Updates to OPGEE

OPGEE v3.0a candidate model

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resources engineering

Outline

- Part 1: Background and context
- Part 2: Updates to the OPGEE model
 - > Improving stream tracking
 - > Gas processing simulation with process simulators
 - Gas fugitives modeling with improved datasets and statistical modeling
 - > Gas functional unit allowed for primarily gas fields

Part 1: Background and context

Model is called Oil Production Greenhouse gas Emissions Estimator (OPGEE)

OPGEE model

• Estimates emissions given field parameters and technologies

The **first** open-source GHG tool for oil and gas operations

- Anyone can download, modify and use
- 36 published papers, complete documentation (~400 pp.) with all sources defined
- Funded by CARB, U.S. DOE, Carnegie Endowment, Ford Motor Co., Saudi Aramco



OPGEE model timeline

- Model development started in 2010
- First official version: OPGEE v1.0 released September 2012
- Second official version: OPGEE v2.0 released Feb 2018
- Third official version (candidate): OPGEE v3.0a Introduced today
- Bibliography at end of slides:

Used in studies of crude oil CI for

- US (Cooney et al. 2017, Yeh et al 2017, Brandt et al. 2016)
- Canada (Cai et al. 2015, Englander et al. 2015)
- China (Masnadi et al. 2018a)
- Globe (Masnadi et al. 2018b)

Methods development

- Overall (El-Houjeri et al. 2013)
- Drilling (Vafi et al. 2016)
- Gas processing (Masnadi et al. 2020
- Uncertainty (Vafi et al. 2014a, 2014b, Brandt et al. 2015)
- Time trends (Masnadi et al. 2018c, Tripathi et al. 2017)

Part 2: Updates to the model

Challenge 1: Model organization and stream tracking

- OPGEE v2.0 had drawbacks in model organization and stream tracking
 - Gas balance sheet tracked gas species, but other streams were not reliably tracked
 - Process units were not on individual sheets, and unclear exactly which mass flows were entering and leaving each sheet
 - Pressures and other properties of streams not reliably tracked
 - No easy way to navigate along the processing path
- OPGEE v3.0a includes a completely reworked model "skeleton"
 - All streams of oil, water, gas, etc. are tracked in mass flows
 - Conservation of mass ensured at process unit and total model level
 - Pressures, temperatures, and other properties tracked
 - Navigation aided by graphical view of process connections (PFD)

Improvement: OPGEE 3.0 process flow sheet map



Streams differentiated by color Green – Oil Red – Gas Blue – Water Yellow – Electricity Purple – Other gas Black – Raw bitumen

Graphical navigation



Trace flows along processing paths and click to navigate to sheets

| Stream num | her: | | 3 | 101 | 26 | 42 | |
|------------------------|------------------|---------|-----------------------------|-------------------------|-----------------------|----------------------------|--|
| Stream description: | | | Crude oil at well bottom | Water at well bottom | Gas at well bottom | Lifting gas to wellbore | |
| Phase | Component | Unit | 0 | 0 | 0 | Value | |
| Solid | Petroleum co | tonne/d | - | - | - | | |
| Liquid | Crude oil | tonne/d | 204.2 | - | - | | |
| Liquid | Liquified petro | tonne/d | - | - | - | | |
| Liquid | Water | tonne/d | 29 | 999 | | | |
| Liquid | Total liq. | tonne/d | 233 | 999 | - | | |
| Gas | N2 | tonne/d | - | _ | 0.9 | | |
| Gas | O2 | tonne/d | - | _ | | | |
| Gas | CO ₂ | tonne/d | - | - | 4.4 | | |
| Gas | H ₂ O | tonne/d | - | - | - | | |
| Gas | CH4 | tonne/d | | | 22.5 | | |
| Gas | C2H6 | tonne/d | | | 2.0 | | |
| Gas | C3H8 | tonne/d | - | - | 1.5 | | |
| Gas | C4H10 | tonne/d | - | - | 1.0 | | |
| Gas | со | tonne/d | - | - | - | | |
| Gas | H2 | tonne/d | - | - | - | | |
| Gas | H ₂ S | tonne/d | - | | 0.6 | | |
| Gas | SO ₂ | tonne/d | | | | | |
| Gas | Total gas | tonne/d | | | 32.9 | | |
| Electricity | Total Elec. | MWh/d | <u> </u> | | | | |
| Phase | Property | Unit | Value | Value | Value | Value | |
| all | Temp | ۰F | 150.0 | 150.0 | 150.0 | 150.0 | |
| all | Pressure | psia | 1227.7 | 1227.7 | 1227.7 | - | |

