuel efficiency estimates and fuel consumption. For freight locomotives, the emission factors are typically derived using both a switching duty cycle and a line haul duty cycle, each of which gives the fraction of operating time locomotives spend at different throttle settings, referred to as notch positions. ${ }^{2}$ These throttle settings (see Table 1) include idle, notches 1 through 8, and dynamic braking (in which the locomotive traction motors are used to generate power which is dissipated through resistor grids). While this approach can provide reasonable estimates for larger regions, neither the overall locomotive fleet composition nor the standard duty cycles accurately reflect the specific activities that occur within an individual railyard. The $\mathrm{g} / \mathrm{bhp}$-hr emission factors vary substantially between throttle settings and between locomotive models. Other confounding factors include: speed limits within yards (which preclude the high throttle settings used for line-haul activity outside of yards); locomotive load (consists commonly move within yards with only one locomotive pulling and no trailing cars); and time spent either shut down or idling. Classification activities are carried out with duty cycles that are unique to yard operations and may vary from yard to yard. To develop more accurate emissions estimates, it is necessary to explicitly identify railyard activities at the level of individual locomotives.

Table 1. Locomotive Duty Cycles.

|  | Throttle Position (Percent Time in Notch) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Duty Cycle | D.B. | Idle | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |
| EPA Line-Haul | 12.5 | 38.0 | 6.5 | 6.5 | 5.2 | 4.4 | 3.8 | 3.9 | 3.0 | 16.2 |
| EPA Switch | 0.0 | 59.8 | 12.4 | 12.3 | 5.8 | 3.6 | 3.6 | 1.5 | 0.2 | 0.8 |
| Trim Operations | 0.0 | 44.2 | 5.0 | 25.0 | 2.3 | 21.5 | 1.5 | 0.6 | 0.0 | 0.0 |
| Hump Pull-Back | 0.0 | 60.4 | 12.5 | 12.4 | 5.9 | 3.6 | 3.6 | 1.5 | 0.0 | 0.0 |
| Hump Push | 0.0 | 0.0 | 0.0 | 100 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Consist Movement | 0.0 | 0.0 | 50.0 | 50.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Load Tests: |  |  |  |  |  |  |  |  |  |  |
| 10-Minute | 0.0 | 20.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 80.0 |
| 15-Minute | 0.0 | 33.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 66.7 |
| 30-Minute | 0.0 | 33.3 | 33.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 33.3 |

To accomplish this, UPRR reviewed the types of databases available for its operations to identify where explicit emission-related activity information could be generated for the Davis Yard. UPRR
operates approximately 7000 locomotives over a network spanning 23 states. Large amounts of data are generated and retained by UPRR for management purposes. These include tracking the location and status of capital assets (e.g., locomotives and rail cars), tracking performance of specific activities, and managing operations. These databases can be queried for data records specific to the Davis Yard, but their content does not directly relate to emissions. Where possible, data providing a complete record of emissions-related events (e.g., locomotive arrivals and departures) were identified and retrieved. Where 100 percent data for an activity could not be obtained (e.g., locomotive model number for each arriving locomotive), distributions were developed based on available data. In some cases, data are not available for specific types of emission events (e.g., the duration of idling for individual trains prior to departure). In these cases, UPRR yard personnel were consulted to derive estimates of averages or typical operating practices.

## Railyard Operations - Inbound and Outbound Trains

The majority of locomotive activity in a railyard arises from inbound and outbound freight traffic. Following arrival, consists are decoupled from their trains in receiving areas and are either taken directly to outbound trains, or more commonly, are sent through servicing which can include washing, sanding, oiling, and minor maintenance prior to connecting to outbound trains. Some fraction of trains arriving at a yard simply pass through, possibly stopping briefly for a crew change. UPRR maintains a database that, when properly queried, can produce detailed information regarding both arriving and departing trains. Table 2 lists some of the key parameters that are available in this database. In this study, 12 months of data were obtained for all trains passing through the Davis Yard. The extracted data (over 60,000 records) included at least one record for every arriving and departing train, and each record contained specific information about a single locomotive, as well as other data for the train as a whole. The data were processed using a commercial relational database program and special purpose FORTRAN code to identify individual train arrivals and departures and train and consist characteristics.

Table 2. Selected Train Database Parameters.

|  | Used to Identify |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Parameter | Identification of <br> Train Events | Location in <br> Railyard | Consist <br> Composition | Temporal <br> Profile | Train <br> Characteristics |
| Train Symbol | X | X |  |  |  |
| Train Section | X |  |  |  |  |
| Train Date | X |  |  |  |  |
| Arrival or <br> Departure | X | X |  |  |  |
| Originating or <br> Terminating | X | X |  |  |  |
| Direction |  | X |  |  |  |
| Crew Change? |  | X |  | X |  |
|  <br> Departure Times |  |  |  |  |  |
| \# of Locomotives |  |  | X |  |  |
| \# of Working <br> Locomotives |  |  | X |  |  |
| Trailing Tons |  |  | X |  |  |
| Locomotive ID \# |  |  | X |  |  |
| Locomotive Model |  |  |  |  |  |

The parameters listed in Table 2 were used to calculate the number of trains by time of day arriving or departing from each area of the yard, as well as average composition of their consists (number of locomotives and distribution of locomotive models). The combination of train symbol, train segment, and train date provided a unique identifier for a single arrival or departure, and the individual locomotive models were tabulated to generate model distributions. Where necessary, working horsepower and total horsepower were used to estimate the number of working locomotives in the consist.

Emission calculations associated with inbound and outbound trains included both periods of movement within the yard boundaries and locomotive idling while consists we connected to their trains. Based on train direction and the location of its arrival or departure, moving emissions were based on calculations of time at different throttle settings based on distance traveled and estimated speed profiles, considering speed limits on different tracks. Yard operators provided estimates for the average duration of such idling for both inbound and outbound trains.

## Railyard Operations - Classification

On arrival, inbound trains are "broken" into sections of rail cars destined for different outgoing trains. Figure 1 shows a schematic diagram of the Davis Yard including a large central "bowl" consisting of a large number of parallel tracks connected by automated switching controls to a single track to the west. Trains are pulled back to the west and then pushed to the "hump," a slightly elevated portion of track just west of the bowl. As cars pass over the hump, they are disconnected and roll by gravity into the appropriate track in the bowl. Dedicated special purpose locomotives, known as "hump sets," are used in this operation. Unlike most locomotives, these units have continuously variable throttles, rather than discrete throttle notch settings, to allow precise control of speed approaching the hump. Switching locomotives, known as "trim sets" are responsible for retrieving the train segments or trains being "built" in the bowl and moving them to the appropriate outbound track. The Davis Yard operates a fixed number of hump sets and trim sets at any given time, with backup sets standing by for shift changes and possible breakdowns.

Figure 1. Schematic of the J. R. Davis Yard.


Emission calculations for hump and trim operations were based on the number of working hump and trim sets at any given time, plus assumed idling times of standby units. For the hump sets, yard operators provided estimates of average pull-back and pushing times, and the duty cycles associated with these operations. For pull-back, based on distance and speed limits, the EPA switcher duty cycle,
excluding notch 7 and 8 was used. Pushing is conducted at the equivalent of notch 2 . For the trim sets, speed limits within the Yard preclude any high throttle setting operation, but there is a greater time spent in mid-throttle settings than reflected in the EPA switcher cycle. A revised duty cycle was developed for these units based on the EPA switcher duty cycle, with high throttle fractions (notches 7 and 8) excluded, but with increased notch 1 and notch 4 operating time. These duty cycles are also shown in Table 1.

## Railyard Operations - Consist Movement, Service, Repair and Testing

After disconnecting from inbound trains, consists move to one of several servicing locations for refueling and other maintenance, following designated routes in the yard. Typically, one locomotive in each consist will pull the others, with throttle settings at notch 1 or 2 . Based on distance and speed limits, movement times were estimated for each route, and emissions calculated using the number of locomotives following each route.

While being serviced, locomotives may be either idling or shut down. Locomotives must be idling while oil and other routine checks are performed. In addition, since locomotive engines are water-cooled and do not use antifreeze, they are commonly left idling during cold weather conditions. New idling reduction technologies known as SmartStart and AESS provide computer-controlled engine shut down and restart as necessary, considering temperature, air pressure, battery charge, and other parameters. Yard personnel provided estimates of the average potential duration of idling associated with different servicing events. Databases for service and maintenance activities maintained by UPRR provide details on the number and types of service events at different locations in the yard. As for train activity, these data were processed with a commercial relational database program and special purpose FORTRAN code to characterize and tabulate service events. These results were used in conjunction with data for the number of inbound and outbound consists to estimate total idling emissions for different service event types and locations. Following service, consists are dispatched to outbound trains. The same procedures were followed for estimating idle time, number of locomotives moving to each outbound area of the yard, and the duration of each movement for emission calculations.

In addition to routine service, the databases include service codes indicating periodic inspections of various types, as well as major maintenance activities requiring load testing of stationary locomotives. Several types of load tests are conducted, including planned maintenance pre- and post-tests, quarterly maintenance tests, and unscheduled maintenance diagnostic and post-repair tests. Depending on the test type and locomotive model, these tests include some period of idling, notch 1 operation, and notch 8 operation. Data are not collected on the exact duration of individual tests, so estimates of average duration for each throttle setting were provided by shop personnel, as shown in Table 1. The number of tests of each type for each locomotive model group were tabulated based on the service codes in the database for each service event.

## Trends in Activity and Technology

The initial study was based on data from December 1999 through November 2000. Since that time, UPRR's locomotive fleet modernization program as well as changes in freight volumes have occurred. A subsequent data retrieval for the period from May 2003 through April 2004 was made, and emission calculations updated. A number of significant changes occurred over this 40-month period. The distribution of locomotive models in line-haul operation showed a substantial shift from older, lower horsepower units to new high horsepower units. The average number of locomotives per consist remained the same at about 3, but the higher horsepower allowed an increase in train capacity (trailing tons per train). The decrease in older units also resulted in a decrease in the frequency of major maintenance load testing. In addition to updating activity inputs (number of locomotives by model) for
emission calculations, calculations were modified to reflect the penetration of new and retrofit technologies in the locomotive fleet, including SmartStart and AESS idling controls and Tier 0 and Tier 1 locomotives. UPRR data identifying the specific technologies installed on individual locomotives were matched with locomotive ID numbers in the train and servicing data retrievals to obtain a specific count of the number of locomotives of each model for which emissions reductions were achieved by these technologies. Historical temperature data for the Roseville area were used to estimate the fraction of time computer controls would require idling when the locomotive would otherwise be shut down.

## EMISSION FACTORS

## Data Sources

The study of the J. R. Davis Yard focused on diesel exhaust particulate matter emissions. At present, there is no unified database of emission test results for in-use locomotives. Appendix B of the USEPA's Regulatory Support Document for setting new emission standards for locomotives ${ }^{2}$ contains a compilation of notch-specific emission factors. These data were supplemented by test data reported by Southwest Research Institute ${ }^{3,4}$, as well as test data provided by locomotive manufacturers to assemble emission factors for each of 11 locomotive model groups.

There are dozens of specific locomotive model designations, and emissions tests are not available for all of them. However many models are expected to have nearly identical emission characteristics. Depending on their intended use, locomotives of different models may have different configurations (e.g., number of axles), but share a common diesel engine. For this project, 11 locomotive model groups were defined based on their engine models (manufacturer, horsepower, number of cylinders, and turbo- or super-charging of intake air). Table 3 lists these model groups and some of the typical locomotive models assigned to each group.

Table 3. Locomotive Model Groups

| Model Group | Engine Family | Representative Models |
| :---: | :---: | :---: |
| Switchers | EMD 12-645E | GP-15, SW1500 |
| GP-3x | EMD 16-645E | GP-30, GP-38 |
| GP-4x | EMD 16-645E3B | GP-40, SD-40-2, SD-45-2 |
| GP-50 | EMD 16-645F3B | GP-50, SD-50M |
| GP-60 | EMD 16-710G3A | GP-60, SD-60M |
| SD-7x | EMD 16-710G3B | SD-70MAC, SD-75 |
| SD-90 | EMD 16V265H | SD-90AC, SD-90-43AC |
| Dash-7 | GE7FDL (12 cyl) | B23-7, B30-7, C36-7 |
| Dash-8 | GE7FDL (12 or 16 cyl) | B39-8, B40-8, C41-8 |
| Dash-9 | GE7FDL (16 cyl) | C44-9, C44AC |
| C60-A | GE7HDL | C60AC |

## Emission Factors and Fuel Effects

Figure 2 shows particulate matter (PM) emission factors for several of the more common locomotive model groups at the low to intermediate throttle settings typical of yard operations. As shown in the figure, emission rates generally increase with throttle setting. However, the older 3000 hp GP-4x series shows emissions comparable to (and in some cases, higher than) the newer 4000 to 4500 hp SD-7x and Dash-9 models. Due to the relatively large fraction of time locomotives spend at low throttle settings while in railyards, the relative differences in emission rates between models at these settings can significantly affect emissions estimates if locomotive model distributions change over time.

Figure 2. Locomotive PM Emission Factors (g/hr).


The emission factors used were based on tests using fuel typical of national off-road diesel. Initial emission estimates were derived by multiplying model-specific $\mathrm{g} / \mathrm{hr}$ emission rates by the total hours of operation and locomotive model fraction for each activity within the yard. At the Davis Yard, over half of the diesel fuel dispensed to locomotives meets California on-road diesel fuel specifications (so-called "CARB diesel"). To account for the effect of fuel quality on emissions, estimates of the fraction of locally dispensed fuel burned by locomotives in different yard activities were developed. These ranged from 100 percent for hump and trim sets to zero percent for inbound line-haul units prior to refueling. These fractions were multiplied by the fraction of CARB diesel dispensed at the yard and an estimate of 14 percent reduction in PM emissions for locomotives burning CARB diesel to develop fuel effects adjustments for individual activities.

## EMISSION TRENDS

Using the procedures described in the preceding sections, emissions estimates were developed for the December 1999 to November 2000 period, and the May 2003 to April 2004 period. During this period, significant changes in the UPRR locomotive fleet occurred, with the addition of new locomotives and the retirement of older units. Figure 3 shows the locomotive model distributions for all servicing events at the Davis Yard during these two periods. Service events include both the line-haul and local units arriving and departing on trains (which make up the bulk of these events), as well as the hump and trim sets. A significant increase in the relative fraction of high horsepower SD-7x and Dash-9 units is seen, and a corresponding decrease in the fraction of older GP-4x, GP-50, GP-60, Dash-7 and Dash-8 models. In addition to the fleet modernization, tabulations of specific emission control technologies on units serviced at the Davis Yard showed substantial penetration of new and retrofit
technologies. Approximately 31 percent of locomotives serviced at the yard were equipped with computer-controlled shut-down and restart technology, resulting in reduced idling times. Also, approximately 27 percent of servicings were for Tier 0 locomotives, and approximately 25 percent were Tier 1 units. Although the Tier 0 and Tier 1 technologies are not expected to substantially reduce PM emissions, their nitrogen oxides emissions are lower. A few prototype Tier 2 units were observed in 2003-2004 data, and their reduced PM emissions will show benefits in the future.

Figure 3. Changes in Locomotive Model Distributions.


The freight volume passing through the yard also changed between these periods. Table 4 lists the percent change in the number of arriving and departing trains, locomotives, and trailing tons (a measure of freight volume). The number of trains and locomotives showed little change, however the trailing tons increased by approximately 15 percent, implying that the average train weight (and correspondingly, the required consist horsepower) increased. This is a result of the increased availability of high horsepower units in the UPRR fleet. A higher fraction of trains bypass the yard, either not stopping, or stopping only for crew changes.

Table 4. Percent Change in Yard Activity Levels from 12/1999-11/2000 to 5/2003-4/2004.

|  | Trains | Locomotives | Trailing Tons |
| :---: | :---: | :---: | :---: |
| Arrivals | $-5.2 \%$ | $-3.5 \%$ | -- |
| Departures | $-7.0 \%$ | $-7.3 \%$ | -- |
| Throughs (Bypassing the yard) | $8.0 \%$ | $6.8 \%$ | -- |
| Total Arrivals and Departures | $-0.3 \%$ | $-0.9 \%$ | $15.1 \%$ |

The newer locomotive fleet also affected the level of load testing activity required. Table 5 lists the percent change in the number of load tests of different types, and the corresponding change in total locomotive testing time at idle, notch 1 , and notch 8 . The extended 30 -minute post-maintenance tests were substantially reduced, and total hours of testing were reduced for the various throttle settings between 12 and 43 percent.

Table 5. Percent Change in Load Test Activity from 12/1999-11/2000 to 5/2003-4/2004.

| 10-Minute Tests | $-18.9 \%$ |
| :---: | :---: |
| 15-Minute Tests | $14.6 \%$ |
| 30-Minute Tests | $-43.2 \%$ |
| Total Tests | $-12.3 \%$ |
| Idling Hours | $-20.6 \%$ |
| Notch 1 Hours | $-43.2 \%$ |
| Notch 8 Hours | $-12.0 \%$ |

The combined net result of these changes is shown in Table 6. Between November 2000 and April 2003, total estimated PM emissions in the yard decreased by approximately 15 percent. Reductions in idling and movement emissions of about 20 percent were calculated, due to the combination of a newer, lower emitting locomotive fleet and the computer-controlled shutdown technologies (both retrofits and standard equipment on newer units). Hump and trim emissions were reduced by about 6 percent, and load testing emissions by about 14 percent.

Table 6. Emissions Changes from 12/1999-11/2000 to 5/2003-4/2004.

|  | Estimated Emissions (tons per year) |  | Percent Change |
| :---: | :---: | :---: | :---: |
|  | $\mathbf{1 2 / 1 9 9 9}-\mathbf{1 1 / 2 0 0 0}$ | $\mathbf{5 / 2 0 0 3}-\mathbf{4 / 2 0 0 4}$ |  |
| Idling and Movement of Trains | 5.2 | 4.2 | $-20.3 \%$ |
| Idling and Movement of Consists | 8.5 | 6.8 | $-20.2 \%$ |
| Testing | 1.5 | 1.3 | $-14.1 \%$ |
| Hump and Trim | 7.0 | 6.6 | $-5.7 \%$ |
| Total | 22.3 | 18.9 | $-15.3 \%$ |

## CONCLUSIONS

Because of the unique features of each individual railyard, top-down methods (e.g., based only on tons of freight handled or number of arriving locomotives) cannot provide reliable estimates of railyard emissions. Yard-specific data are needed. In-yard activity patterns (and emissions) will vary between yards depending on factors such as: the type of yard (e.g., hump or flat switching classification yards, or intermodal facilities); the presence and capabilities of service tracks or locomotive repair shops; the types of freight handled; the location of the yard in the rail network; and yard configuration. The development of procedures for retrieving and analyzing activity data and locomotive characteristics for a specific railyard is a substantial improvement of alternatives based on top-down estimation. By obtaining disaggregate data for the range of specific activities occurring within railyards, it is possible to reliably estimate historical trends in emissions, as well as to evaluate the potential effects of operational changes and new technologies. Railyard operations cannot be treated in isolation, since these yards are only one component of complex national level systems. Nevertheless, the ability to assess the details of yard operations and their emissions provides an improved basis for environmental management decisions at both local and larger scales.