Mass flows into and out of each process unit tracked

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Flow sheet

| 000 | AutoSave 🔵 OFF |) | ∽∽ড ∓ | | | | | | | DPGE | E_3.0a_BET | A_frozen.xlsm ~ | | | | | | | | | | | ۹ ک |
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| A | A B C D E F G H I J K L M N O P Q R S T U V W X Y Z | | | | | | | | | | | | | | | | | | | | | | |
| 1 Active fi | eld flow sheet | | | F | Field: | Generic | | | | | | | To: Inputs | | To: Active | | To: Flows | | | | | | |
| 3 | Ind | ex code ↓ | | Stream nur | mber → | | | | | | | | | | | | | | | | | | |
| 4 number: | UM | | 1 | _ | | | | | | | • | | 10 | 11 12 | 13 | 14 | 4 15 | 5 16 | 3 1 | 7 11 | 3 19 | 20 | 2 |
| | | | | C+r | 2 | h | n | IIM | h | or | \rightarrow | | | | | | | | | | | | |
| Stream | STR | FAM N | | JU | CC | 7 | | un | ID | CI | | Stabilize | d Upgraded | Diluted | Crude oil to | Transported | Petcoke | NGI /diluent | LPG to | LPG to | Crude oil to | Crude oil to | |
| 5 description | AME | | 2 | | | | | | | | | storage | storage | storage | transport | refinery | upgrader | to dilution | crude oil | exports | upgrader | dilution | Matura |
| 7 Solid | Petroleum co M_P | °C | 4 tonne/d | value v | value - | value | value | value | value | Value - | value v | alue Value | - Value | | value | value - | | - value | value | - value | | Value - | - Value |
| 8 Liquid | Crude oil M_O | | 5 tonne/d | 204.2 | - | 204.2 | 204.2 | - | - | 204.2 | 204.2 | - 2 | 03.9 | | 203.8 | 203.8 | 3 - | | - | | | - | |
| 9 Liquid | Liquified petr M_LI | PG | 6 tonne/d | | | | | | | | | | - | - | | | | | - | - 2 | | | _ |
| 10 Liquid | Water M_W | v | 7 tonne/d | 28.6 | - | 28.6 | 28.6 | - | | 28.6 | - | | - | | - | - | | - | - | - | | - | |
| 11 Liquid 12 Gas | Total liquids M_TO N2 M_N | OTLIQ I2 | 8 tonne/d 9 tonne/d | 232.8 | - | 232.8 | 232.8 | | | 232.8 | 204.2 | - 2 | - 03.9 | | 203.8 | | | | | | | - | - |
| 13 Gas | O2 M_O | 02 | 10 tonne/d | - | - | - | - | - | - | - | | | - | | | | N Л . | | ן ד | • •• | | - | - |
| 15 Gas | H2O M_H | 120 | 12 tonne/d | - | - | - | - | - | - | - | - | | - | | | | IVIà | ASS | S TI | OV | VS- | - | - |
| 16 Gas | CH4 M_C C2H6 M C | 2 | 13 tonne/d | - | - | - | - | - | - | - | - | | - | | | | | | | ••• | ••• | - | - |
| 18 Gas | CaHe M_C | 3 | 15 tonne/d | - | - | - | - | - | - | - | - | - | - | | - | - | | | | - | - | - | - |
| 20 Gas | CO M_C | 20 | 16 tonne/d 17 tonne/d | - | | - | | - | | - | | | - | | | - | | | - | | | - | - |
| 21 Gas | H2 M_H | 12 | 18 tonne/d | - | - | - | - | - | - | - | - | | - | | | | | - | - | - | - | - | - |
| 23 Gas | SO2 M_S | 02 | 20 tonne/d | - | - | - | - | - | | - | - | | - | | | | | | - | | | - | |
| 24 Gas 25 Electricity | Total gas M_TO Total Elec. E_El | OTGAS | 21 tonne/d 22 MWh/d | - | - | - | - | - | - | | - | | - | | | | | | - | | | | - |
| 26 Phase | Property | | 23 Unit | Value N | /alue | Value | Value | Value | Value | Value N | Value V | alue Value | Value | Value | Value | Value | Value | Value | Value | Value | Value | Value | Value |
| 28 All | Temp (abs) T_AB | BS | 24 P 25 •R | 609.7 | | 609.7 | 609.7 | | | 549.7 | 549.7 | - 3 |)3.7 | | 519.7 | | | - | - | - 519. | r | - | - |
| 29 All 30 All | Pressure (abs P Contains oil OIL | 01 | 26 psia 27 (0-11 | 1556.6 | - 1 | 1227.7 | 1000.0 | - 1 | - 1 | 150.0 | 150.0 | - 1 | 0.0 | | 14.7 | | | | - | - 400.0 | | - 1 | |
| 31 Liquid | Crude oil API API | 0 | 28 •API | 30.0 | 8.0 | 30.0 | 30.0 | 8.0 | 8.0 | 30.0 | 30.0 | | 30.0 | | 30.0 | | | | | | | - | |
| 32 Liquid 33 Liquid | Solution gas GOR | AMA_O | 29 - 30 scf/bbl | 0.876 | 1.014 | 0.876 | 0.876 | 1.014 | 1.014 | 0.876 | 0.876 | 1.076 0 | 876 1.0 6.8 | | 0.876 | 0. | D | | | | - | 1.076 | - |
| 34 Liquid | Saturated oil FVF | _SAT | 31 bbl/STB | 1.170 | - | 1.138 | 1.117 | - | | 1.022 | 1.022 | - 1 | 149 | | 1.000 | 0 | Ρr | nn | her | ΤΙΑ | י 2נ | - | |
| 36 Liquid | Petroleum iso ISO_ | _CO | 33 - | 0.000 | - | 0.000 | 0.000 | - | | 0.000 | 0.000 | - 0 | 000 | | 0.000 | 0. | • • | | | | | - | - |
| 37 Liquid 38 Liquid | Petroleum FV FVF Petroleum vol OVF | _UNSAT | 34 bbl/STB 35 m3/std-m3 | 1,170 | - | 1,138 | 1,117 | | - | 1.022 | 1.022 | - 1 | 1 149 | | 1.000 | 0,969 | - | - | | - 1.00 | | - | |
| 39 Liquid | Petroleum de RHO | O_LB | 36 lb/ft3 | 49.146 | - | 49.900 | 50.415 | ** | | 53.684 | 53.684 | - 47 | 657 | | 54.687 | 56.432 | 2 - | | | - 67.17 | 5 | - | |
| 40 Liquid 41 Liquid | Petroleum flor Q_O |)_bbl | 37 tonne/m3 38 bbl/d | 0.787 | - | 0.799 | 0.808 | - | - | 0.860 | 0.860 | - 0 | 763 680 | | 0.876 | 0.904 | 1 - 3 - | | - | - 2 | - | - | - |
| 42 Liquid | Petroleum flo Q_O | O btu | 39 m3/d 40 Btu/lb | 259 | 17016 | 256 | 253 | 17210 | 17010 | 238 | 238 | 10 | 267 | | 233 | 18191 | 5 - | | | - 4 | | - | - |
| 44 Liquid | Energy densi LHV | _0 | 41 MJ/kg | 42.3 | 40.045 | 42.290 | 42.290 | 40.045 | 40.045 | 42.290 | 42.290 | - 42 | 290 | | 42.290 | 42.290 | - | | - | 50.000 | | - | - |
| 45 Liquid 46 Liquid | Energy densi LHV Energy flow r E_LH | _O_bbl / | 42 mmBtu/bbl 43 mmBtu/d | 5.0 8184 | - | 5.1 8184 | 5.1 8184 | - | - | 5.5 8184 | 5.5 8184 | - 8 | 4.9 | | 5.6 8167 | 5.8 | 3 - | | - | 8 | | - | - |
| 47 Liquid | Energy flow r E_LH | HV_O | 44 GJ/d | 8635 | - | 8635 | 8635 | - | | 8635 | 8635 | 8 | 620 | | 8617 | 8617 | 7 - | | - | - 104 | - | - | |
| C | i i otar molar nd TOTI | motana i | ionnoru | | | | | | | | | | | | | | | | | | | | |
| 4 b | Inputs Sec | condary inputs | Results | Uncertai | nty A | ctive Field | Flow S | Sheet | llocation | Energy S | ummary | GHG Summary | GHG S | ummary - NE\ | W VFF | Summary | Explor | ation | Drilling & d | evelopment | Reser | roir W | + |