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## KEY WORDS

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## APPENDIX A-7

## SULFUR ADJUSTMENT CALCULATIONS

## Appendix A-7

## Development of Adjustment Factors for Locomotive DPM Emissions Based on Sulfur Content

Wong (undated) provides equations for estimating $\mathrm{g} / \mathrm{bhp}$-hr emission rates for 4 -Stroke (GE) and 2-Stroke (EMD) locomotives. Rather than using these statistically derived estimates for absolute emissions when model- and notch-specific emission factors are available, we used these equations to develop relative emission rate changes for different sulfur levels. The basic form of the equation is

$$
q=a \cdot S+b
$$

Where,
$q$ is the predicted $\mathrm{g} / \mathrm{bhp}$-hr emission rate of a locomotive at a specific throttle setting and sulfur content;
$a$ and $b$ are coefficients specific to a locomotive type (2- or 4-stroke) and throttle notch; and
$S$ is the fuel sulfur content in ppm.
Thus, to calculate the emission adjustment factor for a specific fuel sulfur content, it is necessary to calculate the nominal emission rate $q_{0}$ for the baseline fuel sulfur content $S_{0}$, and the emission rate $q_{i}$ for the fuel of interest with sulfur content $S_{i}$. This adjustment factor $k_{i}$ is simply

$$
k_{i}=1 \frac{\left(q_{0} q_{i}\right)}{q_{0}}
$$

Where, $q_{0}$ and $q_{i}$ are calculated using the equation above. Tables 1 and 2 give the values of the $a$ and $b$ coefficients for 4 -stroke and 2 -stroke locomotives. For throttle settings below notch 3, sulfur content is not expected to affect emission rates. The baseline emission rates from which actual emissions are estimated were derived from emission tests of different locomotive models. Although full documentation of fuels is not available for all of these tests, they are assumed to be representative of actual emissions of the different models running on $3,000 \mathrm{ppm}$ sulfur EPA non-road Diesel fuel. For the purposes of modeling 2005 emissions, these factors are needed to adjust the baseline emission factors to emission factors representative of two fuels -221 ppm and 2639 ppm . Table 3 shows the resulting correction factors for these two fuels by notch and engine type. To generate locomotive model-, throttle-, tier-, and fuel-specific emission factors, the base case (nominal $3,000 \mathrm{ppm} \mathrm{S}$ ) emission factors in Table 4 were multiplied by the corresponding correction factors for throttle settings between notch 3 and notch 8 .

| Table 1 |  |  |
| :---: | :---: | :---: |
| Sulfur Correction Coefficients for 4-Stroke Engines |  |  |
| Throttle Setting | $\boldsymbol{a}$ | $\boldsymbol{b}$ |
| Notch 8 | 0.00001308 | 0.0967 |
| Notch 7 | 0.00001102 | 0.0845 |
| Notch 6 | 0.00000654 | 0.1037 |
| Notch 5 | 0.00000548 | 0.1320 |
| Notch 4 | 0.00000663 | 0.1513 |
| Notch 3 | 0.00000979 | 0.1565 |

Table 2
Sulfur Correction Coefficients for 2-Stroke Engines

| Throttle Setting | $\boldsymbol{a}$ | $\boldsymbol{b}$ |
| :---: | :---: | :---: |
| Notch 8 | 0.0000123 | 0.3563 |
| Notch 7 | 0.0000096 | 0.2840 |
| Notch 6 | 0.0000134 | 0.2843 |
| Notch 5 | 0.0000150 | 0.2572 |
| Notch 4 | 0.0000125 | 0.2629 |
| Notch 3 | 0.0000065 | 0.2635 |


| Table 3 <br> DPM Emission Adjustment Factors for Different Fuel Sulfur Levels |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Throttle Setting | 4-Stroke (GE) |  | 2-Stroke (EMD) |  |
|  | 2,639 ppm S | 221 ppm S | 2,639 ppm S | 221 ppm S |
| Notch 8 | 0.9653 | 0.7326 | 0.9887 | 0.9131 |
| Notch 7 | 0.9662 | 0.7395 | 0.9889 | 0.9147 |
| Notch 6 | 0.9809 | 0.8526 | 0.9851 | 0.8852 |
| Notch 5 | 0.9867 | 0.8974 | 0.9821 | 0.8621 |
| Notch 4 | 0.9860 | 0.8924 | 0.9850 | 0.8844 |
| Notch 3 | 0.9810 | 0.8536 | 0.9917 | 0.9362 |


| Table 4Base Case Locomotive Diesel Particulate Matter Emission Factors (g/hr)(3,000 PPM Sulfur Assumed) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model Group | Tier | Throttle Setting |  |  |  |  |  |  |  |  |  | Source |
|  |  | Idle | DB | N1 | N2 | N3 | N4 | N5 | N6 | N7 | N8 |  |
| Switchers | N | 31.0 | 56.0 | 23.0 | 76.0 | 138.0 | 159.0 | 201.0 | 308.0 | 345.0 | 448.0 | EPA RSD ${ }^{1}$ |
| GP-3x | N | 38.0 | 72.0 | 31.0 | 110.0 | 186.0 | 212.0 | 267.0 | 417.0 | 463.0 | 608.0 | EPA RSD ${ }^{1}$ |
| GP-4x | N | 47.9 | 80.0 | 35.7 | 134.3 | 226.4 | 258.5 | 336.0 | 551.9 | 638.6 | 821.3 | EPA RSD ${ }^{1}$ |
| GP-50 | N | 26.0 | 64.1 | 51.3 | 142.5 | 301.5 | 311.2 | 394.0 | 663.8 | 725.3 | 927.8 | EPA RSD ${ }^{1}$ |
| GP-60 | N | 48.6 | 98.5 | 48.7 | 131.7 | 284.5 | 299.4 | 375.3 | 645.7 | 743.6 | 941.6 | EPA RSD ${ }^{1}$ |
| GP-60 | 0 | 21.1 | 25.4 | 37.6 | 75.5 | 239.4 | 352.2 | 517.8 | 724.8 | 1125.9 | 1319.8 | SwRI ${ }^{2}$ (KCS733) |
| SD-7x | N | 24.0 | 4.8 | 41.0 | 65.7 | 156.8 | 243.1 | 321.1 | 374.8 | 475.2 | 589.2 | SwRI ${ }^{3}$ |
| SD-7x | 0 | 14.8 | 15.1 | 36.8 | 61.1 | 230.4 | 379.8 | 450.8 | 866.2 | 1019.1 | 1105.7 | $\mathrm{GM} \mathrm{EMD}^{4}$ |
| SD-7x | 1 | 29.2 | 31.8 | 37.1 | 66.2 | 219.3 | 295.9 | 436.7 | 713.2 | 783.2 | 847.7 | SwRI ${ }^{5}$ (NS2630) |
| SD-7x | 2 | 55.4 | 59.5 | 38.3 | 134.2 | 271.7 | 300.4 | 335.2 | 551.5 | 672.0 | 704.2 | SwRI ${ }^{5}$ (UP8353) |
| SD-90 | 0 | 61.1 | 108.5 | 50.1 | 99.1 | 255.9 | 423.7 | 561.6 | 329.3 | 258.2 | 933.6 | GM EMD ${ }^{4}$ |
| Dash 7 | N | 65.0 | 180.5 | 108.2 | 121.2 | 359.5 | 327.7 | 331.5 | 299.4 | 336.7 | 420.0 | EPA RSD ${ }^{1}$ |
| Dash 8 | 0 | 37.0 | 147.5 | 86.0 | 133.1 | 291.4 | 293.2 | 327.7 | 373.5 | 469.4 | 615.2 | $\mathrm{GE}^{4}$ |
| Dash 9 | N | 32.1 | 53.9 | 54.2 | 108.1 | 219.9 | 289.1 | 370.6 | 437.7 | 486.1 | 705.7 | SWRI 2000 |
| Dash 9 | 0 | 33.8 | 50.7 | 56.1 | 117.4 | 229.2 | 263.8 | 615.9 | 573.9 | 608.0 | 566.6 | Average of GE \& SwRI ${ }^{6}$ |
| Dash 9 | 1 | 16.9 | 88.4 | 62.1 | 140.2 | 304.0 | 383.5 | 423.9 | 520.2 | 544.6 | 778.1 | SwRI ${ }^{2}$ (CSXT595) |
| Dash 9 | 2 | 7.7 | 42.0 | 69.3 | 145.8 | 304.3 | 365.0 | 405.2 | 418.4 | 513.5 | 607.5 | $\mathrm{SwRI}^{2}$ (BNSF 7736) |
| C60-A | 0 | 71.0 | 83.9 | 68.6 | 78.6 | 277.9 | 234.1 | 276.0 | 311.4 | 228.0 | 362.7 | GE ${ }^{4}$ (UP7555) |
| 1. EPA Regulatory Support Document, "Locomotive Emissions Regulation," Appendix B, $12 / 17 / 97$, as tabulated by ARB and ENVIRON <br> 2. Base emission rates provided by ENVIRON as part of the BNSF analyses for the Railyard MOU (Personal communication from Chris Lindhjem Ireson, 2006) based on data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to C. Lindhjem, 2006) <br> 3. SwRI final report "Emissions Measurments - Locomotives" by Steve Fritz, August 1995. <br> 4. Manufacturers' emissions test data as tabulated by ARB. <br> 5. Base SD-70 emission rates taken from data produced in the AAR/SwRI Exhaust Plume Study (Personal communication from Steve Fritz to R. Ir 2006). <br> 6. Average of manufacturer's emissions test data as tabulated by ARB and data from the AAR/SwRI Exhaust Plume Study, tabulated and calculate ENVIRON.. |  |  |  |  |  |  |  |  |  |  |  |  |

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## OFFROAD Modeling Change Technical Memo

SUBJECT: Changes to the Locomotive Inventory
LEAD: Walter Wong

## Summary

The statewide locomotive emission inventory has not been updated since 2002. Using the Booz-Allen Hamilton's (BAH) study (Locomotive Emission Study) published in 1992 as a guideline (summary of inventory methodology can be found in Appendix A), staff updated the locomotive inventory.

The history of locomotive emission inventory updates began in 1992 using the results from the BAH report as the baseline inventory. In 2003, staff began updating the emissions inventory by revising the growth assumptions used in the inventory. The revised growth factors were incorporated into the ARB's 2003 Almanac Emission Inventory. With additional data, staff is proposing further update to the locomotive inventory to incorporate fuel correction factors, add passenger train data and Class III locomotives. Changes from updated locomotive activity data have made a significant impact on the total inventory (see Table 1).

Table 1. Impact of Changes on Statewide Locomotive Inventory

|  | Pre 2003 ARB <br> Almanac Inventory <br> (tons/day) |  |  | Revised Inventory <br> (tons/day) |  |  | Difference <br> (tons/day) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | HC | NOx | PM | HC | NOx | PM | HC | NOx | PM |
| 1987 | 7.2 | 158.8 | 3.6 | 7.2 | 158.8 | 3.6 | 0.0 | 0.0 | 0.0 |
| 2000 | 7.2 | 144.8 | 2.8 | 9.8 | 207.2 | 4.7 | 2.6 | 62.4 | 1.9 |
| 2010 | 7.2 | 77.8 | 2.8 | 9.5 | 131.9 | 4.2 | 2.3 | 54.1 | 1.4 |
| 2020 | 7.2 | 77.8 | 2.8 | 9.4 | 134.6 | 4.1 | 2.2 | 56.8 | 1.3 |

## Reasons For Change

During the 2003 South Coast's State Implementation Plan (SIP) development process, industry consultants approached Air Resources Board (ARB) staff to refine the locomotive emissions inventory. Specifically, their concerns were related to the growth factors and fuel correction factors used in the inventory

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calculations. This document outlines how the locomotive emissions inventory was updated and the subsequent changes made to address industry's concerns.

## Background : Baseline 1987 Locomotive Emissions Inventory (BAH report)

Locomotive operations can be characterized by the type of service performed. For emission inventory purposes, locomotives are classified into five different service types as defined in BAH's report.

Line-haul/intermodal - Intermodal locomotives generally operate at higher speeds and with higher power than other types and incorporate modern, high-speed engines.

Mixed/bulk - Mixed locomotives are the most common and operate with a wide range of power. They also perform line-haul duties.

Local/Short Haul - Local locomotives perform services that are a mixture of mixed freight and yard service. They operate with lower power and use older horsepower engines.

Yard/Switcher - Yard operations are used in switching locomotives and characterized by stop and start type movements. They operate with smaller engines and have the oldest locomotive engines.

Passenger - Passenger locomotives are generally high speed line haul type operations.

Categories of railroads are further explained by a precise revenue-based definition found in the regulations of the Surface Transportation Board (STB). Rail carriers are grouped into three classes for the purposes of accounting and reporting:

Class I -Carriers with annual operating revenues of $\$ 250$ million or more
Class II - Carriers with annual operating revenues of less than \$250 million but in excess of $\$ 20$ million

Class III - Carriers with annual operating revenues of less than $\$ 20$ million or less, and all switching companies regardless of operating revenues.

The threshold figures are adjusted annually for inflation using the base year of 1991.

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The 1987 locomotive inventory as shown in Table 2 is taken from the BAH report prepared for the ARB entitled "Locomotive Emission Study" completed in 1992 (http://www.arb.ca.gov/app/library/libcc.php). Information was gathered from many sources including ARB, the South Coast Air Quality Management District, the California Energy Commission, the Association of American Railroads (AAR), locomotive and large engine manufacturers, and Southwest Research Institute. Railroad companies, such as Southern Pacific, Union Pacific, and Atchison, Topeka and Santa Fe (ATSF), provided emission factors, train operation data, and throttle position profiles for trains operating in their respective territories. Southwest Research Institute provided emission test data.

Table 2. 1987 Locomotive Inventory in Tons Per Day, Statewide, BAH report

| TYPE | HC | CO | NOX | PM | SOX |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Line-Haul/Intermodal | 3.97 | 12.89 | 86.21 | 1.97 | 6.36 |
| Short-Haul/Local | 0.96 | 3.06 | 21.30 | 0.46 | 1.59 |
| Mixed | 1.51 | 4.85 | 37.34 | 0.81 | 2.76 |
| Passenger | 0.10 | 0.22 | 3.24 | 0.07 | 0.30 |
| Yard/Switcher | 0.62 | 1.57 | 10.69 | 0.24 | 0.58 |
| Total | 7.16 | 22.59 | 158.78 | 3.55 | 11.59 |

The assumed average fuel sulfur content is 2700 parts per million (ppm) obtained from the BAH report.

## Current Growth Estimates

Prior to the 2003 South Coast SIP update, growth factors were based on employment data in the railroad industry. Staff believes that the use of historic employment data, which translates to a decline in emissions in future years, may be masking actual positive growth in locomotive operations. It may be assumed that the number of employees is declining due to increased efficiency.

## Changes to the Locomotive Inventory

## Summary of Growth in Emission Based on BAH Report

Growth is estimated based on train operation type and by several operating characteristics.

Increased Rail Lube and Aerodynamics - this arises from reduction in friction and will help reduce power requirements.

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Introduction of New Locomotives - older locomotive units will be replaced by newer models.

Changes in Traffic Level - the increase or decrease in railroad activity

In the BAH report, projected emission estimates for years 2000 and 2010 were based on the factors shown in Tables 3 and 4. A substantial part of the locomotive emission inventory forecast is based upon projections of rail traffic levels. BAH projected future rail traffic level as a function of population and economic growth in the state. BAH also projected growth in emission only to 2010.

Table 3. Changes in Emissions from 1987-2000 (Exhibit 4 p. 11 of the 8/92 Locomotive Emission Study Supplement) (1987 Base Year)

| Train |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Operation |  |  |  |  |
| Type | Increased Rail <br> Lube and <br> Aerodynamics | Introduction <br> of New <br> Locomotive | Changes in <br> Traffic <br> Levels | Cumulative <br> Net Growth in <br> Emissions |
| Intermodal | $-7.0 \%$ | $-8.0 \%$ | $17.0 \%$ | $2.0 \%$ |
| Mixed \& Bulk | $-7.0 \%$ | $-8.0 \%$ | $2.0 \%$ | $-13.0 \%$ |
| Local | $-3.0 \%$ | $-3.0 \%$ | $-2.0 \%$ | $-8.0 \%$ |
| Yard | $0.0 \%$ | $-1.0 \%$ | $-25.0 \%$ | $-26.0 \%$ |
| Passenger | $-7.0 \%$ | $-8.0 \%$ | $10.0 \%$ | $-5.0 \%$ |

Table 4. Changes in Emissions from 2001-2010 (Exhibit 4 p. 11 of the 8/92 Locomotive Emission Study Supplement) (2000 Base Year)

| Train <br> Operation <br> Type | Increased Rail <br> Lube and <br> Aerodynamics | Improved <br> Dispatching <br> and Train <br> Control | Introduction <br> of New <br> Locomotive | Changes in <br> Traffic <br> Levels | Cumulative <br> Net Growth in <br> Emissions |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal | $-2.0 \%$ | $-3.0 \%$ | $-8.0 \%$ | $25.0 \%$ | $12.0 \%$ |
| Mixed \& Bulk | $-2.0 \%$ | $-3.0 \%$ | $-8.0 \%$ | $0.0 \%$ | $-13.0 \%$ |
| Local | $-1.0 \%$ | $0.0 \%$ | $-12.0 \%$ | $-10.0 \%$ | $-23.0 \%$ |
| Yard | $0.0 \%$ | $0.0 \%$ | $-10.0 \%$ | $-15.0 \%$ | $-25.0 \%$ |
| Passenger | $-2.0 \%$ | $-3.0 \%$ | $-8.0 \%$ | $15.0 \%$ | $2.0 \%$ |

BAH added "Improved Dispatching and Train Control" to differentiate these impacts from the "Increased Rail Lubing" which helps to improve fuel efficiency from locomotive engines. Since train control techniques are emerging from the

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signal company research work, these assumed changes will not impact emission until year 2000.

Based on industry's input, staff recommends several changes to the locomotive emissions inventory. These include modifying growth factors, making adjustments to control factors reflecting the U. S. EPA regulations that went into effect in year 2000, incorporating fuel correction factors, adding smaller class III railroad and industrial locomotive, and updating passenger data.

## Revised Growth in Emissions

Staff revised the growth factors for locomotives based on new data that better reflect locomotive operations. This includes U.S. industrial production and various railroad statistics available from the AAR.

Based on historic data recently obtained from U.S. industrial productions and the AAR, the changes in traffic levels were revised. A better estimate for changes in traffic levels for locomotives can be made to the line-haul class of railroad, which are the intermodal and mixed and bulk type of locomotives, using industrial production and AAR's data.

Industrial production data is considered to be a surrogate for changes in traffic levels of the line-haul locomotive. It is assumed that railroad activity would increase in order to accommodate the need to move more product. Industrial production is the total output of U.S. factories and mines, and is a key economic indicator released monthly by the Federal Reserve Board. U.S. industrial production historical data from 1920 to 2002 was obtained and analyzed from government sources. Figure 1 shows the historical industrial production trend (Source : http://www.research.stlouisfed.org/fred2/series/INDPRO/3/Max). Statistical analysis was used to derive a polynomial equation to fit the data.

## 



Another surrogate for growth is net ton-miles per engine. Consequently, staff analyzed railroad data from the AAR's Railroad Facts booklet (2001 edition). The booklet contains line-haul railroad statistics including financial status, operation and employment data, and usage profiles. Revenue ton-mile and locomotives in service data from the booklet were used to compute the net tonmiles per engine as shown in Table 5.

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Table 5. Revenue Ton-Miles and Ton-Miles/Engine (AAR Railroad Facts 2001 edition)

| Year | Locomotive <br> Diesel in <br> Service (US) | Revenue Ton- <br> Miles | Ton- <br> Miles/Engine |
| :---: | :---: | :---: | :---: |
| 1987 | 19,647 | 943,747 | 48.04 |
| 1988 | 19,364 | 996,182 | 51.45 |
| 1989 | 19,015 | $1,013,841$ | 53.32 |
| 1990 | 18,835 | $1,033,969$ | 54.90 |
| 1991 | 18,344 | $1,038,875$ | 56.63 |
| 1992 | 18,004 | $1,066,781$ | 59.25 |
| 1993 | 18,161 | $1,109,309$ | 61.08 |
| 1994 | 18,496 | $1,200,701$ | 64.92 |
| 1995 | 18,810 | $1,305,688$ | 69.41 |
| 1996 | 19,267 | $1,355,975$ | 70.38 |
| 1997 | 19,682 | $1,348,926$ | 68.54 |
| 1998 | 20,259 | $1,376,802$ | 67.96 |
| 1999 | 20,254 | $1,433,461$ | 70.77 |
| 2000 | 20,026 | $1,465,960$ | 73.20 |

As shown in Figure 2, there is a relatively good correlation between net ton-miles per engine growth and industrial production. Because net ton-miles per engine data are compiled by the railroad industry and pertains directly to the railroad segment, staff believes that net ton-miles per engine will better characterize future traffic level changes.

Figure 2. Ton-miles/Engine vs. Industrial Production (index base year = 1987)


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The ton-miles/engine data were projected to calculate the future growth rate of traffic level using a linear equation.

Staff also made changes to the "Increased Rail Lube and Aerodynamics" assumption shown in Tables 3 and 4. Rail lubing does not benefit the idling portion of locomotive activity. Since idling contributes $20 \%$ of the weighting in the line-haul duty cycle, staff reduced the rail lubing benefit by $20 \%$. Meanwhile, improved dispatching and train control is assumed only to reduce engine idling. Therefore, staff reduced the improved dispatching benefit by $80 \%$.

The benefit of the introduction of new locomotives to the fleet was decreased from the original BAH assumption. BAH assumed $50 \%$ penetration of the new engines by 2000. Literature research suggests that the new engines accounted for only about 34\% of the fleet in 2000 (www.railwatch.com, http://utahrails.net/all-time/modern-index.php). These new engines are assumed to be $15 \%$ cleaner. Therefore, the benefit from new locomotive engines has been reduced to $5 \%(34 \% \times 15 \%=5 \%$ reduction $)$.

Tables 6, 7, and 8 present the revised growth factors to be used to project the baseline (1987) locomotive emissions inventory into the future.

Table 6. ARB Revised Growth 1987-2000, ARB’s 2003 Almanac
Emission Inventory

| Train |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Operation |  |  |  |  |  |  |
| Type | Increased Rail <br> Lube and <br> Aerodynamics | Introduction <br> of New <br> Locos | Population <br> Increase | Changes in <br> Traffic Levels | Cumulative <br> Net Growth in <br> in | Annual <br> Growth |
| Intermodal | $-5.6 \%$ | $-5.1 \%$ | $1.9 \%$ | $50.0 \%$ | $41.2 \%$ | $2.69 \%$ |
| Mixed \& Bulk | $-5.6 \%$ | $-5.1 \%$ | $1.9 \%$ | $50.0 \%$ | $41.2 \%$ | $2.69 \%$ |
| Local | $-2.4 \%$ | $0 \%$ | $0 \%$ | $-2.0 \%$ | $-4.4 \%$ | $-0.35 \%$ |
| Yard | $0.0 \%$ | $0 \%$ | $0 \%$ | $-25.0 \%$ | $-25.0 \%$ | $-2.19 \%$ |
| Passenger | $-5.6 \%$ | $0 \%$ | $1.9 \%$ | $10.0 \%$ | $6.3 \%$ | $0.47 \%$ |

The benefit of new locomotives with cleaner burning engines is accounted for in the control factor from EPA's regulation beginning in 2001, which takes into account introduction of new locomotive engines meeting Tier I and Tier II standards.