Mass balance tracking and error flagging

Errors easier to spot with mass balance tracking across entire model

| | | | | Inputs | | | Outputs | | | | | | |
|--------|---|--|---|---|---|--|--|--|--|--|---|---|--|
| | | From production well | From makeup | From procesing stream | From rest of economy | | Reinjected as water | Reinjected as steam | Disposed | | Transport to market | To other stream | |
| P | Petroleum coke | | | 0.00 | | | | | 0.00 | 0.00 | 0 | 0.00 | |
| ι | Jnstabilized crude oil | 17925 | | | 0.00 | | | | | 0.00 | 17828 | 97 | |
| N | Natural gas liquids / Diluen Vater | 37532 | 0 | 74.67 | 0.00 | | 0 | 0 | 37532 | 0.00 | 74.67 | 0.00 | |
| | | | | Imported | stabilizer | Upgrading | | | | Vented and | Transport to | To other | |
| | | From well | From offsite | fuel gas | and tank | proc. gas | Flared | Reinjected | Consumed | fugitives | market | stream | |
| N | V2 | From well 30.82 | From offsite 0.00 | fuel gas 0.00 | and tank 0.00 | proc. gas 0.00 | Flared 3.52 | Reinjected 21.63 | Consumed 4.61 | fugitives 1.07 | market 0.00 | stream 0.00 | |
| N C | № D2 | From well 30.82 0.00 | From offsite 0.00 0.00 | fuel gas 0.00 0.00 | and tank 0.00 0.00 | proc. gas 0.00 0.00 | Flared 3.52 0.00 | Reinjected 21.63 0.00 | Consumed 4.61 0.00 | fugitives 1.07 0.00 | market 0.00 0.00 | stream 0.00 0.00 | |
| | √2 D2 CO2 | From well 30.82 0.00 145.27 | From offsite 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 | and tank 0.00 0.00 0.64 | proc. gas 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 | Reinjected 21.63 0.00 0.00 | Consumed 4.61 0.00 0.00 | fugitives 1.07 0.00 2.44 | market 0.00 0.00 0.00 | stream 0.00 0.00 126.88 | |
| | № D2 CO2 12O | From well 30.82 0.00 145.27 0.00 | From offsite 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 | and tank 0.00 0.00 0.64 0.00 | proc. gas 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 | Reinjected 21.63 0.00 0.00 0.00 | Consumed 4.61 0.00 0.00 0.00 | fugitives 1.07 0.00 2.44 0.00 | market 0.00 0.00 0.00 0.00 | stream 0.00 0.00 126.88 0.00 | |
| | N2 D2 CO2 12O CH4 | From well 30.82 0.00 145.27 0.00 741.28 | From offsite 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.64 0.00 85.28 | proc. gas 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 | Reinjected 21.63 0.00 0.00 0.00 530.71 | Consumed 4.61 0.00 0.00 0.00 113.03 | fugitives 1.07 0.00 2.44 0.00 97.28 | market 0.00 0.00 0.00 0.00 0.00 | stream 0.00 0.00 126.88 0.00 0.88 | |
| | N2 D2 CO2 12O CH4 C2H6 | From well 30.82 0.00 145.27 0.00 741.28 66.16 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.00 0.64 0.00 85.28 5.72 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 | Reinjected 21.63 0.00 0.00 0.00 530.71 6.64 | Consumed 4.61 0.00 0.00 0.00 113.03 1.41 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 | market 0.00 0.00 0.00 0.00 0.00 54.97 | stream 0.00 0.00 126.88 0.00 0.88 0.00 | |
| | N2 D2 CO2 12O CH4 CH4 C2H6 C3H8 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.00 0.64 0.00 85.28 5.72 3.18 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 | Reinjected 21.63 0.00 0.00 530.71 6.64 0.79 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 | market 0.00 0.00 0.00 0.00 0.00 54.97 0.00 | stream 0.00 126.88 0.00 0.88 0.00 44.35 | |