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Table 7. ARB Revised Growth 2001-2010 (2000 Base Year, ARB’s 2003 Almanac Emission Inventory)

| Train <br> Operation <br> Type | Increased Rail <br> Lube and <br> Aerodynamics | Improved <br> Dispatching <br> and Train <br> Control | Changes in <br> Traffic <br> Levels | Cumulative <br> Net Growth in <br> Emissions | Annual <br> Growth |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal | $-1.6 \%$ | $-0.6 \%$ | $22.5 \%$ | $20.3 \%$ | $1.87 \%$ |
| Mixed \& Bulk | $-1.6 \%$ | $-0.6 \%$ | $22.5 \%$ | $20.3 \%$ | $1.87 \%$ |
| Local | $-0.8 \%$ | $-0.6 \%$ | $-10.0 \%$ | $-11.4 \%$ | $-1.20 \%$ |
| Yard | $0.0 \%$ | $0.0 \%$ | $-15.0 \%$ | $-15.0 \%$ | $-1.61 \%$ |
| Passenger | $-1.6 \%$ | $0.0 \%$ | $15.0 \%$ | $13.4 \%$ | $1.27 \%$ |

Table 8. ARB Revised Growth 2010-2020 (2010 Base Year, ARB's 2003 Almanac Emission Inventory)

| Train <br> Operation <br> Type | Increased Rail <br> Lube and <br> Aerodynamics | Improved <br> Dispatching <br> and Train <br> Control | Changes in <br> Traffic <br> Levels | Cumulative <br> Net Growth | Annual <br> Growth |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal | $0.0 \%$ | $0.0 \%$ | $18.0 \%$ | $18.0 \%$ | $1.67 \%$ |
| Mixed \& Bulk | $0.0 \%$ | $0.0 \%$ | $18.0 \%$ | $18.0 \%$ | $1.67 \%$ |
| Local | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.00 \%$ |
| Yard | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.00 \%$ |
| Passenger | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.0 \%$ | $0.00 \%$ |

In Table 8, staff assumes no benefit from aerodynamics and improved train controls. Staff seeks guidance from industry as to their input regarding future benefits.

Table 9. Revised Growth in Emissions (Base Year 1987)

| Year | Intermodal | Mixed \& Bulk | Local | Yard | Passenger |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1987 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 1988 | 1.03 | 1.03 | 1.00 | 0.98 | 1.00 |
| 1989 | 1.05 | 1.05 | 0.99 | 0.96 | 1.01 |
| 1990 | 1.08 | 1.08 | 0.99 | 0.94 | 1.01 |
| 1991 | 1.11 | 1.11 | 0.99 | 0.92 | 1.02 |
| 1992 | 1.14 | 1.14 | 0.98 | 0.90 | 1.02 |
| 1993 | 1.17 | 1.17 | 0.98 | 0.88 | 1.03 |
| 1994 | 1.20 | 1.20 | 0.98 | 0.86 | 1.03 |
| 1995 | 1.24 | 1.24 | 0.97 | 0.84 | 1.04 |
| 1996 | 1.27 | 1.27 | 0.97 | 0.82 | 1.04 |
| 1997 | 1.30 | 1.30 | 0.97 | 0.80 | 1.05 |
| 1998 | 1.34 | 1.34 | 0.96 | 0.78 | 1.05 |
| 1999 | 1.38 | 1.38 | 0.96 | 0.77 | 1.06 |
| 2000 | 1.41 | 1.41 | 0.96 | 0.75 | 1.06 |
| 2001 | 1.44 | 1.44 | 0.94 | 0.74 | 1.08 |
| 2002 | 1.47 | 1.47 | 0.93 | 0.73 | 1.09 |
| 2003 | 1.49 | 1.49 | 0.92 | 0.71 | 1.10 |
| 2004 | 1.52 | 1.52 | 0.91 | 0.70 | 1.12 |
| 2005 | 1.55 | 1.55 | 0.90 | 0.69 | 1.13 |
| 2006 | 1.58 | 1.58 | 0.89 | 0.68 | 1.15 |
| 2007 | 1.61 | 1.61 | 0.88 | 0.67 | 1.16 |
| 2008 | 1.64 | 1.64 | 0.87 | 0.66 | 1.18 |
| 2009 | 1.67 | 1.67 | 0.86 | 0.65 | 1.19 |
| 2010 | 1.70 | 1.70 | 0.85 | 0.64 | 1.21 |
| 2011 | 1.73 | 1.73 | 0.85 | 0.64 | 1.21 |
| 2012 | 1.76 | 1.76 | 0.85 | 0.64 | 1.21 |
| 2013 | 1.79 | 1.79 | 0.85 | 0.64 | 1.21 |
| 2014 | 1.81 | 1.81 | 0.85 | 0.64 | 1.21 |
| 2015 | 1.85 | 1.85 | 0.85 | 0.64 | 1.21 |
| 2016 | 1.88 | 1.88 | 0.85 | 0.64 | 1.21 |
| 2017 | 1.91 | 1.91 | 0.85 | 0.64 | 1.21 |
| 2018 | 1.94 | 1.94 | 0.85 | 0.64 | 1.21 |
| 2019 | 1.97 | 1.97 | 0.85 | 0.64 | 1.21 |
| 2020 | 2.00 | 2.00 | 0.85 | 0.64 | 1.21 |

## Control Factors for U.S. EPA regulation

In December 1997, the U.S. EPA finalized the locomotive emission standard regulation. The regulatory support document lists the control factors used (http://www.epa.gov/otaq/regs/nonroad/locomotv/frm/locorsd.pdf). Staff modified the control factors to incorporate the existing memorandum of understanding (http://www.arb.ca.gov/msprog/offroad/loco/loco.htm) between the South Coast AQMD and the railroads that operate in the region. Previously, one control factor was applied statewide. In the revised emissions inventory starting in 2010, a lower control factor reflecting the introduction of lower emitting locomotive

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engines in the SCAB region was applied. Tables 10 and 11 show the revised control factors. Road hauling definition as used by U.S. EPA applies to the linehaul/intermodal, mixed, and local/short haul train type in the emissions inventory.

Table 10. Revised Statewide Control Factors

|  | State <br> Road <br> Hauling <br> HC | State <br> Road <br> Hauling <br> NOx | State <br> Road <br> Hauling <br> PM | State <br> Switcher <br> HC | State <br> Switcher <br> NOx | State <br> Switcher <br> PM | State <br> Passenger <br> HC | State <br> Passenger <br> NOx | State <br> Passenger |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1999 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2000 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2001 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2002 | 1.00 | 0.88 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 |
| 2003 | 1.00 | 0.82 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.96 | 1.00 |
| 2004 | 1.00 | 0.75 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.94 | 1.00 |
| 2005 | 0.96 | 0.68 | 0.96 | 0.99 | 0.93 | 0.99 | 0.98 | 0.92 | 0.98 |
| 2006 | 0.92 | 0.62 | 0.92 | 0.99 | 0.91 | 0.99 | 0.96 | 0.90 | 0.96 |
| 2007 | 0.89 | 0.59 | 0.89 | 0.98 | 0.89 | 0.98 | 0.94 | 0.83 | 0.94 |
| 2008 | 0.87 | 0.57 | 0.86 | 0.98 | 0.87 | 0.97 | 0.92 | 0.76 | 0.92 |
| 2009 | 0.84 | 0.55 | 0.84 | 0.97 | 0.85 | 0.97 | 0.91 | 0.69 | 0.90 |
| 2010 | 0.82 | 0.54 | 0.81 | 0.96 | 0.83 | 0.96 | 0.89 | 0.62 | 0.88 |
| 2011 | 0.81 | 0.53 | 0.80 | 0.96 | 0.81 | 0.95 | 0.87 | 0.57 | 0.87 |
| 2012 | 0.80 | 0.53 | 0.79 | 0.95 | 0.79 | 0.94 | 0.85 | 0.56 | 0.85 |
| 2013 | 0.79 | 0.52 | 0.78 | 0.94 | 0.77 | 0.93 | 0.83 | 0.54 | 0.83 |
| 2014 | 0.77 | 0.51 | 0.76 | 0.94 | 0.75 | 0.93 | 0.82 | 0.53 | 0.81 |
| 2015 | 0.76 | 0.50 | 0.75 | 0.93 | 0.73 | 0.92 | 0.80 | 0.52 | 0.79 |
| 2016 | 0.75 | 0.50 | 0.74 | 0.92 | 0.71 | 0.91 | 0.78 | 0.51 | 0.77 |
| 2017 | 0.74 | 0.49 | 0.72 | 0.91 | 0.70 | 0.90 | 0.76 | 0.50 | 0.75 |
| 2018 | 0.73 | 0.48 | 0.71 | 0.90 | 0.69 | 0.89 | 0.74 | 0.49 | 0.73 |
| 2019 | 0.71 | 0.48 | 0.70 | 0.89 | 0.68 | 0.88 | 0.73 | 0.48 | 0.71 |
| $2020+$ | 0.70 | 0.47 | 0.69 | 0.89 | 0.67 | 0.87 | 0.71 | 0.47 | 0.69 |

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Table 11. Revised SCAB Control Factors

|  | SCAB <br> Road <br> Hauling <br> HC | SCAB <br> Road <br> Hauling <br> NOx | SCAB <br> Road <br> Hauling <br> PM | SCAB <br> Switcher <br> HC | SCAB <br> Switcher | SCAB <br> Switcher |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1999 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2000 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2001 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 |
| 2002 | 1.00 | 0.88 | 1.00 | 1.00 | 0.98 | 1.00 |
| 2003 | 1.00 | 0.82 | 1.00 | 1.00 | 0.97 | 1.00 |
| 2004 | 1.00 | 0.75 | 1.00 | 1.00 | 0.95 | 1.00 |
| 2005 | 0.96 | 0.68 | 0.96 | 0.99 | 0.93 | 0.99 |
| 2006 | 0.92 | 0.62 | 0.92 | 0.99 | 0.91 | 0.99 |
| 2007 | 0.89 | 0.59 | 0.89 | 0.98 | 0.89 | 0.98 |
| 2008 | 0.87 | 0.57 | 0.86 | 0.98 | 0.87 | 0.97 |
| 2009 | 0.84 | 0.55 | 0.84 | 0.97 | 0.85 | 0.97 |
| 2010 | 0.82 | 0.36 | 0.81 | 0.96 | 0.36 | 0.96 |
| 2011 | 0.81 | 0.36 | 0.80 | 0.96 | 0.36 | 0.95 |
| 2012 | 0.80 | 0.36 | 0.79 | 0.95 | 0.36 | 0.94 |
| 2013 | 0.79 | 0.36 | 0.78 | 0.94 | 0.36 | 0.93 |
| 2014 | 0.77 | 0.36 | 0.76 | 0.94 | 0.36 | 0.93 |
| 2015 | 0.76 | 0.36 | 0.75 | 0.93 | 0.36 | 0.92 |
| 2016 | 0.75 | 0.36 | 0.74 | 0.92 | 0.36 | 0.91 |
| 2017 | 0.74 | 0.36 | 0.72 | 0.91 | 0.36 | 0.90 |
| 2018 | 0.73 | 0.36 | 0.71 | 0.90 | 0.36 | 0.89 |
| 2019 | 0.71 | 0.36 | 0.70 | 0.89 | 0.36 | 0.88 |
| $2020+$ | 0.70 | 0.36 | 0.69 | 0.89 | 0.36 | 0.87 |

## Addition of Class III Locomotive and Industrial/Military Locomotive

The annual hours operated by the class III railroads are shown in Table 12. The results were tabulated from ARB Stationary Source Division's (SSD) survey (http://www.arb.ca.gov/regact/carblohc/carblohc.htm) conducted to support regulation with regards to ARB ultra-clean diesel fuel.

## PRELIMINARY DRAFT - DO NOT CITE OR QUOTE

Table 12. Short-Haul and Switcher Annual Hours for Class III Railroads

| Air Basin | Operations | Population | Annual Hours Operated |
| :--- | :--- | :---: | :---: |
| Mountain Counties | SW | 2 | 10214 |
| Mojave Desert | L | 10 | 27440 |
| North Coast | L | 3 | 5700 |
| North Central Coast | L | 1 | 1332 |
|  | SW | 3 | 3996 |
| Northeast Plateau | L | 5 | 9892 |
| South Coast | SW | 21 | 75379 |
| South Central Coast | L | 5 | 3200 |
| San Diego | L | 4 | 5000 |
| San Francisco | L | 8 | 31600 |
|  | SW | 4 | 5059 |
| San Joaquin Valley | L | 29 | 68780 |
|  | SW | 19 | 72248 |
| Sacramento Valley | L | 6 | 11400 |
| Total |  | 120 | 331240 |

L = local short-haul, SW = switcher

The short-haul and switcher emission rate are derived from BAH report. The report cites studies from testing done at EPA and Southwest Research Institute.

Table 13. Short-Haul and Switcher Emission Rate

| Emission Rate | Short-Haul <br> $(\mathrm{g} / \mathrm{bhp}-\mathrm{hr})$ | Switcher <br> $(\mathrm{g} / \mathrm{bhp}-\mathrm{hr})$ |
| :--- | :---: | :---: |
| HC | 0.38 | 0.44 |
| CO | 1.61 | 1.45 |
| NOx | 12.86 | 15.82 |
| PM | 0.26 | 0.28 |
| SOx | 0.89 | 0.90 |
| Fuel Rate (lb/hr) | 120.00 | 60.00 |

## PRELIMINARY DRAFT - DO NOT CITE OR QUOTE

Table 14. Statewide Summary of Industrial Locomotives

| Air Basin | Number of <br> Locomotives | Avg. HP | Avg. Age |
| :--- | :---: | :---: | :---: |
| Mojave Desert | 9 | 1,138 | 56 |
| Others | 11 | 587 | 54 |
| San Francisco | 11 | 525 | 54 |
| San Joaquin Valley | 38 | 1,176 | 54 |
| South Coast | 24 | 1,290 | 55 |
| TOTALS | 93 | 1,055 | 55 |

Table 15. Statewide Summary of Military Locomotives

| Air Basin | Number of <br> Locomotives | Avg. HP | Avg. Age |
| :--- | :---: | :---: | :---: |
| Mojave Desert | 7 | 900 | 50 |
| Northeast Plateau | 2 | 1,850 | 50 |
| Sacramento Valley | 1 | 500 | 50 |
| San Diego | 7 | 835 | 50 |
| San Francisco | 4 | 1525 | 47.5 |
| San Joaquin Valley | 2 | 400 | 50 |
| South Central Coast | 1 | 500 | 50 |
| TOTALS | 24 | 930 | 49.6 |

The data from the survey provides a reasonable depiction of railroad activities in 2003. To forecast and backcast, an assumption was made to keep the data constant and have no growth. More research is needed to quantify the growth projections of smaller, local railroad activities.

## Update to Passenger Trains

ARB's survey of intrastate locomotives included passenger agency trains that operated within the state. Staff attempted to reconcile the survey results by calculating the operation schedules posted by the operating agency to obtain hours of operation and mileage information. The results of the survey and calculated operating hours were comparable. Table 16 lists the calculated annual hours operated and miles traveled used to estimate emissions.

## PRELIMINARY DRAFT - DO NOT CITE OR QUOTE

Table 16. Passenger Trains Annual Miles and Hours

| Air Basin | Annual <br> Miles Operated | Annual <br> Hours Operated |
| :--- | :---: | :---: |
| South Coast | $3,700,795$ | 92,392 |
| South Central Coast | 151,864 | 4,020 |
| San Diego | 914,893 | 25,278 |
| San Francisco | $2,578,862$ | 77,944 |
| San Joaquin Valley | 674,824 | 17,313 |
| Sacramento Valley | 635,384 | 20,058 |
| Total | $8,656,621$ | 237,006 |

The passenger train emission rate is derived from testing done at SWRI on several passenger locomotives.

Table 17. Passenger Train Emission Rate

| Emission Rate | Passenger Train <br> $(\mathrm{g} / \mathrm{bhp}-\mathrm{hr})$ |
| :--- | :---: |
| HC | 0.50 |
| CO | 0.69 |
| Nox | 12.83 |
| PM | 0.36 |
| Sox | 0.90 |
| Fuel Rate (lb/hr) | 455.00 |

## Fuel Correction Factors

## Aromatics

Previous studies quantifying the effects of lowering aromatic content are listed in Table 18. These studies tested four-stroke heavy-duty diesel engines (HDD). Although staff would have preferred to analyze data from tests performed on various locomotive engines to determine the effects of lower aromatics, these HDD tests are the best available resources to determine the fuel corrections factors due to lower aromatics.

## PRELIMINARY DRAFT - DO NOT CITE OR QUOTE

Table 18. Effect of Lowering Aromatic Volume on PM Emission

| STUDY | Sulfur <br> (ppm) | Aromatics <br> (Volume \%) | PM Reduction <br> (\%) |
| :--- | :---: | :---: | :---: |
| Chevron (1984) | 2,800 | 31 | Baseline |
| Chevron (1984) | 500 | 31 | 23.8 |
| Chevron (1984) | 500 | 20 | 32.2 |
| Chevron (1984) | 500 | 15 | 36.0 |
| Chevron (1984) | 500 | 10 | 39.9 |
|  |  |  |  |
| CRC-SWRI (1988) | 500 | 31 | Baseline |
| CRC-SWRI (1988) | 500 | 20 | 9 |
| CRC-SWRI (1988) | 500 | 15 | 13 |
| CRC-SWRI (1988) | 500 | 10 | 17 |

Source : http://www.arb.ca.gov/fuels/diesel/diesel.htm

Using a linear regression of the data from the Table 18, the PM reduction from a change in aromatic content can be described as:

## 4-Stroke Engine

PM reduction $=[($ Difference in Aromatic Volume) * $0.785+0.05666] / 100$

For 2-Stroke engines, staff used test data from SWRI's report published in 2000 entitled "Diesel Fuel Effects on Locomotive Exhaust Emissions" to estimate indirectly the potential PM reduction for 2-Stroke engines due to lower aromatics. Table 19 lists the summary of the test results.

Table 19. SWRI 2000 Study Summary Results

| Locomotive <br> Engine | Aromatic <br> Changes <br> (Volume \%) | PM <br> Difference <br> (g/bhp-hr) | PM \% <br> Difference |
| :--- | :---: | :---: | :---: |
| 4 Stroke | 28.35 to 21.84 | 0.080 | $37.6 \%$ |
| 2 Stroke | 28.35 to 21.84 | 0.056 | $14.1 \%$ |

Staff assumes that PM emission reduction from 2-Stroke engine will have a factor of $0.38(14.1 \% / 37.6 \%)$ to the 4 -Stroke engine PM emission reduction.

Currently, the baseline locomotive emissions inventory assumes an aromatic total volume percent of $31 \%$. Table 21 describes the changes in PM emission due to changes in total volume percent of aromatics.

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Table 20. Examples of PM Reductions Due to Changes in Aromatic Total Volume Percent

| Aromatic Volume Percent |  | PM Reduction | PM Reduction | PM Reduction |
| :---: | :---: | :---: | :---: | :---: |
| From | To | 2 Stroke | 4 Stroke | Composite |
| 31 | 28 | 0.9\% | 2.4\% | 1.3\% |
| 31 | 19 | 3.6\% | 9.5\% | 5.1\% |
| 31 | 10 | 6.3\% | 16.5\% | 8.9\% |

Table 21,Table 22, and Table 23 show the PM emission reduction for the different type of fuels used in the state.

Table 21. PM Emission Percent Change of Line-Haul Due to Aromatics, Statewide

| Calendar <br> Year | CARB <br> Aromatic <br> Volume <br> $(\%)$ | EPA <br> Aromatic <br> Volume <br> $(\%)$ | Off-road <br> Aromatic <br> Volume <br> $(\%)$ | Weighted <br> Aromatic <br> Volume <br> $(\%)$ | PM Emission <br> Percent <br> Change |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1992 | 31 | 31 | 31 | 31.00 | 0.00 |
| 1993 | 10 | 31 | 31 | 31.00 | 0.00 |
| 1994 | 10 | 31 | 31 | 31.00 | 0.00 |
| 1995 | 10 | 31 | 31 | 31.00 | 0.00 |
| 1996 | 10 | 31 | 31 | 31.00 | 0.00 |
| 1997 | 10 | 31 | 31 | 31.00 | 0.00 |
| $1998-2001$ | 10 | 31 | 31 | 30.18 | -0.004 |
| $2002-2006$ | 10 | 31 | 31 | 29.05 | -0.009 |
| $2007+$ | 10 | 31 | 31 | 29.05 | -0.009 |

## PRELIMINARY DRAFT - DO NOT CITE OR QUOTE

Table 22. Class I Line Haul Weighted Aromatic Volume Percent by Air Basin

| Interstate <br> Locomotive | Air <br> Basin | $1993-2001$ <br> Weighted <br> Aromatic | 2002+ <br> Weighted <br> Aromatic |
| :--- | :--- | :---: | :---: |
|  |  | Volume Percent | Volume Percent |
| Class I Line Haul | SCC | 31.0 | 31.0 |
|  | MC | 31.0 | 26.6 |
|  | MD | 30.0 | 29.8 |
|  | NEP | 31.0 | 27.9 |
|  | SC | 31.0 | 31.0 |
|  | SF | 28.6 | 23.1 |
|  | SJV | 29.1 | 29.4 |
|  | SS | 31.0 | 31.0 |
|  | SV | 31.0 | 27.4 |

Table 23. PM Emission Reduction from Intrastate Locomotives Due to Aromatics by Air Basin, 1993+

| Intrastate Locomotive | Air Basin | CARB Aromatic | EPA Aromatic | Nonroad Aromatic | Weighted Aromatic | PM Emission Reduction |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volume Percent | Volume Percent | Volume Percent | Volume Percent | Percent |
| Class I <br> Local/Switcher | SC | 10 | 31 | 31 | 29.0 | -0.9\% |
|  | SJV | 10 | 31 | 31 | 25.2 | -2.4\% |
|  | MD | 10 | 31 | 31 | 31.0 | 0.0\% |
|  | BA | 10 | 31 | 31 | 13.9 | -7.2\% |
|  | SD | 10 | 31 | 31 | 13.2 | -7.5\% |
|  | SV | 10 | 31 | 31 | 13.2 | -7.5\% |
|  | SCC | 10 | 31 | 31 | 13.2 | -7.5\% |
| Class III Local/Switcher | SC | 10 | 31 | 31 | 31.0 | 0.0\% |
|  | SJV | 10 | 31 | 31 | 18.6 | $\begin{aligned} & -5.2 \% \\ & -8.8 \% \end{aligned}$ |
|  | MD | 10 | 31 | 31 | 10.0 |  |
|  | BA | 10 | 31 | 31 | 10.0 | -8.8\% |
|  | SD | 10 | 31 | 31 | 10.0 | -8.8\% |
|  | SV | 1010 | 31 | 31 | 10.0 | -8.8\% |
|  | SCC |  | 3131 | 31 | 10.0 | -8.8\% |
|  | NEP | 10 |  | 3131 | 26.6 | -1.9\% |
|  | MC | 10 | 31 |  | 31.0 | 0.0\% |
|  | NC | 10 | 31 | 31 | 10.0 | -8.8\% |
|  | NCC | 10 | 31 | 31 | 10.0 | -8.8\% |
| Industrial/Military | SC | 10 | 31 | 31 | 24.0 | -3.0\% |
|  | SJV | 10 | 31 | 31 | 24.0 | -3.0\% |
|  | MD | 10 | 31 | 31 | 24.0 | -3.0\% |
|  | BA | 10 | 31 | 31 | $\begin{aligned} & 24.0 \\ & 24.0 \end{aligned}$ | -3.0\% |
|  | NEP | 10 | 31 | 31 |  | -3.0\% |
|  | SD | 10 | 31 | 31 | 24.0 | -3.0\% |
|  | SV | 10 | 31 | 31 | 24.0 | $\begin{aligned} & -3.0 \% \\ & -3.0 \% \\ & \hline \end{aligned}$ |
|  | SCC | 10 | 31 | 31 | 24.0 |  |
| Passenger | SC | 10 | 3131 | 3131 | 10.8 | $\begin{aligned} & \hline-8.5 \% \\ & -8.8 \% \end{aligned}$ |
|  | SJV | 10 |  |  | $\begin{aligned} & 10.0 \\ & 10.0 \end{aligned}$ |  |
|  | BA | 10 | 3131 | 31 |  | -8.8\% |
|  | SD | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ |  | 31 | 10.0 | -8.8\% |
|  | SV |  | 31 31 | 3131 |  |  |
|  | SCC | $\begin{aligned} & 10 \\ & 10 \\ & \hline \end{aligned}$ | 31 |  | 10.0 12.1 | $\begin{aligned} & -8.8 \% \\ & -8.0 \% \\ & \hline \end{aligned}$ |

Source : Fuel Estimate from http://www.arb.ca.gov/regact/carblohc/carblohc.htm

## Sulfur

Currently, the baseline locomotive emissions inventory assumes an average fuel sulfur content of 2700 ppm . Industry has provided information on the sulfur content of the fuel that is currently being used by intrastate locomotives.
Together with industry data and prior locomotive tests, staff believes a fuel correction factor should be incorporated into the model.

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Table 24 shows the test data collected by the ARB, U.S. EPA, and others, where locomotive engines were tested on different fuel sulfur levels.

Table 24. Locomotive Engine Test with Different Sulfur Levels

| Locomotive Engine | Fuel Properties Sulfur Content | Percent Change PM | Percent Change NOX | Percent Change CO | Percent Change HC | Source |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EMD 12-645E3B | 100/3300ppm | -0.29 | -0.06 | 0.17 | 0.07 | Fritz, 1991 |
| GE DASH9-40C | 330/3150ppm | -0.43 | -0.07 | -0.05 | -0.18 | Fritz (1995, EPA/SWRI) |
| MK 5000C | 330/3150ppm | -0.71 | -0.03 | -0.03 | -0.07 | Fritz (1995, EPA/SWRI) |
| EMD 16-710G3B, SD70MAC | 330/3150ppm | -0.38 | -0.08 | -0.30 | -0.01 | Fritz (1995, EPA/SWRI) |
| EMD SD70MAC | 50/330ppm | -0.03 | -0.04 | 0.07 | 0.01 | Fritz (ARB/AAR, 2000) |
| EMD SD70MAC | 50/4760ppm | -0.16 | -0.06 | 0.08 | 0.03 | Fritz (ARB/AAR, 2000) |
| EMD SD70MAC | 330/4760ppm | -0.13 | -0.03 | 0.01 | 0.01 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 50/330ppm | -0.03 | -0.03 | -0.01 | -0.04 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 50/4760ppm | -0.39 | -0.07 | -0.02 | 0.02 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 330/4760ppm | -0.38 | -0.04 | -0.02 | 0.06 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 50/3190ppm | -0.27 | -0.05 | -0.03 | 0.01 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 330/3190ppm | -0.25 | -0.02 | -0.02 | 0.04 | Fritz (ARB/AAR, 2000) |
| GE DASH9-44CW | 3190/4760ppm | -0.17 | -. 02 | 0.00 | 0.02 | $\begin{aligned} & \text { Fritz (ARB/AAR, } \\ & 2000 \text { ) } \end{aligned}$ |
| Average |  | -0.28 | -0.05 | -0.01 | 0.00 |  |

From the above table, staff concluded that HC and CO emissions are not affected by different sulfur levels in the fuel. From these tests, staff computed the changes in PM emissions associated with changes in sulfur level. Staff corrected the PM emissions to account for the aromatic differences because the test data were not tested at the same aromatic volume percent. Because the locomotive engine testing was performed at various fuel sulfur levels (some at 330 ppm vs. 3190 ppm and some at 50 ppm vs. 3190 ppm), staff cannot assume the average percent change in PM emission is characteristics over the whole range of sulfur levels. From previous studies that staff has analyzed, it is possible to generate estimates of the percent change at various sulfur levels and throttle positions. Locomotive engines have 8 throttle positions plus dynamic braking and idle. During idle, braking, and throttle positions 1 and 2, there are no significant differences in emissions attributable to sulfur level. For the GE 4-

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stroke engine, effect of sulfur on PM for throttle positions 3 to 8 can be defined by using the following equations:

## Equations to correct for PM for GE (4-Stroke) engines

Notch 8 : PM (g/bhp-hr) $=0.00001308$ * (sulfur level,ppm) +0.0967
Notch 7 : PM (g/bhp-hr) $=0.00001102$ * (sulfur level,ppm) +0.0845
Notch 6 : PM (g/bhp-hr) $=0.00000654$ * (sulfur level,ppm) +0.1037
Notch 5 : PM (g/bhp-hr) $=0.00000548$ * (sulfur level,ppm) +0.1320
Notch 4 : PM (g/bhp-hr) $=0.00000663$ * (sulfur level,ppm) +0.1513
Notch 3 : PM (g/bhp-hr) $=0.00000979$ * (sulfur level,ppm) +0.1565

For the EMD 2-stroke engine, throttle positions 3 to 8 can be defined by using the following equations:

## Equations to correct for PM for EMD (2-Stroke) engines

Notch 8 : PM (g/bhp-hr) $=0.0000123$ * (sulfur level,ppm) +0.3563
Notch 7 : PM (g/bhp-hr) $=0.0000096$ * (sulfur level,ppm) +0.2840
Notch 6 : PM (g/bhp-hr) $=0.0000134$ * (sulfur level,ppm) +0.2843
Notch 5 : PM (g/bhp-hr) $=0.0000150$ * (sulfur level,ppm) +0.2572
Notch 4 : PM (g/bhp-hr) $=0.0000125^{*}($ sulfur level,ppm $)+0.2629$
Notch 3 : PM (g/bhp-hr) $=0.0000065$ * (sulfur level,ppm) +0.2635

Table 25. Examples of PM Reductions Due to Changes in Sulfur Level

| Sulfur Level (ppm) |  | PM Reduction | PM Reduction | PM Reduction |
| :---: | :---: | :---: | :---: | :---: |
| From | To | 2 Stroke | 4 Stroke | Composite |
| 3100 | 1900 | $4.1 \%$ | $8.4 \%$ | $5.2 \%$ |
| 3100 | 1300 | $6.1 \%$ | $12.6 \%$ | $7.7 \%$ |
| 1300 | 330 | $3.5 \%$ | $7.9 \%$ | $4.6 \%$ |
| 1300 | 140 | $4.2 \%$ | $9.5 \%$ | $5.5 \%$ |
| 140 | 15 | $1.8 \%$ | $4.0 \%$ | $2.4 \%$ |

*composite is 75\% 2 Stroke Engine and 25\% 4 Stroke Engine

Data provided by industry show that when operating in California, the three main types of diesel fuel used in locomotive engines consists of CARB diesel, EPA On-Highway diesel fuel, and EPA Off-road or High Sulfur diesel fuel. Four-stroke engines and two-stroke engines show different characteristics with respect to sulfur content. From the BAH report, 4-stroke engines make up about $25 \%$, and 2-stroke engines make up about 75\% of the locomotive engine fleet. Combining industry data, 4 -stroke/2-stroke engine percent change and fleet makeup, Table 26 shows the percent change in PM emissions by year for the line-haul segment of the fleet.

Table 26. PM Emission Percent Change of Line-Haul Due to Sulfur, Statewide

| Calendar <br> Year | CARB <br> Sulfur <br> Content | EPA <br> On- <br> Highway <br> Sulfur <br> Content | EPA <br> Off-road <br> Sulfur <br> Content | Weighted <br> Fuel <br> Sulfur <br> Content | 4-Stroke <br> Engines | 2-Stroke <br> PM <br> Percent <br> Changes | Weighted <br> PM <br> Percent <br> Change |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1992 | 3100 | 3100 | 3100 | 3100 | 0.03 | 0.01 | Emission <br> Percent <br> Change |
| 1993 | 500 | 330 | 3100 | 2919 | 0.02 | 0.01 | 0.009 |
| 1994 | 150 | 330 | 3100 | 2740 | 0.01 | 0.00 | 0.003 |
| 1995 | 140 | 330 | 3100 | 2557 | -0.01 | 0.00 | -0.006 |
| 1996 | 140 | 330 | 3100 | 2377 | -0.02 | -0.01 | -0.014 |
| 1997 | 140 | 330 | 3100 | 2196 | -0.04 | -0.02 | -0.022 |
| $1998-2001$ | 140 | 330 | 3100 | 1899 | -0.06 | -0.03 | -0.035 |
| $2002-2006$ | 140 | 330 | 3100 | 1312 | -0.10 | -0.05 | -0.061 |
| $2007+$ | 15 | 15 | 330 | 129 | -0.19 | -0.09 | -0.113 |

Table 27 and Table 28 provide further details of weighted fuel sulfur level by air basin. Weighted sulfur levels vary significantly from one air basin to another.

Table 27. Class I Line Haul Weighted Fuel Sulfur by Air Basin

| Interstate <br> Locomotive | Air <br> Basin | 1998 <br> Weighted <br> Sulfur | 2002-2006 <br> Weighted <br> Sulfur | 2007+ <br> Weighted <br> Sulfur |
| :--- | :--- | :---: | :---: | :---: |
| Class I Line Haul | SCC | ppm | ppm | ppm |
| 1023 | 467 | 31 |  |  |
|  | MC | 2333 | 1149 | 113 |
|  | MD | 2352 | 1767 | 180 |
|  | NEP | 2560 | 1632 | 166 |
|  | SC | 1985 | 1472 | 145 |
|  | SF | 1711 | 899 | 88 |
|  | SJV | 1600 | 868 | 78 |
|  | SS | 2425 | 1328 | 129 |
|  | SV | 2473 | 1456 | 147 |

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Table 28. Intrastate Locomotives Weighted Fuel Sulfur by Air Basin

| Intrastate Locomotive | Air <br> Basin | 1993 <br> Weighted <br> Sulfur | $1994-2006$ <br> Weighted <br> Sulfur | $2007+$ <br> Weighted <br> Sulfur |
| :--- | :--- | :---: | :---: | :---: |
| Class I Local/Switcher | SC | ppm | ppm | ppm |
|  | SJV | 346 | 312 | 15 |
|  | MD | 330 | 278 | 15 |
|  | BA | 468 | 330 | 15 |
|  | SD | 475 | 169 | 15 |
|  | SV | 475 | 169 | 15 |
|  | SCC | 475 | 169 | 15 |
|  | SC | 388 | 388 | 15 |
|  | SJV | 1016 | 804 | 21 |
|  | MD | 500 | 140 | 15 |
|  | BA | 500 | 140 | 15 |
|  | SD | 500 | 140 | 15 |
|  | SV | 500 | 140 | 15 |
|  | SCC | 500 | 140 | 15 |
|  | NEP | 2628 | 2553 | 264 |
|  | MC | 1573 | 1573 | 152 |
|  | NC | 500 | 140 | 15 |
|  | NCC | 500 | 140 | 15 |
| Industrial/Military | SC | 1340 | 1220 | 120 |
|  | SJV | 1340 | 1220 | 120 |
|  | MD | 1340 | 1220 | 120 |
|  | BA | 1340 | 1220 | 120 |
| Passenger | NEP | 1340 | 1220 | 120 |
|  | SD | 1340 | 1220 | 120 |
|  | SV | 1340 | 1220 | 120 |
|  | SCC | 1340 | 1220 | 120 |
|  | SC | 493 | 147 | 15 |
| SJV | 500 | 140 | 15 |  |
|  | BA | 500 | 140 | 15 |
| SD | 500 | 140 | 15 |  |
| SD | 500 | 140 | 15 |  |
| SV | 483 | 159 | 15 |  |

Appendix B,C, and D contains the fuel correction factors for PM, NOx, and SOx emissions by air basin.

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## Revised Locomotive Emission Inventory

Tables 29-31 shows the revised locomotive emission inventory for calendar years 2000,2010 and 2020.

Table 29. 2000 Statewide Locomotive Emission Inventory, tons/day

| TYPE | HC | CO | NOx | PM | SOx |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal/Line-Haul | 5.61 | 18.21 | 113.03 | 2.68 | 6.22 |
| Local/Short-Run | 1.01 | 3.33 | 22.58 | 0.41 | 0.22 |
| Mixed/Bulk | 2.13 | 6.85 | 48.95 | 1.09 | 2.20 |
| Passenger/Amtrak | 0.53 | 1.01 | 12.21 | 0.29 | 0.05 |
| Yard/Switcher | 0.55 | 1.46 | 10.43 | 0.20 | 0.09 |
| Total | 9.83 | 30.86 | 207.20 | 4.67 | 8.78 |

Table 30. 2010 Statewide Locomotive Emission Inventory, tons/day

| TYPE | HC | CO | NOx | PM | SOx |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal/Line-Haul | 5.56 | 21.90 | 71.35 | 2.40 | 0.60 |
| Local/Short-Run | 0.77 | 2.99 | 12.03 | 0.30 | 0.01 |
| Mixed/Bulk | 2.11 | 8.24 | 29.46 | 0.99 | 0.19 |
| Passenger/Amtrak | 0.58 | 1.14 | 12.29 | 0.31 | 0.02 |
| Yard/Switcher | 0.47 | 1.29 | 6.78 | 0.17 | 0.01 |
| Total | 9.49 | 35.56 | 131.91 | 4.17 | 0.83 |

Table 31. 2020 Statewide Locomotive Emission Inventory, tons/day

| TYPE | HC | CO | NOx | PM | SOx |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Intermodal/Line-Haul | 5.60 | 25.84 | 74.33 | 2.38 | 0.71 |
| Local/Short-Run | 0.67 | 2.99 | 11.17 | 0.26 | 0.01 |
| Mixed/Bulk | 2.13 | 9.72 | 31.14 | 0.98 | 0.23 |
| Passenger/Amtrak | 0.56 | 1.14 | 11.72 | 0.30 | 0.02 |
| Yard/Switcher | 0.44 | 1.29 | 6.22 | 0.16 | 0.01 |
| Total | 9.40 | 40.98 | 134.58 | 4.08 | 0.98 |

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## Appendix A

Methodology to Calculate Locomotive Inventory

## Methodology

The methodology and assumptions used for estimating locomotive emissions consists of several steps taken from the Booz-Allen Hamilton's Locomotive Emission Study report (http://www.arb.ca.gov/app/library/libcc.php). First, emission factor data from various engine manufacturers such as EMD and General Electric (GE) must be gathered to calculate average emission factors for locomotives operated by the railroad companies. Second, train operations data, including throttle position profiles and time spent on various types of operations from different railroad companies needs to be estimated. Finally, the locomotive emission inventory can be calculated using train operations data, emission factors, and throttle position profiles.

## Step 1 - Average Emission Factors

Engine emission factors are required for the different locomotive engines manufactured by the major locomotive suppliers EMD or GE. Emission factors are obtained from testing done by either the engine manufacturers or by Southwest Research Institute, a consulting company that has performed many tests on locomotive engines. Table A-1 lists the available emission factors.

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Table A-1. Available Emission Factors for Different Locomotive Engines

| Engine <br> Manufacturer | Engine Model | Locomotive Model |
| :---: | :--- | :--- |
| EMD | $12-567 B C$ | SW10 |
| EMD | $12-645 \mathrm{E}$ | SW1500,MP15,GP15-1 |
| EMD | $16-567 \mathrm{C}$ | GP9 |
| EMD | $16-645 \mathrm{E}$ | GP38,GP38-2, GP28 |
| EMD | $12-645 \mathrm{E} 3 \mathrm{~B}$ | GP39-2 |
| EMD | $12-645 \mathrm{E} 3$ | GP39-2, SD39 |
| EMD | $16-645 \mathrm{E} 3$ | GP40, SD40, F40PH |
| EMD | $16-645 \mathrm{E} 3 \mathrm{~B}$ | GP40-2, SD40-2, SDF40-2, F40PH |
| EMD | $16-645 \mathrm{~F} 3$ | GP40X, GP50, SD45 |
| EMD | $16-645 F 3 B$ | SD50 |
| EMD | $20-645 \mathrm{E} 3$ | SD45,SD45-2, F45, FP45 |
| EMD | $16-710 \mathrm{G3}$ | GP60, SD60, SD60M |
| GE | $127 F D L 2500$ | B23-7 |
| GE | $127 F D L 3000$ | SF30B |
| GE | $167 F D L 3000$ | C30-7, SF30C |
| GE | $167 F D L 4000$ | B40-8 |

Source: BAH report, 1992

Next, the locomotive roster from the largest railroad companies operating in the state were obtained. Table A-2 lists the locomotive roster for railroad companies in 1987.