| | N2 D2 CO2 12O CH4 C2H6 C3H8 C3H8 C4H10 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 31.97 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.64 0.00 85.28 5.72 3.18 1.91 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 3.65 | Reinjected 21.63 0.00 0.00 530.71 6.64 0.79 0.19 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 0.04 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 0.55 | market 0.00 0.00 0.00 0.00 0.00 54.97 0.00 0.00 | stream 0.00 126.88 0.00 0.88 0.00 44.35 29.45 | |
| | N2 D2 CO2 CA2 CAH4 C2H6 C3H8 C4H10 C0 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 31.97 0.00 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0. | and tank 0.00 0.00 0.64 0.00 85.28 5.72 3.18 1.91 0.00 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 3.65 0.00 | Reinjected 21.63 0.00 0.00 530.71 6.64 0.79 0.19 0.00 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 0.04 0.00 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 0.55 0.00 | market 0.00 0.00 0.00 0.00 0.00 54.97 0.00 0.00 0.00 | stream 0.00 0.00 126.88 0.00 0.88 0.00 44.35 29.45 0.00 | |
| | N2 D2 CO2 H2O D2H4 C2H6 C3H8 C3H8 C4H10 C0 C0 C0 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 31.97 0.00 0.00 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.64 0.00 85.28 5.72 3.18 1.91 0.00 0.00 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 3.65 0.00 0.00 | Reinjected 21.63 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.019 0.00 0.00 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 0.04 0.00 0.00 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 0.55 0.00 0.00 | market 0.00 0.00 0.00 0.00 54.97 0.00 0.00 0.00 0.00 | stream 0.00 0.00 126.88 0.00 0.88 0.00 44.35 29.45 0.00 0.00 | |
| | N2 202 202 120 244 22H6 23H8 C3H8 C4H10 C0 24 20 24 22 20 24 22 20 24 22 24 22 24 22 24 22 24 22 24 22 24 22 24 24 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 31.97 0.00 0.00 18.75 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.64 0.00 85.28 5.72 3.18 1.91 0.00 0.00 0.00 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 3.65 0.00 0.00 0.00 2.14 | Reinjected 21.63 0.00 0.00 0.00 530.71 6.64 0.79 0.19 0.00 0.00 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 0.04 0.00 0.00 0.00 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 0.55 0.00 0.00 0.31 | market 0.00 0.00 0.00 0.00 54.97 0.00 0.00 0.00 0.00 0.00 | stream 0.00 0.126.88 0.000 0.88 0.000 44.35 29.45 0.000 0.000 0.000 0.000 0.000 | |
| | N2 D2 CO2 H2O CH4 22H6 23H6 C4H10 C0 C0 H2 H2S SO2 | From well 30.82 0.00 145.27 0.00 741.28 66.16 48.51 31.97 0.00 0.00 18.75 0.00 | From offsite 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | fuel gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | and tank 0.00 0.64 0.64 0.00 85.28 5.72 3.18 1.91 0.00 0.00 0.00 0.00 | proc. gas 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | Flared 3.52 0.00 16.59 0.00 84.67 7.56 5.54 3.65 0.00 0.00 0.2.14 0.00 | Reinjected 21.63 0.00 0.00 0.00 530.71 6.64 0.79 0.19 0.00 0.00 0.00 | Consumed 4.61 0.00 0.00 113.03 1.41 0.17 0.04 0.00 0.00 0.00 0.00 | fugitives 1.07 0.00 2.44 0.00 97.28 1.31 0.85 0.55 0.00 0.00 0.31 0.00 | market 0.00 0.00 0.00 0.00 54.97 0.00 0.00 0.00 0.00 0.00 0.00 | stream 0.00 0.01 126.88 0.00 0.88 0.00 44.35 29.45 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | |

| Totals | | | |
|--------------|------------------|----------|----|
| | | | |
| | | | |
| | | | |
| Total inputs | Iota. outputs | Batio | |
| 0 | 0 | 1.0000 | ОК |
| 17925 | 17925 | 000 | ОК |
| | | | |
| | | | |
| 74.67 | 74.67 | 1.0000 | OK |
| 37532 | 37532 | 1.0000 | ОК |
| | Total | | |
| Total inputs | outputs | Ratio | |
| 30.82 | 30.82 | 1.000000 | OK |
| 0.00 | 0.00 | 1.000000 | ОК |
| 145.91 | 145.91 | 1.000000 | ок |
| 0.00 | 0.00 | 1.000000 | ок |
| 826.57 | 826.57 | 1.000000 | ОК |
| 71.89 | 71.89 | 1.000000 | ОК |
| 51.69 | 51.69 | 1.000000 | OK |
| 33.88 | 33.88 | 1.000000 | ОК |
| 0.00 | 0.00 | 1.000000 | ОК |
| 0.00 | 0.00 | 1.000000 | ОК |
| 18.75 | 18.75 | 1.000000 | ОК |
| 0.00 | 0.00 | 1.000000 | ОК |
| 1179.50 | 1179.50 | 1.000000 | ОК |
| | | Overall | OK |

Gas as a primary product, different assessment points

- OPGEE 2.0 always required oil to be the primary product
- CI: gCO₂/MJ oil at refinery inlet
- OPGEE 3.0 allows for gas as the primary product
- CI: gCO₂/MJ **gas** at transportation system inlet



Oil at field boundary or refinery inlet

Gas at field boundary, transportation inlet or consumer

Challenge 2: Gas processing simulation

- OPGEE v2.0 had relied on "textbook" treatment of gas processing units
 - Models largely taken from classic text Manning and Thompson
 - Simple models of energy use and power requirements per unit of throughput
 - No way to customize process unit energy use for particular conditions
 - Feedback from industry: "Why not use process simulation tools?"
- OPGEE v3.0a includes "proxy" models generated from process simulation tools
 - Obtained access to Aspen HYSYS process simulation package
 - Work from template models of 4 key gas processing units
 - Acid Gas Removal, Dehydration, Demethanizer, Claus Unit
 - Simulated many cases at a variety of conditions
 - Generated statistical representations to predict Aspen HYSYS results

M.S. Masnadi *, P.R. Perrier , J. Wang , J. Rutherford , A.R. Brandt. Statistical proxy modeling for life cycle assessment and energetic analysis. Energy DOI: 10.1016/j.energy.2019.116882

Example: AGR modeling using process simulation software

- Modeled AGR unit in Aspen HYSYS chemical process simulation
- Five different solvents (amines):
 - > 1. MEA; 2. DEA (30% wt.); 3. DEA high load (35% wt.); 4. MDEA; 5. DGA
- Five independent variables:
 - 1. CO₂ concentration; 2. H₂S concentration; 3. Regeneration reflux ratio; 4. Regeneration feed temperature; 5. Acid gas pressure



Sampling approaches

AGR input variables to be sampled:

CO₂ concentration in gas H₂S concentration in gas Reflux ratio Regenerator feed temperature Feed gas pressure Deterministic sampling: Box-Behnken Random sampling: Latin hypercube



Total of ~9000 simulations of AGR systems across independent variables

Proxy modeling (cont'd)

- Experimental design: five independent variables
 - > Settings of each dependent on type of solvent applied
 - Model is allowed to adjust some parameters to make simulation converge (e.g., amine circulation rate)
 - > Save combination of 5 input variables plus multiple outputs

| Variable | MEA | DGA | DEA | DEA-HL | MDEA |
|--------------------------------------|--------------|--------------|--------------|--------------|--------------|
| Reflux ratio [-] | 1.5 - 3.0 | 1.5 - 3.0 | 1.5 - 3.0 | 1.5 - 3.0 | 6.5 - 8.0 |
| Regen. feed temp. [°F] | 190 - 220 | 190 - 220 | 190 - 220 | 190 - 220 | 190 - 220 |
| Feed gas pressure [psia] | 14.7 - 514.7 | 14.7 - 514.7 | 14.7 - 514.7 | 14.7 - 514.7 | 14.7 - 514.7 |
| Amine loading [wt.%] | 20 | 60 | 30 | 35 | 50 |
| Amine circ. rate ^{<i>a</i>} | Var. | Var. | Var. | Var. | Var. |
| H ₂ S conc. [mol.%] | 1 - 20 | 1 - 20 | 1 - 20 | 1 - 20 | 1 - 20 |
| CO ₂ conc. [mol.%] | 1 - 15 | 1 - 15 | 1 - 15 | 1 - 15 | 1 - 15 |