Table A-2. Locomotive Roster 1987

|  |  |  |  |  | Type of Service |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Railroad Company | Engine Manufacturer | Engine Model | Horspower Rating | Units | Line Haul | Local | Yard/Switcher |
| ATSF | EMD | 16-567BC | 1500 | 211 |  |  | X |
| ATSF | EMD | 16-567C | 1750 | 53 |  |  | X |
| ATSF | EMD | 16-567D2 | 2000 | 71 |  | X | X |
| ATSF | EMD | 16-645E | 2000 | 69 |  | X | X |
| ATSF | EMD | 12-645E3 | 2300 | 62 |  | X |  |
| ATSF | EMD | 12-645E3B | 2300 | 60 |  | X |  |
| ATSF | EMD | 16-645E3 | 2500 | 231 | X | X |  |
| ATSF | EMD | 16-645E3 | 3000 | 18 | X | X |  |
| ATSF | EMD | 16-645E3B | 3000 | 203 | X | X |  |
| ATSF | EMD | 16-645F3 | 3500 | 52 | X |  |  |
| ATSF | EMD | 16-645F3B | 3600 | 15 | X |  |  |
| ATSF | EMD | 20-645E3 | 3600 | 243 | X |  |  |
| ATSF | EMD | 16-710G3 | 3800 | 20 | X |  |  |
| ATSF | GE | GE-12 | 2350 | 60 |  | X |  |
| ATSF | GE | GE-12 | 3000 | 10 | X | X |  |
| ATSF | GE | GE-16 | 3000 | 226 | X | X |  |

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| ATSF | GE | GE-16 | 3600 | 43 | X |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ATSF | GE | GE-16 | 3900 | 3 | X |  |  |
| ATSF | GE | GE-16 | 4000 | 20 | X |  |  |
| Union Pacific | EMD | 16-645BC | 1200 | 56 |  |  | X |
| Union Pacific | EMD | 12-567A | 1200 | 12 |  |  | X |
| Union Pacific | EMD | 12-645E | 1500 | 281 |  |  | X |
| Union Pacific | EMD | 16-567CE | 1500 | 35 |  |  | X |
| Union Pacific | EMD | 16-645E | 2000 | 365 |  | X | X |
| Union Pacific | EMD | 12-645E3C | 2300 | 24 |  | X |  |
| Union Pacific | EMD | 16-567D3A | 2500 | 16 |  | X |  |
| Union Pacific | EMD | 16-645E3 | 3000 | 828 | X | X |  |
| Union Pacific | EMD | 16-645E3B | 3000 | 446 | X | X |  |
| Union Pacific | EMD | 16-645F3 | 3500 | 36 | X |  |  |
| Union Pacific | EMD | 16-645F3B | 3600 | 60 | X |  |  |
| Union Pacific | EMD | 16-710G3 | 3800 | 227 | X |  |  |
| Union Pacific | GE | GE-12 | 2300 | 106 |  | X |  |
| Union Pacific | GE | GE-12 | 3000 | 57 | X | X |  |
| Union Pacific | GE | GE-16 | 3000 | 156 | X | X |  |
| Union Pacific | GE | GE-16 | 3750 | 60 | X |  |  |
| Union Pacific | GE | GE-16 | 3800 | 256 | X |  |  |
| Southern Pacific | EMD | 12-567C | 1200 | 11 |  |  | X |
| Southern Pacific | EMD | 12-645E | 1500 | 286 |  |  | X |
| Southern Pacific | EMD | 16-567BC | 1500 | 37 |  |  | X |
| Southern Pacific | EMD | 16-567C | 1750 | 326 |  | X |  |
| Southern Pacific | EMD | 16-567D2 | 2000 | 145 |  | X |  |
| Southern Pacific | EMD | 16-645E | 2000 | 84 |  | X |  |
| Southern Pacific | EMD | 12-645E3 | 2300 | 12 |  | X |  |
| Southern Pacific | EMD | 16-645E3 | 2500 | 137 | X | X |  |
| Southern Pacific | EMD | 16-645E3 | 3000 | 92 | X |  |  |
| Southern Pacific | EMD | 16-645E3B | 3000 | 353 | X |  |  |
| Southern Pacific | EMD | 16-645F3 | 3500 | 4 | X |  |  |
| Southern Pacific | EMD | 20-645E3 | 3600 | 425 | X |  |  |
| Southern Pacific | EMD | 16-710G3 | 3800 | 65 | X |  |  |
| Southern Pacific | GE | GE-12 | 2300 | 15 |  | X |  |
| Southern Pacific | GE | GE-12 | 3000 | 107 | X |  |  |
| Southern Pacific | GE | GE-16 | 3600 | 20 | X |  |  |
| Southern Pacific | GE | GE-16 | 3900 | 92 | X |  |  |

Source : BAH report, 1992

Using the available emission factors and the locomotive rosters, the average emission factors for each class of service can be calculated. Emission factors for models that were not available were assigned an emission factor based on horsepower rating and the number of cylinders from similar engine models.

## Step 2 - Throttle Position Profiles and Train Operations Data

The railroad companies provided throttle position profiles. Locomotive engines operate at eight different constant loads and speeds called throttle notches. In

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addition, several other settings (idle and dynamic brake) are also common. For line haul and local operations, profiles were obtained from Train Performance Calculation (TPC) data and actual event recorder data, which are summarized in the BAH report.

For line haul operations, the data was modified to account for additional idle time between dispatch. Data supplied by Atchison, Topeka and Santa Fe (ATSF) indicates that the turnaround time for line haul locomotives in yards is approximately eight hours.

For local operations, several assumptions were used to develop throttle profiles. First, ten hours was used as an average hours per assignment. Second, the additional average idle time per day per locomotive was assumed to be ten hours.

The switch engine duty cycle is based upon actual tape data supplied by the ATSF railroad company on a switch engine that operated over a 2-day period. Yard engines are assumed to operate 350 days per year, with 2 weeks off for inspections and maintenance.

Train operations data provided by the railroad companies included :

| Line Haul | Local | Yard/Switcher |
| :---: | :---: | :---: |
| Train type | Average trailing tons | Number of units assigned |
| Number of runs per year | Number of runs per year | Number of assignments |
| Average horsepower | Average horsepower | Average horsepower |
| Average units | Average units |  |
| Origin/destination | Origin/destination |  |
| Link miles |  |  |

## Step 3 - Calculate Locomotive Emission Inventory

Emission inventories are calculated on a train-by-train basis using train operations data, average emission factor, and throttle position profiles.

Emission Inventory = Emission factor x average horsepower x time in notch per train $x$ number of runs per year
PM Fuel Correction Factor by Air Basin

| Interstate Loc | Air Basin | PM Fuel Correction Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | pre 1993 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007+ |
| Class I Line ' | SCC | 1.000 | 0.991 | 0.982 | 0.973 | 0.964 | 0.955 | 0.937 | 0.931 | 0.925 | 0.919 | 0.913 | 0.913 | 0.913 | 0.913 | 0.913 | 0.883 |
|  | MC | 1.000 | 0.998 | 0.996 | 0.994 | 0.992 | 0.990 | 0.987 | 0.971 | 0.955 | 0.939 | 0.923 | 0.923 | 0.923 | 0.923 | 0.923 | 0.867 |
|  | MD | 1.000 | 0.998 | 0.995 | 0.993 | 0.991 | 0.988 | 0.984 | 0.978 | 0.973 | 0.967 | 0.962 | 0.962 | 0.962 | 0.962 | 0.962 | 0.884 |
|  | NEP | 1.000 | 0.999 | 0.998 | 0.998 | 0.997 | 0.996 | 0.995 | 0.983 | 0.971 | 0.959 | 0.947 | 0.947 | 0.947 | 0.947 | 0.947 | 0.875 |
|  | SC | 1.000 | 0.996 | 0.993 | 0.989 | 0.986 | 0.982 | 0.975 | 0.970 | 0.965 | 0.960 | 0.955 | 0.955 | 0.955 | 0.955 | 0.955 | 0.888 |
|  | SF | 1.000 | 0.993 | 0.987 | 0.980 | 0.974 | 0.967 | 0.954 | 0.940 | 0.926 | 0.912 | 0.898 | 0.898 | 0.898 | 0.898 | 0.898 | 0.851 |
|  | SJV | 1.000 | 0.993 | 0.986 | 0.979 | 0.972 | 0.965 | 0.952 | 0.944 | 0.937 | 0.930 | 0.923 | 0.923 | 0.923 | 0.923 | 0.923 | 0.878 |
|  | SS | 1.000 | 0.999 | 0.997 | 0.996 | 0.995 | 0.993 | 0.991 | 0.980 | 0.970 | 0.959 | 0.949 | 0.949 | 0.949 | 0.949 | 0.949 | 0.887 |
|  | SV | 1.000 | 0.993 | 0.986 | 0.979 | 0.972 | 0.965 | 0.952 | 0.948 | 0.945 | 0.942 | 0.939 | 0.939 | 0.939 | 0.939 | 0.939 | 0.873 |


| Intrastate Lod | Air Basin | PM Fuel Corre | actor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | pre 1993 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007+ |
| Class I Local | SC | 1.000 | 0.890 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.865 |
|  | SJV | 1.000 | 0.863 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.858 | 0.836 |
|  | MD | 1.000 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.906 | 0.882 |
|  | BA | 1.000 | 0.778 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.764 | 0.747 |
|  | SD | 1.000 | 0.772 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.741 |
|  | SV | 1.000 | 0.772 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.741 |
|  | SCC | 1.000 | 0.772 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.758 | 0.741 |
| Class III Loca | SC | 1.000 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.909 | 0.882 |
|  | SJV | 1.000 | 0.839 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.830 | 0.787 |
|  | MD | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | BA | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | SD | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | SV | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | ScC | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | NEP | 1.000 | 0.963 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.960 | 0.858 |
|  | MC | 1.000 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | 0.888 |
|  | NC | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | NCC | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.722 |
| Industrial/Milif | SC | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | SJV | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | MD | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | BA | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | NEP | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | SD | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | SV | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
|  | SCC | 1.000 | 0.894 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.889 | 0.831 |
| Passenger | SC | 1.000 | 0.754 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.739 | 0.723 |
|  | SJV | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | BA | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | SD | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | SV | 1.000 | 0.749 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.733 | 0.717 |
|  | SCC | 1.000 | 0.764 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.749 | 0.733 |

## NOx Fuel Correction Factor by Air Basin

| Interstate Log | Air Basin | ${ }^{\text {NOX Fuel Coris }}$ | Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | pre 1993 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | $2007+$ |
| Class I Line | ¢scc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | ${ }^{0.940}$ | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | мС | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | MD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | NEP | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SF | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SJv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | ss | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  |  | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |  |


| Intrastate Lod | Air Basin | ${ }^{\text {NOX Fuel Corri }}$ | Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Class I Local | SC | pre 1993 | ${ }_{0} 0.940$ | 0.940 | ${ }_{0} 0.940$ | $\frac{1996}{0.940}$ | 0.940 | 0.940 | 1.940 | 2000 | 2001 | $\frac{2002}{} 0.940$ | 2003 | 2004 | 2005 | 2006 | 2007+ |
|  | sJv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | MD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | BA | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | Scc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
| Class III Loc | Sc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sJv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | MD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | BA | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | scc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | NEP | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | мс | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | NC | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | NCC | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
| Industrial/Milif |  | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sJv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | MD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | BA | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | NEP | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | Scc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
| Passenger | SC | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sJv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | BA | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | SD | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | sv | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |
|  | Scc | 1.000 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 | 0.940 |


| Interstate LodAir Basin |  | SOx Fuel Correction Factor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | pre 1993 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007+ |
| Class I Line $\dagger$ | SCC | 1.000 | 0.896 | 0.793 | 0.689 | 0.586 | 0.482 | 0.379 | 0.327 | 0.276 | 0.225 | 0.173 | 0.173 | 0.173 | 0.173 | 0.173 | 0.011 |
|  | MC | 1.000 | 0.977 | 0.955 | 0.932 | 0.909 | 0.887 | 0.864 | 0.755 | 0.645 | 0.535 | 0.426 | 0.426 | 0.426 | 0.426 | 0.426 | 0.042 |
|  | MD | 1.000 | 0.979 | 0.957 | 0.936 | 0.914 | 0.893 | 0.871 | 0.817 | 0.763 | 0.709 | 0.654 | 0.654 | 0.654 | 0.654 | 0.654 | 0.067 |
|  | NEP | 1.000 | 0.991 | 0.983 | 0.974 | 0.965 | 0.957 | 0.948 | 0.862 | 0.776 | 0.690 | 0.605 | 0.605 | 0.605 | 0.605 | 0.605 | 0.062 |
|  | SC | 1.000 | 0.956 | 0.912 | 0.868 | 0.823 | 0.779 | 0.735 | 0.688 | 0.640 | 0.593 | 0.545 | 0.545 | 0.545 | 0.545 | 0.545 | 0.054 |
|  | SF | 1.000 | 0.939 | 0.878 | 0.817 | 0.756 | 0.695 | 0.634 | 0.559 | 0.483 | 0.408 | 0.333 | 0.333 | 0.333 | 0.333 | 0.333 | 0.033 |
|  | SJV | 1.000 | 0.932 | 0.864 | 0.796 | 0.728 | 0.660 | 0.593 | 0.525 | 0.457 | 0.389 | 0.322 | 0.322 | 0.322 | 0.322 | 0.322 | 0.029 |
|  | SS | 1.000 | 0.983 | 0.966 | 0.949 | 0.932 | 0.915 | 0.898 | 0.797 | 0.695 | 0.594 | 0.492 | 0.492 | 0.492 | 0.492 | 0.492 | 0.048 |
|  | SV | 1.000 | 0.986 | 0.972 | 0.958 | 0.944 | 0.930 | 0.916 | 0.822 | 0.728 | 0.634 | 0.539 | 0.539 | 0.539 | 0.539 | 0.539 | 0.054 |


| Intrastate Loo Air Basin |  | $\begin{array}{\|l} \hline \begin{array}{l} \text { SOx Fuel Cor } \\ \text { pre } 1993 \end{array} \\ \hline \end{array}$ | Factor 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007+ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Class I Local/ | SC | 1.000 | 0.128 | 0.127 | 0.126 | 0.125 | 0.124 | 0.122 | 0.121 | 0.120 | 0.119 | 0.118 | 0.117 | 0.115 | 0.115 | 0.115 | 0.006 |
|  | SJV | 1.000 | 0.139 | 0.136 | 0.133 | 0.130 | 0.126 | 0.123 | 0.120 | 0.116 | 0.113 | 0.110 | 0.106 | 0.103 | 0.103 | 0.103 | 0.006 |
|  | MD | 1.000 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.122 | 0.006 |
|  | BA | 1.000 | 0.173 | 0.164 | 0.154 | 0.144 | 0.134 | 0.124 | 0.114 | 0.104 | 0.095 | 0.085 | 0.075 | 0.065 | 0.065 | 0.065 | 0.006 |
|  | SD | 1.000 | 0.176 | 0.165 | 0.155 | 0.145 | 0.135 | 0.124 | 0.114 | 0.104 | 0.093 | 0.083 | 0.073 | 0.062 | 0.062 | 0.062 | 0.006 |
|  | SV | 1.000 | 0.176 | 0.165 | 0.155 | 0.145 | 0.135 | 0.124 | 0.114 | 0.104 | 0.093 | 0.083 | 0.073 | 0.062 | 0.062 | 0.062 | 0.006 |
|  | SCC | 1.000 | 0.176 | 0.165 | 0.155 | 0.145 | 0.135 | 0.124 | 0.114 | 0.104 | 0.093 | 0.083 | 0.073 | 0.062 | 0.062 | 0.062 | 0.006 |
| Class III Loca | SC | 1.000 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.144 | 0.008 |
|  | SJV | 1.000 | 0.376 | 0.369 | 0.362 | 0.355 | 0.348 | 0.341 | 0.333 | 0.326 | 0.319 | 0.312 | 0.305 | 0.298 | 0.298 | 0.298 | 0.029 |
|  | MD | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | BA | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SD | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SV | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SCC | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | NEP | 1.000 | 0.973 | 0.971 | 0.968 | 0.966 | 0.963 | 0.961 | 0.958 | 0.956 | 0.953 | 0.951 | 0.948 | 0.946 | 0.946 | 0.946 | 0.098 |
|  | MC | 1.000 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.583 | 0.056 |
|  | NC | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | NCC | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
| Industrial/Milii | SC | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | SJV | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | MD | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | BA | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | NEP | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | SD | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | SV | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
|  | SCC | 1.000 | 0.496 | 0.492 | 0.488 | 0.484 | 0.480 | 0.476 | 0.472 | 0.468 | 0.464 | 0.460 | 0.456 | 0.452 | 0.452 | 0.452 | 0.044 |
| Passenger | SC | 1.000 | 0.183 | 0.171 | 0.159 | 0.148 | 0.136 | 0.124 | 0.113 | 0.101 | 0.090 | 0.078 | 0.066 | 0.055 | 0.055 | 0.055 | 0.006 |
|  | SJV | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | BA | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SD | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SV | 1.000 | 0.185 | 0.173 | 0.161 | 0.149 | 0.137 | 0.125 | 0.112 | 0.100 | 0.088 | 0.076 | 0.064 | 0.052 | 0.052 | 0.052 | 0.006 |
|  | SCC | 1.000 | 0.179 | 0.168 | 0.157 | 0.146 | 0.135 | 0.124 | 0.113 | 0.103 | 0.092 | 0.081 | 0.070 | 0.059 | 0.059 | 0.059 | 0.006 |

## APPENDIX B

EMISSION FACTOR DERIVATION AND EMFAC 2007 OUTPUT FOR DIESEL-FUELED YARD TRUCKS
Running Exhaust Emissions

| Equipment Type | Equipment ID/Owner | VehicleID | Make/Model | Year | Vehicle <br> Class | Emission Factors (g/mi ${ }^{1,2}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | ROG | CO | NOx | PM10 ${ }^{3}$ | $\mathrm{DPM}^{3}$ | SOx |
| Truck | Engineering | 69496 | Chevy CK 3500 | 1998 | LDT | 0.12 | 1.13 | 1.60 | 0.06 | 0.06 | 0.06 |
| Truck | Engineering | 69499 | Chevy CK 3500 | 1998 | LDT | 0.12 | 1.13 | 1.60 | 0.06 | 0.06 | 0.06 |
| Truck | Car Dept | 1915-73119 | Ford F-450 | 2003 | LHDT1 | 0.33 | 1.70 | 6.70 | 0.11 | 0.08 | 0.04 |
| Truck | Engineering | 9007E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 1.25 | 0.16 |
| Truck | Engineering | 9009E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 1.25 | 0.16 |
| Truck | Engineering | 9031 E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 1.25 | 0.16 |
| Truck | Engineering | 9018 E | Ford F-800 | 1992 | MHD | 0.94 | 9.70 | 18.46 | 1.25 | 1.25 | 0.16 |
| Truck | Car Dept | NA | International | 1987 | HHD | 12.31 | 41.26 | 31.86 | 5.72 | 5.72 | 0.22 |
| Truck | Engineering | 64274 | Ford LT8000 | 1989 | HHD | 12.06 | 40.31 | 31.60 | 5.48 | 5.42 | 0.24 |
| Truck | Car Dept | 1915-9038E | Ford LT9000 | 1997 | HHD | 6.92 | 16.99 | 31.05 | 2.34 | 2.26 | 0.24 |
| Total |  |  |  |  |  |  |  |  |  |  |  |

Idling Exhaust Emissions

| Equipment Type | Equipment ID/Owner | Vehicle <br> ID | Make/Model | Year | Vehicle <br> Class | Emission Factors (g/hr) ${ }^{4}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | ROG | CO | NOx | PM10 ${ }^{3}$ | $\mathrm{DPM}^{3}$ | SOx |
| Truck | Engineering | 69496 | Chevy CK 3500 | 1998 | LDT | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Truck | Engineering | 69499 | Chevy CK 3500 | 1998 | LDT | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Truck | Car Dept | 1915-73119 | Ford F-450 | 2003 | LHDT2 | 3.17 | 26.30 | 75.05 | 0.75 | 0.75 | 0.34 |
| Truck | Engineering | 9007E | Ford F-800 | 1992 | MHD | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 |
| Truck | Engineering | 9009E | Ford F-800 | 1992 | MHD | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 |
| Truck | Engineering | 9031 E | Ford F-800 | 1992 | MHD | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 |
| Truck | Engineering | 9018E | Ford F-800 | 1992 | MHD | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 |
| Truck | Car Dept | NA | International | 1987 | HHD | 22.84 | 61.55 | 82.94 | 4.28 | 4.28 | 0.55 |
| Truck | Engineering | 64274 | Ford LT8000 | 1989 | HHD | 19.45 | 58.49 | 85.53 | 3.43 | 3.43 | 0.55 |
| Truck | Car Dept | 1915-9038E | Ford LT9000 | 1997 | HHD | 12.41 | 49.53 | 110.27 | 1.93 | 1.93 | 0.55 |
| Total |  |  |  |  |  |  |  |  |  |  |  |

1. Running exhaust emissions calculated using the EMFAC2007 model with the BURDEN output option. 3. The PM10 emission factor includes engine exhaust emissions along with brake and tire wear. The DPM emission factor includes engine exhaust emissions only. 4. Idling exhaust emissions factors calculated using the EMFAC2007 model with the EMFAC output option.

Title : Statewide totals Avg Annual CYr 2005 Default Title
Version: Emfac2007 V2.3 Nov 12006 ** WIS Enabled **
Run Date : 2007/08/29 12:52:46
Scen Year: 2005 -- Model year 1998 selected
Season : Annual
Area : Statewide totals Average
I/M Stat : Enhanced Interim (2005) -- Using I/M schedule for area 59 Los Angeles (SC)
Emissions: Tons Per Day

| $* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * ~$ |  |
| :--- | :---: |
|  | LDT1-DSL |
| Vehicles | 4219 |
| VMT/1000 | 153 |
| Trips | 27083 |
| Reactive Organic Gas Emissions |  |
| Run Exh | 0.02 |
| Idle Exh | 0 |
| Start Ex | 0 |
|  | -----2 |

Diurnal 0
Hot Soak 0
Running 0
Resting 0
Total 0.02

| Carbon Monoxide Emissions |  |
| :--- | :--- |
| Run Exh | 0.19 |

Idle Exh 0
Start Ex 0
Total Ex 0.19
Oxides of Nitrogen Emissions
Run Exh
Idle Exh 0
Start Ex 0
Total Ex 0.27

Carbon Dioxide Emissions (000)
Run Exh

| Run Exh | 0 |
| :--- | :---: |
| Idle Exh | 0 |

Total Ex $\quad 0.06$

| PM10 Emissions |  |
| :--- | :--- |
| Run Exh | 0.01 |

Idle Exh 0
Start Ex 0
Total Ex 0.01

| TireWear | 0 |
| :--- | :---: |
| BrakeWr | 0 |
|  | ------ |
| Total | 0.01 |
| Lead | 0 |
| SOx | 0.01 |
| Fuel Consumption (000 gallons) | 0 |
| Gasoline | 5.24 |
| Diesel |  |


| Title : Statewide totals Avg Annual CYr 2005 Default Title |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Version : Emfac2007 V2.3 Nov 12006 ** WIS Enabled ** |  |  |  |  |  |  |  |
| Run Date : 2007/08/29 12:53:28 |  |  |  |  |  |  |  |
| Scen Year: 2005 -- Model year 1998 selected |  |  |  |  |  |  |  |
| Season : Annual |  |  |  |  |  |  |  |
| Area : Statewide totals |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Year: 2005 |  |  | -- Model Years |  |  | Emfac2007 Emission Factors: V2.3 Nov 12006 ** WIS Enabled ** |  |
| State Average |  |  | State Average |  |  |  |  |
| Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour) |  |  |  |  |  |  |  |
| Pollutant Name: Reactive Org Gases |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| Speed <br> MPH | LDT1 | LDT1 | LDT1 | LDT1 |  |  |  |
|  | NCAT | CAT | DSL | ALL |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |
| Pollutant Name: Carbon Monoxide |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| Speed <br> MPH | LDT1 | LDT1 | LDT1 | LDT1 |  |  |  |
|  | NCAT | CAT | DSL | ALL |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |
| Pollutant Name: Oxides of Nitrogen |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| Speed <br> MPH | LDT1 | LDT1 | LDT1 | LDT1 |  |  |  |
|  | NCAT | CAT | DSL | ALL |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |
| Pollutant Name: Carbon Dioxide |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| Speed MPH | LDT1 | LDT1 | LDT1 | LDT1 |  |  |  |
|  | NCAT | CAT | DSL | ALL |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |
| Pollutant Name: Sulfur Dioxide |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| SpeedMPH | LDT1 | LDT1 | LDT1 | LDT1 |  |  |  |
|  | NCAT | CAT | DSL | ALL |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |
| Pollutant Name: PM10 |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |  |
| Speed | LDT1 | LDT1 | LDT1 | ALL 1 |  |  |  |
| MPH | NCAT | CAT | DSL |  |  |  |  |
|  | 0 | 0 | 0 | 0 | 0 |  |  |

Title : Statewide totals Avg Annual CYr 2005 Default Title
Version : Emfac2007 V2.3 Nov 12006 ** WIS Enabled **
Run Date : 2007/08/29 12:53:28
Scen Year: 2005 -- Model year 1998 selected
Season : Annual
Area : Statewide totals

| Year: 2005 | -- Model Years |
| :--- | :---: |
| $\quad$ Emfac2007 Emission Factors: V2.3 Nov 12006 ** WIS Enabled ** |  |

State Average
State Average
Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant Name: PM10 - Tire Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | LDT1 | LDT1 | LDT1 |  | LDT1 |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: PM10 - Brake Wear |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | LDT1 | LDT1 | LDT1 |  | LDT1 |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Gasoline - mi/gal |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | LDT1 | LDT1 | LDT1 |  | LDT1 |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Diesel - mi/gal |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | LDT1 | LDT1 | LDT1 |  | LDT1 |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |







County Average Los Angeles

Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant Name: PM10 - Tire Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | MHD | MHD | MHD |  | MHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: PM10 - Brake Wear |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | MHD | MHD | MHD |  | MHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Gasoline - mi/gal |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | MHD | MHD | MHD |  | MHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Diesel - mi/gal |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | MHD | MHD | MHD |  | MHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |




Title : Los Angeles County Avg Annual CYr 2005 Default Title
Version : Emfac2007 V2.3 Nov 12006 ** WIS Enabled **
Run Date : 2007/08/29 11:57:55
Scen Year: 2005 -- Model year 1987 selected
Season : Annual
Area : Los Angeles

| Year: 2005 | - Model Years | 1987 to |
| :--- | :---: | :---: |
| Emfac2007 Emission Factors: V2.3 Nov 12006 ** WIS Enabled ** |  |  |

County Average Los Angeles

Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant Name: PM10 - Tire Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: PM10 - Brake Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Gasoline - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Diesel - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed <br> MPH | HHD | HHD | HHD |  | HHD |  |
|  | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |



Title: Los Angeles County Avg Annual CYr 2005 Default Title
Version : Emfac2007 V2.3 Nov 12006 ** WIS Enabled **
Run Date: 2007/08/29 11:58:37
Scen Year: 2005 -- Model year 1989 selected
Season: Annual
Area : Los Angeles

| $* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * ~$ |
| :--- | :--- |
| Year: $\quad$-- Model Years |
| Emfac2007 Emission Factors: V2.3 Nov 12006 ** WIS Enabled ** |

County Average Los Angeles

Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant Name: PM10 - Tire Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: PM10 - Brake Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Gasoline - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Diesel - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |

Title : Los Angeles County Avg Annual CYr 2005 Default Title
Version: Emfac2007 V2.3 Nov 12006 ** WIS Enabled **
Run Date : 2007/08/29 11:49:25
Scen Year: 2005 -- Model year 1997 selected
Season : Annual
Area : Los Angeles County Average
I/M Stat : Enhanced Interim (2005) -- Using I/M schedule for area
Emissions: Tons Per Day
**************************************************************************

## HHDT-DSL

1395
Vehicles
VMT/1000 345
Trips 7058
Reactive Organic Gas Emissions
Run Exh

| Idle Exh | 0.03 |
| :--- | :--- |

Start Ex 0
$\begin{array}{ll}\text { Total Ex } & 2.66\end{array}$

| Diurnal | 0 |
| :--- | :---: |
| Hot Soak | 0 |
| Running | 0 |
| Resting | 0 |
| Total | ----- |
| Carbon Monoxide Emissions | 2.66 |
| Run Exh | 6.46 |
| Idle Exh | 0.13 |
| Start Ex | 0 |
|  | -----9 |
| Total Ex | 6.59 |
| Oxides of Nitrogen Emissions |  |
| Run Exh | 11.81 |
| Idle Exh | 0.29 |
| Start Ex | 0 |
|  | ------ |
| Total Ex | 12.1 |
| Carbon Dioxide Emissions (000) |  |
| Run Exh | 1.09 |
| Idle Exh | 0.02 |
| Start Ex | 0 |

Total Ex 1.11
$\begin{array}{ll}\text { PM10 Emissions } \\ \text { Run Exh } & 0.86\end{array}$
Idle Exh 0
Start Ex 0
Total Ex $\quad 0.86$

TireWear 0.01
BrakeWr 0.01
Total 0.89
Lead 0
SOx 0.09
Fuel Consumption (000 gallons)
Gasoline

| Gasoline | 0 |
| :--- | :---: |
| Diesel | 99.81 |



Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant |  |  | Temperature: $65 F$ | Relative Humidity: $60 \%$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Speed | HHD | HHD | HHD | HHD |  |
| MPH | NCAT | CAT | DSL | ALL |  |
|  | 0 | 0 | 0 | 12.413 | 11.839 |


| Pollutant Name: Carbon Monoxide |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | HHD | HHD |  | HHD | HHD |  |
| MPH | NCAT | CAT |  | DSL | ALL |  |
|  |  | 0 | 0 | 49.525 | 47.237 |  |



| Pollutant Name: Sulfur Dioxide |  |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | HHD | HHD |  | HHD |  | HHD |  |
| MPH | NCAT | CAT |  | DSL |  | ALL |  |
|  | 0 | 0 | 0 |  | 0.55 | 0.525 |  |
| Pollutant Name: PM10 |  |  |  |  |  | Temperature: 65F | Relative Humidity: 60\% |
| Speed | HHD | HHD |  | HHD |  | HHD |  |
| MPH | NCAT | CAT |  | DSL |  | ALL |  |
|  | 0 | 0 | 0 |  | 1.928 | 1.839 |  |


County Average Los Angeles

Table 1: Running Exhaust Emissions (grams/mile; grams/idle-hour)

| Pollutant Name: PM10 - Tire Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: PM10 - Brake Wear |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Gasoline - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |
| Pollutant Name: Diesel - mi/gal |  |  |  | Temperature: 65F |  | Relative Humidity: 60\% |
| Speed | HHD | HHD | HHD |  | HHD |  |
| MPH | NCAT | CAT | DSL |  | ALL |  |
|  | 0 | 0 | 0 | 0 | 0 |  |

## APPENDIX C

EMISSION FACTOR DERIVATION AND EMFAC 2007 OUTPUT FOR HHD DIESEL-FUELED DELIVERY TRUCKS

Emission Factors for HHD Diesel-Fueled Delivery Trucks
Dolores and ICTF Rail Yards, Long Beach, CA

Running Exhaust Emissions

| Delivery | 2005 Emission Factors (g/mi) ${ }^{1,2}$ |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROG | CO | NOx | PM10 | DPM $^{3}$ | SOx |  |
| Gasoline | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 |  |
| Lube Oil | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 |  |
| Used Oil | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 |  |
| Soap | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 |  |
| Sand | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 |  |
| Total |  |  |  |  |  |  |  |

Idling Exhaust Emissions

| Delivery <br> Type | 2005 Emission Factors $(\mathrm{g} / \mathrm{hr})^{4}$ |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ROG | CO | NOx | PM10 | DPM | SOx |  |
|  | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 |  |
| Lube Oil | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 |  |
| Used Oil | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 |  |
| Soap | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 |  |
| Sand | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 |  |
| Total |  |  |  |  |  |  |  |

Notes:

1. Running exhaust emission factors ( $\mathrm{g} / \mathrm{mi}$ ) from EMFAC 2007 using the BURDEN output option. The EMFAC default model year distribution for L.A. County was used.
2. Emission factor calculations assumed an average speed of 15 mph .
3. The PM10 emission factor includes engine exhaust emissions along with brake and tire wear. The DPM emission factor includes engine exhaust emissions only.
4. Idling exhaust emission factors from EMFAC 2007 using the EMFAC output option. The EMFAC default model year distribution for L.A. County was used.



## APPENDIX D

EMISSION FACTOR DERIVATION AND OFFROAD2007 OUTPUT FOR HEAVY EQUIPMENT

| CO2-Exhaust | SO2-Exhaust |
| ---: | ---: |
| 0.120235 | $1.17247 \mathrm{E}-05$ |
| 0.2120184 | $2.15547 \mathrm{E}-05$ |
| 0.4716508 | $4.5993 \mathrm{E}-05$ |
| 0.09395151 | $9.16167 \mathrm{E}-06$ |

APPENDIX D
OFFROAD2007 OUTPUT
NOx-Exhaust
0.001769009
0.003119413
0.004416037
0.00215985

APPENDIX D
OFFROAD2007 OUTPUT


APPENDIX D
OFFROAD2007 OUTPUT


## APPENDIX E

TANKS OUTPUT AND SPECIATE DATABASE SECTIONS FOR THE GASOLINE STORAGE TANKS
TANKS 4.0.9d
Emissions Report - Detail Format
Tank Indentification and Physical Characteristics
Identification

$$
\begin{aligned}
& \text { Colton \# } 1189 \\
& \text { Los Angeles C.O. } \\
& \text { California } \\
& \text { UPRR } \\
& \text { Horizontal Tank }
\end{aligned}
$$ $00^{\circ}$ GL8' $\varepsilon$

$L^{\circ} \angle$
$0^{\circ} 009$
$Z^{\circ} \downarrow$

$0^{\circ} \mathrm{G}$ | 5.00 |
| ---: |
| 4.20 |
| 500.00 |
| 7.75 |
| 75.00 |
|  |
|  |
|  |
|  |
|  |
|  |
|  |
| -0.03 |
| 0.03 | Meterological Data used in Emissions Calculations: Los Angeles C.O., California (Avg Atmospheric Pressure $=14.67 \mathrm{psia}$ )

TANKS 4.0.9d
Emissions Report - Detail Format
Liquid Contents of Storage Tank
$\underset{\substack{\text { yund } \\ \text { fuex }}}{ }$

| Month | Daily Liquid Surf. Temperature ( $\operatorname{deg} \mathrm{F}$ ) |  |  | Liquid BulkTemp (deg F) | Vapor Pressure (psia) |  |  | Vapor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Avg. | Min. | Max. |  | Avg. | Min. | Max. | Weight. |
| All | 68.08 | 62.92 | 73.24 | 65.99 | 8.0605 | 7.3344 | 8.8422 | 62.0000 |

file://C::Program Files|Tanks409d|summarydisplay.htm
TANKS 4.0.9d
Emissions Report - Detail Format Detail Calculations (AP-42) Colton \# 1189 - Horizontal Tank
Los Angeles C.O., California

| Annual Emission Calcaulations |  |
| :--- | ---: |
| Standing Losses (lb): | 193.3005 |
| Vapor Space Volume (cu ft): | 44.1224 |
| Vapor Density (lb/cu ft): | 0.0882 |
| Vapor Space Expansion Factor: | 0.2580 |
| Vented Vapor Saturation Factor: | 0.5271 |
| Tank Vapor Space Volume: |  |
| Vapor Space Volume (cu ft): | 44.1224 |
| Tank Diameter (ft): (ft): | 4.2000 |
| Effective Diameter | 5.1722 |
| Vapor Space Outage (ft): | 2.1000 |
| Tank Shell Length (ft): | 5.0000 |

file://C:|Program Files 1 Tanks409d|summarydisplay.htm
Emissions Report for: Annual
Colton \# 1189 - Horizontal Tank
Los Angeles C.O., California Components
Gasoline (RVP 13)
TANKS 4.0.9d
Emissions Report - Detail Format
Tank Indentification and Physical Characteristics

TANKS 4.0.9d
Emissions Report - Detail Format
Liquid Contents of Storage Tank
TANKS 4.0.9d
Emissions Report - Detail Format
Detail Calculations (AP-42)
Colton \#1172-Horizontal Tank
Los Angeles C.O., California

| Annual Emission Calcaulations |  |
| :--- | ---: |
| Standing Losses (lb): | 193.3005 |
| Vapor Space Volume (cu ft): | 44.1224 |
| Vapor Density (lb/cu ft): | 0.0882 |
| Vapor Space Expansion Factor: | 0.2580 |
| Vented Vapor Saturation Factor: | 0.5271 |
| Tank Vapor Space Volume: |  |
| Vapor Space Volume (cu ft): | 44.1224 |
| Tank Diameter (ft): | 4.2000 |
| Effective Diameter (ft): | 5.1722 |
| Vapor Space Outage (ft): | 2.1000 |
| Tank Shell Length (ft): | 5.0000 |

[^12]file://C:|Program Files\Tanks409d|summarydisplay.htm
Emissions Report for: Annual
Colton \#1172 - Horizontal Tank
Los Angeles C.O., California Components
Gasoline (RVP 13)

TANKS 4.0.9d
Emissions Report - Detail Format
Tank Indentification and Physical Characteristics

$$
\begin{array}{llr}
\begin{array}{l}
\text { Identification } \\
\text { User Identification: } \\
\text { City: }
\end{array} & \begin{array}{l}
\text { Colton \#1187 } \\
\text { State: }
\end{array} & \begin{array}{l}
\text { Los Angeles C.O. }
\end{array} \\
\text { Company: } & \text { California } \\
\text { Type of Tank: } & \text { UPRR } \\
\text { Description: } & & \\
& & \\
\text { Tarizontal Tank }
\end{array}
$$

TANKS 4.0.9d
Emissions Report - Detail Format Detail Calculations (AP-42)
Colton \#1187-Horizontal Tank
Los Angeles C.O., California

| Annual Emission Calcaulations |  |
| :--- | ---: |
| Standing Losses (lb): | 193.3005 |
| Vapor Space Volume (cu ft): | 44.1224 |
| Vapor Density (lb/cu ft): | 0.0882 |
| Vapor Space Expansion Factor: | 0.2580 |
| Vented Vapor Saturation Factor: | 0.5271 |
|  |  |
| Tank Vapor Space Volume: | 44.1224 |
| Vapor Space Volume (cu ft): | 4.2000 |
| Tank Diameter (ft): | 5.1722 |
| Effective Diameter (ft): | 2.1000 |
| Vapor Space Outage (ft): | 5.0000 |

[^13]Emissions Report for: Annual
Colton \#1187 - Horizontal Tank
Los Angeles C.O., California
os Angeles C.O., California Components
Gasoline (RVP 13)
TANKS 4.0.9d
Emissions Report - Detail
Emissions Report - Detail Format
Individual Tank Emission Totals

0ع'E61
sso7 6u!̣łеәдя
(squ)səssoา
Working Loss
40.93

\[

$$
\begin{aligned}
& \text { Identification }
\end{aligned}
$$
\]

$\begin{aligned} & \text { N } \\ & \text { N } \\ & \begin{array}{l}\text { White/White } \\ \text { Good }\end{array}\end{aligned}$
Good
TANKS 4.0.9d
Emissions Report - Detail Format
Detail Calculations (AP-42)
Colton \#1498 - Horizontal Tank
Los Angeles C.O., California

|  |  |
| :--- | ---: |
| Annual Emission Calcaulations |  |
| Standing Losses (lb): | 193.3005 |
| Vapor Space Volume (cu ft): | 44.1224 |
| Vapor Density (lb/cu ft): | 0.0882 |
| Vapor Space Expansion Factor: | 0.2580 |
| Vented Vapor Saturation Factor: | 0.5271 |
| Tank Vapor Space Volume: |  |
| Vapor Space Volume (cu ft): | 44.1224 |
| Tank Diameter (ft): | 4.2000 |
| Effective Diameter (ft): | 5.1722 |
| Vapor Space Outage (ft): | 2.1000 |
| Tank Shell Length (ft): | 5.0000 |


Emissions Report for：Annual

Exerpts from CARB's Speciation Profile Database

ORGPROFN

 199
$s 199$
199
199
199
s 199
s 199
s 1996
s 199
s 199
 Headspace vapors Headspace vapors pors Headspace vapors Headspace vapors
ORGFRAC
0.01540998 0.01540998
0.01028 0.01294998 0.0036 0.01702 0.00118 0.00118
0.00128 0.00343 0.00107

APPENDIX F

DETAILED EMISSION CALCULATIONS

Summary of Diesel Particulate Matter Emissions
Colton Rail Yard, Bloomington, CA

| Source | DPM Emissions <br> (tpy) |
| :--- | :---: |
| Locomotives | 16.30 |
| Yard Trucks | 0.19 |
| HHD Diesel-Fueled Delivery Trucks | 0.00 |
| Heavy Equipment | 0.05 |
| Emergency Generator | 0.00 |
| Total | $\mathbf{1 6 . 5 4}$ |

Summary of Toxic Air Contaminant Emissions
Colton Rail Yard, Bloomington, CA

| CAS | Chemical Name | Non-DPM TAC Emissions (tpy) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Gasoline Storage Tanks | WWTP | Total |
| 540841 | 2,2,4-trimethylpentane | $3.61 \mathrm{E}-03$ | - | $3.61 \mathrm{E}-03$ |
| 71432 | benzene | $1.00 \mathrm{E}-03$ | $3.88 \mathrm{E}-01$ | $3.89 \mathrm{E}-01$ |
|  | bis(2-ethylhexyl) Phthalate | - | $1.91 \mathrm{E}-02$ | $1.91 \mathrm{E}-02$ |
|  | bromomethane | - | $6.81 \mathrm{E}-01$ | $6.81 \mathrm{E}-01$ |
| 67663 | chloroform | - | $4.77 \mathrm{E}-01$ | $4.77 \mathrm{E}-01$ |
| 110827 | cyclohexane | $2.86 \mathrm{E}-03$ | - | $2.86 \mathrm{E}-03$ |
| 100414 | ethylbenzene | $3.29 \mathrm{E}-04$ | $2.31 \mathrm{E}+00$ | $2.31 \mathrm{E}+00$ |
| 78784 | isopentane | $1.04 \mathrm{E}-01$ | - | $1.04 \mathrm{E}-01$ |
| 98828 | isopropylbenzene (cumene) | $3.06 \mathrm{E}-05$ | - | $3.06 \mathrm{E}-05$ |
|  | methylene chloride | - | $8.17 \mathrm{E}+00$ | $8.17 \mathrm{E}+00$ |
| 108383 | m-xylene | $9.55 \mathrm{E}-04$ | - | $9.55 \mathrm{E}-04$ |
| 110543 | n-hexane | $4.29 \mathrm{E}-03$ | - | $4.29 \mathrm{E}-03$ |
| 95476 | o-xylene | $3.57 \mathrm{E}-04$ | - | $3.57 \mathrm{E}-04$ |
| 106423 | p-xylene | $2.98 \mathrm{E}-04$ | - | $2.98 \mathrm{E}-04$ |
| 108883 | toluene | $4.74 \mathrm{E}-03$ | $2.65 \mathrm{E}+00$ | $2.66 \mathrm{E}+00$ |
| 1330207 | xylene (total) | - | $4.77 \mathrm{E}+00$ | $4.77 \mathrm{E}+00$ |
| Total |  | 1.22E-01 | $1.95 \mathrm{E}+01$ | $1.96 \mathrm{E}+01$ |

Summary of Emissions from Locomotives
Colton Rail Yard, Bloomington, CA

| Activity | DPM Emissions <br> (tpy) |
| :--- | :---: |
| Through Trains and Power Mov | 0.51 |
| Freight Trains | 2.45 |
| Local Trains | 0.47 |
| Power Moves in Yard | 0.14 |
| Hump Operations | 4.74 |
| Trim Operations | 5.28 |
| Crew Changes | 0.07 |
| Service Movements | 0.06 |
| Service Idling | 2.14 |
| Load Testing | 0.44 |
|  |  |
| Total | $\mathbf{1 6 . 3 0}$ |

Summary of Emissions from Diesel-Fueled Yard Trucks Colton Rail Yard, Bloomington, CA
Running Exhaust Emissions

| Equipment | Equipment | Ve |
| :---: | :---: | ---: |
| Type | ID/Owner | ID |
| Truck | Engineering | 69 |
| Truck | Engineering | 69 |
| Truck | Car Dept | $1915-7$ |
| Truck | Engineering | 9007 |
| Truck | Engineering | 90 |
| Truck | Engineering | 903 |
| Truck | Engineering | 90 |
| Truck | Car Dept | Na |
| Truck | Engineering | 64 |
| Truck | Car Dept | 1915 |
| Total |  |  |

## Idling Exhaust Emissions

| Equipment Type | Equipment ID/Owner | Vehicle ID | Make/Model | Year | Vehicle Class | Idling ${ }^{1}$ |  | Emission Factors (g/hr) ${ }^{2}$ |  |  |  |  |  | Emissions (tpy) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | (min/day) | (hr/yr) | ROG | CO | NOx | PM10 | DPM | SOx | ROG | CO | NOx | PM10 | DPM | SOx |
| Truck | Engineering | 69496 | Chevy CK 3500 | 1998 | LDT | 15 | 91.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 69499 | Chevy CK 3500 | 1998 | LDT | 15 | 91.25 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Truck | Car Dept | 1915-73119 | Ford F-450 | 2003 | LHDT2 | 15 | 91.25 | 3.17 | 26.30 | 75.05 | 0.75 | 0.75 | 0.34 | 0.000 | 0.003 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 9007E | Ford F-800 | 1992 | MHD | 15 | 91.25 | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 | 0.000 | 0.003 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 9009E | Ford F-800 | 1992 | MHD | 15 | 91.25 | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 | 0.000 | 0.003 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 9031 E | Ford F-800 | 1992 | MHD | 15 | 91.25 | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 | 0.000 | 0.003 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 9018 E | Ford F-800 | 1992 | MHD | 15 | 91.25 | 3.17 | 26.30 | 75.05 | 1.40 | 1.40 | 0.34 | 0.000 | 0.003 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Car Dept | NA | International | 1987 | HHD | 15 | 91.25 | 22.84 | 61.55 | 82.94 | 4.28 | 4.28 | 0.55 | 0.002 | 0.006 | 0.008 | 0.000 | 0.000 | 0.000 |
| Truck | Engineering | 64274 | Ford LT8000 | 1989 | HHD | 15 | 91.25 | 19.45 | 58.49 | 85.53 | 3.43 | 3.43 | 0.55 | 0.002 | 0.006 | 0.009 | 0.000 | 0.000 | 0.000 |
| Truck | Car Dept | 1915-9038E | Ford LT9000 | 1997 | HHD | 15 | 91.25 | 12.41 | 49.53 | 110.27 | 1.93 | 1.93 | 0.55 | 0.001 | 0.005 | 0.011 | 0.000 | 0.000 | 0.000 |
| Total |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.007 | 0.030 | 0.066 | 0.002 | 0.002 | 0.000 |

[^14]Summary of Emissions from HHD Diesel-Fueled Delivery Trucks Dolores and ICTF Rail Yards, Long Beach, CA

| Delivery <br> Type | TruckTrips$(\text { trips } / \mathrm{yr})^{1,2}$ | $\begin{aligned} & \hline \text { VMT per } \\ & \text { Trip } \\ & (\text { mi/trip })^{3} \\ & \hline \end{aligned}$ | VMT per <br> Year | 2005 Emission Factors (g/mi) ${ }^{4,5}$ |  |  |  |  |  | 2005 Emission Estimates (tons/yr) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ROG | CO | NOx | PM10 ${ }^{6}$ | $\mathrm{DPM}^{6}$ | SOx | ROG | CO | NOx | PM10 | DPM | SOx |
| Gasoline | 2 | 0.33 | 0.66 | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Lube Oil | 57 | 0.58 | 33.06 | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Used Oil | 24 | 0.58 | 13.92 | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Soap | 18 | 0.71 | 12.78 | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Sand | 195 | 0.58 | 113.10 | 6.40 | 17.23 | 28.68 | 2.53 | 2.47 | 0.24 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Total | 296 |  |  |  |  |  |  |  |  | 1.22E-03 | 3.30E-03 | 5.49E-03 | 4.84E-04 | 4.72E-04 | 4.64E-05 |


| Delivery <br> Type | Number of <br> Truck Trips | Idling |  | 2005 Emission Factors (g/hr) ${ }^{8}$ |  |  |  |  |  | 2005 Emission Estimates (tons/yr) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (mins/trip) ${ }^{7}$ | (hr/yr) | ROG | CO | NOx | PM10 | DPM | SOx | ROG | CO | NOx | PM10 | DPM | SOx |
| Gasoline | 2 | 10 | 0.33 | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Lube Oil | 57 | 10 | 9.50 | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Used Oil | 24 | 10 | 4.00 | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Soap | 18 | 10 | 3.00 | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Sand | 195 | 30 | 97.50 | 16.16 | 52.99 | 100.38 | 2.85 | 2.85 | 0.55 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| Total | 296 |  |  |  |  |  |  |  |  | 2.04E-03 | 6.68E-03 | 1.27E-02 | 3.59E-04 | 3.59E-04 | 6.93E-05 |

[^15]Notes:
Notes:

1. Lube oil and journal box oil throughput based on 2003 Trinity Report. Assumptions confirmed by UPRR staff. 2. Diesel throughput provided by UPRR staff. Diesel fuel is delivered via Kinder Morgan pipeline.
2. Stormwater thoughput is equal to WWTP throughput, equally divided between tanks.
3. Soap throughput provided by UPRR staff
4. Used oil throughput is based on the 2005 facility used oil total (191,867 gallons) and was allocated to tanks based on the assumptions in 2003 Trinity Report.
The 2003 tank specific throughput was divided by the total throughput to determine the percent of the total handeled by each tank. This allocation was
then applied to the 2005 total throughput.
5. VOC emissions were calculated for tanks that were not exempt from SMAQMD permitting rules only
Toxic Air Contaminant Emissions from the Gasoline Storage Tank Colton Rail Yard, Bloomington, CA

| Profile ${ }^{1}$ | CAS | Chemical Name | Organic <br> Fraction | 2005 Emission Estimates (tpy) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Tank \#1172 | Tank \#1187 | Tank \#1189 | Tank \#1498 | Total |
| 661 | 540841 | 2,2,4-trimethylpentane | 0.0129 | $7.71 \mathrm{E}-04$ | $9.52 \mathrm{E}-04$ | $9.79 \mathrm{E}-04$ | $9.04 \mathrm{E}-04$ | $3.61 \mathrm{E}-03$ |
| 661 | 71432 | benzene | 0.0036 | $2.14 \mathrm{E}-04$ | $2.65 \mathrm{E}-04$ | $2.72 \mathrm{E}-04$ | $2.51 \mathrm{E}-04$ | $1.00 \mathrm{E}-03$ |
| 661 | 110827 | cyclohexane | 0.0103 | $6.12 \mathrm{E}-04$ | $7.56 \mathrm{E}-04$ | $7.77 \mathrm{E}-04$ | $7.18 \mathrm{E}-04$ | $2.86 \mathrm{E}-03$ |
| 661 | 100414 | ethylbenzene | 0.0012 | $7.03 \mathrm{E}-05$ | $8.68 \mathrm{E}-05$ | $8.92 \mathrm{E}-05$ | $8.24 \mathrm{E}-05$ | $3.29 \mathrm{E}-04$ |
| 661 | 78784 | isopentane | 0.3734 | $2.22 \mathrm{E}-02$ | $2.75 \mathrm{E}-02$ | $2.82 \mathrm{E}-02$ | $2.61 \mathrm{E}-02$ | $1.04 \mathrm{E}-01$ |
| 661 | 98828 | isopropylbenzene (cumene) | 0.0001 | $6.55 \mathrm{E}-06$ | $8.09 \mathrm{E}-06$ | $8.32 \mathrm{E}-06$ | $7.68 \mathrm{E}-06$ | $3.06 \mathrm{E}-05$ |
| 661 | 108383 | m-xylene | 0.0034 | $2.04 \mathrm{E}-04$ | $2.52 \mathrm{E}-04$ | $2.59 \mathrm{E}-04$ | $2.40 \mathrm{E}-04$ | $9.55 \mathrm{E}-04$ |
| 661 | 110543 | n-hexane | 0.0154 | $9.18 \mathrm{E}-04$ | $1.13 \mathrm{E}-03$ | $1.16 \mathrm{E}-03$ | $1.08 \mathrm{E}-03$ | $4.29 \mathrm{E}-03$ |
| 661 | 95476 | o-xylene | 0.0013 | $7.62 \mathrm{E}-05$ | $9.41 \mathrm{E}-05$ | $9.68 \mathrm{E}-05$ | $8.94 \mathrm{E}-05$ | $3.57 \mathrm{E}-04$ |
| 661 | 106423 | p-xylene | 0.0011 | $6.37 \mathrm{E}-05$ | $7.87 \mathrm{E}-05$ | $8.09 \mathrm{E}-05$ | $7.47 \mathrm{E}-05$ | $2.98 \mathrm{E}-04$ |
| 661 | 108883 | toluene | 0.0170 | $1.01 \mathrm{E}-03$ | $1.25 \mathrm{E}-03$ | $1.29 \mathrm{E}-03$ | $1.19 \mathrm{E}-03$ | $4.74 \mathrm{E}-03$ |
| Total |  |  |  | 2.62E-02 | 3.23E-02 | 3.32E-02 | 3.07E-02 | 1.22E-01 |

[^16]Summary of Emissions from Sand Tower Operations
Colton Rail Yard, Bloomington, CA

|  | 2005 Sand | Pneumatic Transfer |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Pollutant | Gravity Transfer <br> (ton/yr) | Emission Factor <br> (lb/ton) | Emission Factor <br> (lb/ton) | Process Emissions (lb/yr) <br>  <br> Transfer |  |  |
| PM10 | 3885.42 | 0.00034 | 0.0009 | Travity <br> Transfer | Total |  |

Notes:

1. Sand throughput provided by Union Pacific
2. Pneumatic transfer emission factor from AP-42, Table 11.12-2, 6/06. Factor for controlled pneumatic cement unloading to elevated storage silo was used. The unit is equipped with a fabric filter.
3. Gravity transfer emission factor from AP-42, Table 11.12-2, 6/06. Factor for sand transfer was used.
4. There are no TAC emissions from this source.

Toxic Air Contaminant Emissions the Wastewater Treatment Plant
Colton Rail Yard, Bloomington, CA

| Pollutant | Emission Rate |  | 2005 Emissions |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $(\mathrm{lb} / \mathrm{yr})$ | $(\mathrm{g} / \mathrm{sec})$ | $(\mathrm{lb} / \mathrm{yr})$ | $($ tpy $)$ |
| Benzene | 0.22 | $3.16 \mathrm{E}-06$ | $3.36 \mathrm{E}-01$ | $1.68 \mathrm{E}-04$ |
| Bromomethane | 0.84 | $1.21 \mathrm{E}-05$ | $1.28 \mathrm{E}+00$ | $6.41 \mathrm{E}-04$ |
| Chloroform | 0.43 | $6.18 \mathrm{E}-06$ | $6.56 \mathrm{E}-01$ | $3.28 \mathrm{E}-04$ |
| Ethylbenzene | 1.36 | $1.96 \mathrm{E}-05$ | $2.08 \mathrm{E}+00$ | $1.04 \mathrm{E}-03$ |
| Methylene Chloride | 7.50 | $1.08 \mathrm{E}-04$ | $1.14 \mathrm{E}+01$ | $5.72 \mathrm{E}-03$ |
| Toluene | 3.02 | $4.34 \mathrm{E}-05$ | $4.61 \mathrm{E}+00$ | $2.31 \mathrm{E}-03$ |
| Xylene | 5.42 | $7.80 \mathrm{E}-05$ | $8.27 \mathrm{E}+00$ | $4.14 \mathrm{E}-03$ |
| Total | $\mathbf{1 8 . 7 9}$ | $\mathbf{2 . 7 0 E - 0 4}$ | $\mathbf{2 8 . 6 8}$ | $\mathbf{1 . 4 3 E - 0 2}$ |

1. Emission rates are from the Air Emissions Inventory and Regulatory Analysis Report for Colton Yard, Trinity Consultants, May 30, 2003.
2. Emission rates are from the July 2002 Permit to Operate Application and are based on a wastewater flow rate of 15,500 gallons per day ( $5,657,500$ gallons per year).
3. Emissions ( $\mathrm{lb} / \mathrm{yr}$ ) were calculated multipling the emission rate by the ratio of the 2002 wasterwater flow rate and the 2005 wastewater flow rate.
$\mathrm{lb} / \mathrm{yr}=$ Emission Rate $(\mathrm{lb} / \mathrm{yr}) \times(8,636,710 \mathrm{gal} / \mathrm{yr} / 5,657,500 \mathrm{gal} / \mathrm{yr})$
4. The 2005 wastewater flow rate was $8,636,710$ gallons, per T.D. Wash.
Summary of Emissions from the Emergency Generator
Colton Rail Yard, Bloomington, CA

|  |  | Fuel | Rating | Annual of Operation | Emission Factors (g/hp-hr) |  |  |  |  |  | Emission (tpy) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Equipment Type | Type | (hp) | (hr/yr) | ROG | CO | NOx | PM10 | DPM | SOx | ROG | CO | NOx | PM10 | DPM | SOx |
| Bowl Area | Emergency Generator | Diesel | 50 | 20 | 1.14 | 3.03 | 14.06 | 1.00 | 1.00 | 0.93 | 0.001 | 0.003 | 0.016 | 0.001 | 0.001 | 0.001 |

1. CARB's ATCM for Stationary Compression Ignition Engines limits non-emergency operation to 20 hours per year.
2. Emission factors from AP-42, Table 3.3-1, 10/96.

Equipment Specifications for Boilers and Heaters
Colton Rail Yard, Bloomington, CA

|  | Heater <br> Type | Fuel Type | Rating <br> (MMBtu/hr) |
| :--- | :---: | :---: | :---: |
| Location | Heater | Natural Gas | 0.14 |
| Locomotive Wash $^{1}$ | Boiler | Natural Gas | 1.995 |
| Locomotive Wash $^{1}$ | Boiler | Natural Gas | 2.5 |

## Notes:

1. These units are exempt from SCAQMD permitting requirements per Rule 219 (b)(2).
2. This unit was installed in 2006, and therefore, did not operate in 2005.

Equipment Specifications for Welders
Colton Rail Yard, Bloomington, CA

|  |  |  |  | Make |
| :--- | :---: | :---: | :---: | :---: |
| Location | Model | Fuel Type | Rating <br> $(\mathrm{hp})$ |  |
| Receiving Yard | Lincoln | Ranger 8 | Gasoline | 16 |
| Receiving Yard | Miller | Blue Star | Gasoline | 12.5 |
| Receiving Yard | Miller | Blue Star | Gasoline | 13 |
| One Spot | Miller | Blue Star 6000 | Gasoline | 13 |
| One Spot | Miller | Blue Star 6000 | Gasoline | 13 |
| One Spot | Miller | Blue Star 6000 | Gasoline | 13 |
| One Spot | Miller | Blue Star 145 | Gasoline | 10 |
| One Spot | Miller | Blue Star 145 | Gasoline | 10 |
| One Spot | Miller | Blue Star | Gasoline | 13 |
| One Spot | Miller | Blue Star 180K | Gasoline | 13 |
| Departure Yard | Miller | Blue Star | Gasoline | 12.5 |
| Departure Yard | Miller | Blue Star | Gasoline | 13 |
| Departure Yard | Miller | Blue Star | Gasoline | 13 |
| Service Track | Miller | Blue Star | Gasoline | 13 |
| Service Track | Miller | Blue Star | Gasoline | 13 |
| Service Track | Miller | Unknown | Gasoline | 13 |

Notes:

1. Welding equipment is exempt from SCAQMD permitting requirements per Rule 219(e)(8).
2. IC Engines meet the exempt requirements of SCAQMD Rule 219(b)(1).

Equipment Specifications for Steam Cleaners
Colton Rail Yard, Bloomington, CA

| Location | Make | Emission <br> Unit | Fuel Type | Rating <br> (MMBtu/hr or hp) |
| :--- | :---: | :---: | :---: | :---: |
| Locomotive Shop | Hydroblaster | Pump | Electirc | NA |
|  |  | Heater | Propane | 0.360 |
| Wheel Shop | Hydroblaster | Pump | Electirc | NA |
|  |  | Heater | Propane | 0.360 |

Notes:

1. These units are exempt from SCAQMD permitting requirements per Rule 219(d)(5) and (b)(2).

Specifications for Miscellaneous Combustion Equipment
Colton Rail Yard, Bloomington, CA

| Location | Equipment Type | Fuel Type | Rating <br> (hp or MMBtu/hr) |
| :--- | :---: | :---: | :---: |
| Service Track | Pressure Washer ${ }^{1}$ | Propane | 0.325 |
| Service Track | Pressure Washer ${ }^{1}$ | Propane | 0.325 |
| Service Track | Pressure Washer ${ }^{1}$ | Propane | 0.325 |
| Service Track | Pressure Washer ${ }^{1}$ | Propane | 0.325 |
| One Spot | Air Compressor ${ }^{2}$ | Gasoline | 8 |
| One Spot | Air Compressor ${ }^{2}$ | Gasoline | 11 |
| Bridge Department | Air Compressor ${ }^{2}$ | Diesel | 42 |

1. These units are exempt from SCAQMD permitting requirements per Rule 219 (b)(2).
2. These units are exempt from SCAQMD permitting requirements per Rule 219(b)(1).

## APPENDIX G

DETAILED RISK SCREENING CALCULATIONS

Summary of Risk Index Values
Colton Rail Yard, Bloomington, CA

| Source | Risk Index Value <br> Cancer | \% of Total <br> Cancer Risk | Risk Index Value <br> Chronic | \% of Total <br> Chronic Risk |
| :--- | :---: | :---: | :---: | :---: |
| Locomotives | $4.89 \mathrm{E}-03$ | 98.54 | $8.15 \mathrm{E}+01$ | 56.42 |
| Yard Trucks | $5.72 \mathrm{E}-05$ | 1.15 | $9.53 \mathrm{E}-01$ | 0.66 |
| HHD Diesel-Fueled Delivery Trucks | $2.49 \mathrm{E}-07$ | 0.01 | $4.15 \mathrm{E}-03$ | 0.00 |
| Heavy Equipment | $1.44 \mathrm{E}-05$ | 0.29 | $2.41 \mathrm{E}-01$ | 0.17 |
| WWTP | $1.23 \mathrm{E}-08$ | 0.00 | $8.06 \mathrm{E}+00$ | 5.58 |
| Sand Tower | $0.00 \mathrm{E}+00$ | 0.00 | $0.00 \mathrm{E}+00$ | 0.00 |
| Gasoline Storage Tanks | $4.69 \mathrm{E}-08$ | 0.00 | $5.37 \mathrm{E}+01$ | 37.17 |
| Emergency Generator | $3.30 \mathrm{E}-07$ | 0.01 | $5.50 \mathrm{E}-03$ | 0.00 |
| Total | $4.96 \mathrm{E}-03$ | 100.00 |  |  |

Notes:

1. There are no TAC emissions from the sand tower or the Diesel fuel storage tanks.

Calculation of Risk Index Values for Diesel-Fueled Sources
Colton Rail Yard, Bloomington, CA

| Source | DPM Emissions <br> (tpy) | Unit Risk Factor <br> Cancer | Cancer Risk <br> Index Value | Unit Risk Factor <br> Chronic | Chronic Risk <br> Index Value |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Locomotives | 16.30 | $3.00 \mathrm{E}-04$ | $4.89 \mathrm{E}-03$ | $5.00 \mathrm{E}+00$ | $8.15 \mathrm{E}+01$ |
| Yard Trucks | 0.19 | $3.00 \mathrm{E}-04$ | $5.72 \mathrm{E}-05$ | $5.00 \mathrm{E}+00$ | $9.53 \mathrm{E}-01$ |
| HHD Diesel-Fueled Delivery Trucks | 0.00 | $3.00 \mathrm{E}-04$ | $2.49 \mathrm{E}-07$ | $5.00 \mathrm{E}+00$ | $4.15 \mathrm{E}-03$ |
| Heavy Equipment | 0.05 | $3.00 \mathrm{E}-04$ | $1.44 \mathrm{E}-05$ | $5.00 \mathrm{E}+00$ | $2.41 \mathrm{E}-01$ |
| Emergency Generator | 0.00 | $3.00 \mathrm{E}-04$ | $3.30 \mathrm{E}-07$ | $5.00 \mathrm{E}+00$ | $5.50 \mathrm{E}-03$ |
| Total |  |  |  |  | $\mathbf{8 . 2 7 E}+\mathbf{0 1}$ |

Notes:

1. Unit risk factor from Consolidated Table of OEHHA/ARB Approved Risk Assessment Health Values, April 25, 2005. Cancer inhalation risk used.
Calculation of Risk Index Values for TAC Sources
Colton Rail Yard, Bloomington, CA

|  |  | Emission | (tpy) | Unit Risk Factor | Unit Risk Factor | Cancer Risk In | dex Value | Chronic Risk | dex Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CAS | Chemical Name | Gasoline Tanks | WWTP | Cancer | Chronic | Gasoline Tank | WWTP | Gasoline Tank | WWTP |
| 540841 | 2,2,4-trimethylpentane | $5.81 \mathrm{E}-03$ | - |  |  |  |  |  |  |
| 71432 | Benzene | $1.62 \mathrm{E}-03$ | $1.68 \mathrm{E}-04$ | $2.90 \mathrm{E}-05$ | $6.00 \mathrm{E}+01$ | $4.69 \mathrm{E}-08$ | 4.87E-09 | $9.70 \mathrm{E}-02$ | $1.01 \mathrm{E}-02$ |
|  | Bromomethane | - | 6.41E-04 |  |  |  |  |  |  |
| 67663 | Chloroform | - | $3.28 \mathrm{E}-04$ | 5.30E-06 | $3.00 \mathrm{E}+02$ |  | $1.74 \mathrm{E}-09$ |  | $9.85 \mathrm{E}-02$ |
| 110827 | Cyclohexane | $4.62 \mathrm{E}-03$ | - |  |  |  |  |  |  |
| 100414 | Ethylbenzene | $5.30 \mathrm{E}-04$ | $1.04 \mathrm{E}-03$ |  | $2.00 \mathrm{E}+03$ |  |  | $1.06 \mathrm{E}+00$ | $2.08 \mathrm{E}+00$ |
| 78784 | isopentane | $1.68 \mathrm{E}-01$ | - |  |  |  |  |  |  |
| 98828 | Isopropylbenzene (cumene) | 4.94E-05 | - |  |  |  |  |  |  |
| 75092 | Methylene Chloride | - | 5.72E-03 | $1.00 \mathrm{E}-06$ | $4.00 \mathrm{E}+02$ |  | 5.72E-09 |  | $2.29 \mathrm{E}+00$ |
| 108383 | m -xylene | $1.54 \mathrm{E}-03$ | - |  | $7.00 \mathrm{E}+02$ |  |  | $1.08 \mathrm{E}+00$ |  |
| 110543 | n-hexane | $6.92 \mathrm{E}-03$ | - |  | $7.00 \mathrm{E}+03$ |  |  | $4.84 \mathrm{E}+01$ |  |
| 95476 | o-xylene | $5.75 \mathrm{E}-04$ | - |  | $7.00 \mathrm{E}+02$ |  |  | $4.02 \mathrm{E}-01$ |  |
| 106423 | p-xylene | $4.80 \mathrm{E}-04$ | - |  | $7.00 \mathrm{E}+02$ |  |  | $3.36 \mathrm{E}-01$ |  |
| 108883 | Toluene | 7.64E-03 | $2.31 \mathrm{E}-03$ |  | $3.00 \mathrm{E}+02$ |  |  | $2.29 \mathrm{E}+00$ | 6.92E-01 |
| 1330207 | Xylene (total) | - | 4.14E-03 |  | $7.00 \mathrm{E}+02$ |  |  |  | $2.90 \mathrm{E}+00$ |
| Total |  | 1.97E-01 | 1.4E-02 |  |  | 4.69E-08 | 1.23E-08 | 5.37E +01 | 8.06E+00 |

# APPENDIX H <br> SOURCE TREATMENT AND ASSUMPTIONS FOR AIR DISPERSION MODELING FOR NON-LOCOMOTIVE SOURCES 

## Appendix H

## Source Treatment and Assumptions for Air Dispersion Modeling for NonLocomotive Sources

As shown in Figure 2, emissions were allocated spatially throughout the Yard in the areas where each source type operates or is most likely to operate. Emissions from mobile sources, heavy equipment, and moving locomotives were simulated as a series of volume sources along their corresponding travel routes and work areas. Emissions from heavy equipment were first allocated to the areas of the yard where their activity occurs, and were then allocated uniformly to a series of sources within the defined areas.

Emissions from stationary sources, such as fuel tanks, were simulated as a point source corresponding to the actual equipment location within the Yard. Assumptions used spatially to allocate emissions for each source group are shown in the Table below. See Figure 2 for the source locations. See Appendix A-4 for assumptions regarding the spatial allocation of locomotive emissions.

| Source Treatment and Assumptions for Air Dispersion Modeling for NonLocomotive Sources Colton Rail Yard |  |  |
| :---: | :---: | :---: |
| Source | Source Treatment | Assumptions for Spatial Allocation of Emissions |
| Gasoline Storage Tanks | Point | Assumed all emissions occurred at the storage tank location. |
| WWTP | Point | Assumed all emissions occurred at the storage tank location. |
| Heavy Equipment (idling and traveling) | Volume | Rail Cleaner - allocated all emissions to the area in and around locomotive shop volume source. <br> Rerailer, Lorain Crane, and Forklift - allocated all emissions to area in and around the One Spot as volume sources. |

APPENDIX I
SEASONAL AND DIURNAL ACTIVITY PROFILES

## Appendix I

## Development of Temporal Activity Profiles for the UPRR Colton Yard

Locomotive activity can vary by time of day and season. For each yard, the number of trains arriving and departing from the yard in each month and each hour of the day was tabulated and used to develop temporal activity profiles for modeling. The number of locomotives released from service facilities in each month was also tabulated. The AERMOD EMISFACT SEASHR option was used to adjust emission rates by season and hour of the day, and the EMISFACT SEASON option was used where only seasonal adjustments were applied. Where hour of day adjustments (but not seasonal) were applied, the EMISFACT HROFDY option was used.
Time of day profiles for train idling activity were developed assuming that departure events involved locomotive idling during the hour of departure and the preceding hour, and that arrival events involved locomotive idling during the hour of arrival only. Thus, the hourly activity fraction for departing trains during hour $i$ is given by

$$
\frac{1 / 2 \cdot \sum_{j=i}^{i} N D(j)}{\sum_{j=1}^{24} N D(j)},
$$

and that for arriving trains during hour $i$ is given by

$$
\frac{N A(i)}{\sum_{j=1}^{24} N A(j)}
$$

where $N A(j)$ and $N D(j)$ are respectively the number of arriving and departing trains in hour $j$. The hourly adjustment factor for idling is then calculated as 24 times the average of the departing and arriving idle time fractions. These factors were applied to both idling on arriving and departing trains.
Similarly, time of day profiles for road power movements in the yard (arrivals, departures, and power moves) were developed without including arrivals in preceding hours and departures in subsequent hours. In this case, the hourly activity adjustment factor for hour $i$ is given by

$$
\frac{N A(i)+N D(i)}{\sum_{j=1}^{24}(N A(j)+N D(j))} .
$$

Seasonal adjustment factors are calculated as the sum of trains arriving and departing in each three month season, divided by the total number of arrivals and departures for the
year. The hourly adjustment factors for each season are simply the product of the seasonal adjustment factor and the 24 hourly adjustment factors.
The seasonal profile for train activity at Colton was applied for yard switching operations, but no hourly factors were applied since the hump and trim sets work 24/7. Similarly, a seasonal profile was developed for Service Track and maintenance activities based on monthly Service Track release counts. No hourly factor was applied to either service idling or load testing.
Table I-1 lists the hourly activity factors derived for train movements and train idling at the UPRR Colton Yard. Separate temporal profiles are listed for day and night moving emissions as different volume source parameters are used for day and night. Table I-2 lists the seasonal activity factors for train and yard operations, and service and load test activity.

Table I-1. Hourly Activity Factors for Train Activity at the UPRR Colton Yard

| Hour | Train Idling | Train Movements <br> (Daytime) | Train Movements <br> (Nighttime) |
| :---: | :---: | :---: | :---: |
| 1 | 1.070 | 0.000 | 1.138 |
| 2 | 0.871 | 0.000 | 0.938 |
| 3 | 0.947 | 0.000 | 0.887 |
| 4 | 0.936 | 0.000 | 0.950 |
| 5 | 0.913 | 0.000 | 0.960 |
| 6 | 0.949 | 0.000 | 0.933 |
| 7 | 0.965 | 0.912 | 0.000 |
| 8 | 1.101 | 1.031 | 0.000 |
| 9 | 1.072 | 1.039 | 0.000 |
| 10 | 1.121 | 1.131 | 0.000 |
| 11 | 1.047 | 1.055 | 0.000 |
| 12 | 0.972 | 1.009 | 0.000 |
| 13 | 0.843 | 0.960 | 0.000 |
| 14 | 0.717 | 0.726 | 0.000 |
| 15 | 0.821 | 0.752 | 0.000 |
| 16 | 0.955 | 0.909 | 0.000 |
| 17 | 1.017 | 0.980 | 0.000 |
| 18 | 1.135 | 1.092 | 0.000 |
| 19 | 1.228 | 0.000 | 1.282 |
| 20 | 1.116 | 0.000 | 1.136 |
| 21 | 1.059 | 0.000 | 1.117 |
| 22 | 0.976 | 0.000 | 0.992 |
| 23 | 1.028 | 0.000 | 0.968 |
| 24 | 1.142 | 0.000 | 1.104 |

Table I-2. Seasonal Activity Factors for the UPRR Colton Yard

| Activity Type | Winter | Spring | Summer | Fall |
| :---: | :---: | :---: | :---: | :---: |
| Trains | 0.921 | 1.037 | 1.027 | 1.015 |
| Service | 0.994 | 0.956 | 1.041 | 1.009 |

## APPENDIX J

SELECTION OF POPULATION FOR THE URBAN OPTION INPUT IN AERMOD AIR DISPERSION MODELING ANALYSIS

## Appendix J

## Selection of Population for the Urban Option Input in AERMOD Air Dispersion Modeling Analysis

Urban heat islands and the thermal domes generated by them extend over an entire urbanized area ${ }^{1}$. Hot spots within the urban heat island are associated with roads and roofs, which surround each Union Pacific (UP) rail yard in high density. Following guidance cited by the ARB ("For urban areas adjacent to or near other urban areas, or part of urban corridors, the user should attempt to identify that part of the urban area that will contribute to the urban heat island plume affecting the source."), it is the entire metropolitan area that contributes to the urban heat island plume affecting the rail yard. For metropolitan areas containing substantial amounts of open water, the area of water should not be included.

To simulate the effect of the urban heat island on turbulence in the boundary layer, especially at night, when the effect is substantial, AERMOD adjusts the height of the nighttime urban boundary layer for the heat flux emitted into the boundary layer by the urban surface, which is warmer than surrounding rural areas ${ }^{2,3}$. The difference between the urban and rural boundary layer temperatures is proportional to the maximum temperature difference of 12 Celsius degrees observed in a study of several Canadian cities, and directly related to the logarithm of the ratio of the urban population to a reference population of $2,000,000$ (i.e., Montreal, the Canadian city with the maximum urban-rural temperature difference) ${ }^{4}$.

The adjusted height of the nocturnal urban boundary layer is proportional to the onefourth power of the ratio of the population of the city of interest to the reference population, based on the observation that the convective boundary layer depth is proportional to the square root of the city size, and city size is roughly proportional to the square root of its population, assuming constant population density ${ }^{5}$. Regardless of wind direction during any specific hour used by AERMOD, it is the entire metropolitan area, minus bodies of water, which moves additional heat flux into the atmosphere and affects its dispersive properties, not just the $400 \mathrm{~km}^{2}$ area of the air dispersion modeling domain that surrounds the each rail yard, which was chosen purely for modeling convenience.

Continuing to follow the guidance cited by the ARB ("If this approach results in the identification of clearly defined MSAs, then census data may be used as above to determine the appropriate population for input to $A E R M O D$ "), the population of each Metropolitan Statistical Area, or a smaller area if appropriate, is being used in the modeling run for each rail yard.

[^17]
## APPENDIX K

DEMOGRAPHIC DATA

## Appendix K

## Population Shape Files for UPRR Rail Yards

The accompanying shape files include census boundaries as polygons and the corresponding residential populations from the 2000 U.S. Census. Separate shape files are included at the tract, block group, and block levels. The primary ID for each polygon begins with ssccctttttt, where $s s$ is the FIPS state code ( 06 for California), $c c$ is the county code, and $t t t t t$ is the tract code. The primary IDs for block groups have a single additional digit which is the block group number within each tract. Those for blocks have four additional digits identifying the block number. The population for each polygon are included as both the secondary ID and as attribute 1. Polygon coordinates are UTM zone 10 (Oakland and Stockton) or 11 (southern California yards), NAD83, in meters. The files contain entire tracts, block groups, or blocks that are completely contained within a specified area. For all yards except Stockton, the area included extends 10 kilometers beyond the $20 \times 20$ kilometer modeling domains. For Stockton, this area was extended to 20 kilometers beyond the modeling domain boundaries to avoid excluding some very large blocks.
In merging the population data ${ }^{1}$ with the corresponding boundaries ${ }^{2}$, it was noted that at all locations, there are defined census areas (primarily blocks, but in some cases block groups and tracts) for which there are no population records listed in the population files. Overlaying these boundaries on georeferenced aerial photos indicates that these are areas that likely have no residential populations (e.g., industrial areas and parks). The defined areas without population data have been excluded from these files. Areas with an identified population of zero have been included. It was also observed that some blocks, block groups and tracts with residential populations cover both residential areas and significant portions of the rail yards themselves. For this reason, any analysis of population exposures based on dispersion modeling should exclude receptors that are within the yard boundaries or within 20 meters of any modeled emission source locations.

To facilitate the exclusion of non-representative receptors, separate shape files have been generated that define the area within 20 meters of the yard boundaries for each yard. These files are also included with the accompanying population files. It should also be noted that the spatial extent of individual polygons can vary widely, even within the same type. For example, single blocks may be as small as 20 meters or as large as 10,000 meters or more in length. To estimate populations contained within specific areas, it may prove most useful to generate populations on a regular grid (e.g., $250 \times 250 \mathrm{~m}$ cells) rather than attempting to process irregularly shaped polygons.

[^18]
[^0]:    ${ }^{1}$ The Yard is referred to by a variety of names, including the West Colton Yard. In this report, the facility will be called the Colton Yard, for consistency with the MOU.

[^1]:    ${ }^{2}$ In 2005, the locomotive shop was under construction. Prior to the opening of the new shop, locomotive maintenance was done at the Service Track.
    ${ }^{3}$ In 2005, the wheel shop was under construction and not operational.

[^2]:    ${ }^{4}$ Power moves are a group of locomotives with no attached railcars, whose objective is either to move locomotives to locations where they are needed, or to take malfunctioning units to service facilities. In general, only one or two locomotives in the consist are in operation during power moves.

[^3]:    ${ }^{5}$ UP personnel report that although the train data records for power moves may show all locomotives "working," in actuality all locomotives except for one at the front and rear end (and more commonly only one at the front end) are shut down as they are not needed to pull a train that consists only of locomotives. Assuming 1.5 working locomotives per power move may slightly overestimate the actual average number of working locomotives per power move.

[^4]:    ${ }^{6}$ Foreign locomotives are locomotives not owned by UPRR, including passenger trains and locomotives owned by other railroads that are brought onto the UPRR system via interchange.
    ${ }^{7}$ Ireson, R.G., M.J. Germer, L.A. Schmid (2005). "Development of Detailed Rail yard Emissions to Capture Activity, Technology, and Operational Changes." Proceedings of the USEPA $14^{\text {th }}$ Annual Emission Inventory Conference, http://www.epa.gov/ttn/chief/conference/ei14/session8/ireson.pdf, Las Vegas NV, April 14, 2006.
    ${ }^{8}$ Emission estimates are based on the total number of working locomotives. Therefore, the total number of locomotives used in the emission calculations will be slightly lower than the total number of locomotives shown in Table 1. See Appendix A for detailed emission calculations

[^5]:    ${ }^{9}$ There are two primary types of auto start/stop technology—"Auto Engine Start Stop" (AESS), which is factory-installed on recent model high-horsepower units; and the ZTR "SmartStart" system (ZTR), which is a retrofit option for other locomotives. Both are programmed to turn off the Diesel engine after 15 to 30 minutes of idling, provided that various criteria (air pressure, battery charge, and others) are met. The engine automatically restarts if required by one of the monitored parameters. We assume that an AESS/ZTR-equipped locomotive will shut down after 30 minutes of idling in an extended idle event.

[^6]:    ${ }^{10}$ Personal communication from Theron Hinckley of Chevron Products Company to Jon Germer of UPRR and Rob Ireson, December 13, 2006.

[^7]:    ${ }^{11}$ The term "steady-state" means that the model assumes no variability in meteorological parameters over a one-hour time period.
    ${ }^{12}$ Federal Register, November 9, 2005; Volume 70, Number 216, Pages 68218-68261.

[^8]:    ${ }^{13}$ The albedo of a specified surface is the ratio of the radiative flux reflected from the surface to the radiative flux incident on the surface. Flux is the amount of energy per unit time incident upon or crossing a unit area of a defined flat plane. For example, the albedo for snow and ice varies from $80 \%$ to $85 \%$ and the albedo for bare ground from $10 \%$ to $20 \%$. Bowen ratio is the ratio of heat energy used for sensible heating (conduction and convection) of the air above a specified surface to the heat energy used for latent heating (evaporation of water or sublimation of snow) at the surface. The Bowen ratio ranges from 0.1 for the ocean surface to more than 2.0 for deserts; negative values are also possible.
    ${ }^{14}$ Weighting was based on wind direction frequency, as determined from a wind rose.
    ${ }^{15}$ USEPA (1986), and published as Appendix W to 40 CFR Part 51 (as revised).

[^9]:    ${ }^{16}$ AERMOD Implementation Guide, September 27, 2005, http://www.epa.gov/scram001/7thconf/aermod/aermod_implmtn_guide.pdf
    ${ }^{17}$ County of Riverside. http://www.city-data.com/county/Riverside_County-CA.html..

[^10]:    ${ }^{1}$ The term "consist" refers to the group of locomotives (typically between one and four) that provide power for a specific train.
    ${ }^{2}$ Two types of automatic idling control equipment are in use, known as ZTR SmartStart (typically retrofit equipment on low horsepower units) and AESS (typically factory installed on newer high horsepower units). Both are programmed to automatically shut off the engines of parked idling locomotives after a specified period of time, and to restart the unit if any of a number of operating parameters (battery state, air pressure, coolant temperature, etc.) reach specified thresholds.

[^11]:    ${ }^{3}$ USEPA (1998). Locomotive Emission Standards -- Regulatory Support Document. (Available at www.epa.gov/otaq/regs/nonroad/locomotv/frm/locorsd.pdf).

[^12]:    Vapor Density

[^13]:    Vapor Density
    Vapor Density ( $\mathrm{lb} / \mathrm{cu} \mathrm{ft}$ ):

[^14]:    1. Annual VMT estimated based on the vehicle age and odometer reading.
    2. Running exhaust emissions calculated using the EMFAC2007 model with the BURDEN output option.
    3. Running exhaust emission factor calculations assumed an average speed of 15 mph .
    4. Idling exhaust emissions factors calculated using the EMFAC2007 model with the EMFAC output option.
[^15]:    1. Annual truck trips based on annual product deliveries and a tanker truck volume of 8,000 gallons.
    2. Running exhaust emission factors ( $\mathrm{g} / \mathrm{mi}$ ) from EMFAC 2007 using the BURDEN output option. The EMFAC default model year distribution for L.A. County was used. 5. Emission factor calculations assumed an average speed of 15 mph .
    3. The PM10 emission factor includes engine exhaust emissions along with brake and tire wear. The DPM emission factor includes engine exhaust emissions only. 7. Engineering estimate based on personal observation.
    4. Idling exhaust emission factors from EMFAC 2007 using the EMFAC output option. The EMFAC default model year distribution for L.A. County was used.
[^16]:    Notes

    1. Organic fraction from ARBs SPECIATE database. Data is from
    "Headspace vapors 1996 SSD etoh $2.0 \%$ (MTBE phaseout)" option.
    2. Emissions were calculated for only chemicals that were in both the SPECIATE
[^17]:    ${ }^{1}$ USEPA. Thermally-Sensed Image of Houston, http://www.epa.gov/heatisland/pilot/houston thermal.htm, included in Heat Island Effect website, http://www.epa.gov/heatisland/about/index.html, accessed November 8, 2006.
    ${ }^{2}$ USEPA. AERMOD: Description of Model Formulation, Section 5.8 - Adjustments for the Urban Boundary Layer, pages 66-67, EPA-454/R-03-004, September 2004, accessed at http://www.epa.gov/scram001/7thconf/aermod/aermod mfd.pdf on November 9,
    ${ }^{3}$ Oke, T.R. City Size and the Urban Heat Island, Atmospheric Environment, Volume 7, pp. 769-779, 1973.
    ${ }^{4}$ Ibid for References 3 and 4.
    ${ }^{5}$ Ibid.

[^18]:    ${ }^{1}$ Population data were extracted from the Census 2000 Summary File 1 DVD, issued by the U.S. Department of Commerce, September 2001.
    ${ }^{2}$ Boundaries were extracted from ESRI shapefiles (*.shp) created from the U.S. Census TIGER Line Files downloaded from ESRI (http://arcdata.esri.com/data/tiger2000/tiger_download.cfm).