Training and testing dataset

After 9,000 simulations, dataset is split into training and testing

Training data used to fit optimal model functional form

Test data "held out" and never examined until reporting results

Tested variety of polynomial and other classical models

Quadratic regression balances complexity and fit

$$P = \beta_0 + \sum_{i=1}^5 \beta_a x_i + \sum_{i=1}^5 \sum_{j=i+1}^5 \beta_b \left(x_i \times x_j \right) + \sum_{i=1}^5 \beta_c x_i^2$$



Test fitted AGR model against hold-out set



Demethanizer product composition results



Composition and shares of C1, C2, C3 to streams harder to predict

Take-aways from process simulation

- Quadratic regression able to fit extremely well in most cases
- Most fits have R² >0.95
- OPGEE now produces, for cases within our sampled input ranges, results very close to Aspen HYSYS

Challenges for extension

Expertise and software license

Computational requirements very large for 10,000s of simulations

Unable to extrapolate – Can only model ranges of T, P, composition sampled

Challenge 3: Fugitive and vented CH₄ emissions

- OPGEE v2.0 relied on CARB survey data for fugitive and vented CH4
 - Survey of California producers required detailed reporting on emissions
 - Emissions factors obtained from EPA GHG Inventory
 - Survey unable to account for differences between US regions
 - Independent measurements lacking, with lots of studies done since OPGEE v2.0

 OPGEE v3.0a includes modern, independently measured field data for CH₄ emissions sources

- Two models: "site" and "component" level
- Component level data draws from multiple studies, 1000s of measured leaks
- Monte Carlo sampling approach includes super-emitter characteristics
- Able to recreate observed US wide emissions (e.g., Alvarez et al. 2018)

J.S. Rutherford, E.D. Sherwin, A.P. Ravikumar, G.A. Heath, J.G. Englander, D. Cooley, D. Lyon, M. Omara, Q. Langfitt, A.R. Brandt Closing the gap: Explaining persistent underestimation by US oil and natural gas production-segment methane inventories Submitted: Nature Energy

Different varieties of methane measurement inform our understanding of emissions quantities and sources



Policy and programs

Validation and assessment

Site-level emissions for production operations

Site level loss rates can be assessed from downwind or aboveview measurements

About 1000 sites from many basins compiled in Omara 2018

Relationship between production rate and loss rate imported and used to estimate site-level emissions



Source: Omara 2018

Collecting component-level data from various studies

- Informed by comprehensive literature search of component-level surveys (6 studies, ~3200 measurements)
- Filtered to (in current OPGEE version) include US studies only
 - Limited global coverage
 - Future model versions could include emissions distributions from other regions
- Data consolidated to consistent component and equipment type categories
 - Consistent component definitions (details in full paper) allow combination of samples from different studies
 - Consistent equipment definitions allows generation of component counts per equipment

Development of a bottom-up tool



Development of a bottom-up tool



Development of a bottom-up tool



Fraction loss rates: Oil wells (<100 mscf/bbl)



Results of loss fraction are strong function of well productivity

This effect has been seen repeatedly in the empirical literature

Using equipment distributions in OPGEE

- A separate equipment-level loss fraction distribution is generated for each productivity tranche
 - A stochastic leak process will tend to cause higher loss fraction in less productive wells, even if that well is same age or has similar equipment type
- Resulting equipment distributions can be used in two ways in OPGEE
 - 1. Deterministic: Create average equipment leakage rate for a given productivity tranche
 - 2. Uncertainty: Draw a given number of equipment realizations for the size of the population you are analyzing, randomized from the sampled equipment types

Validating the method

Ideally the method adopted in OPGEE would recreate the key results of the literature on methane emissions from the last 5 years

Key empirical features that have been found repeatedly that any tool should be able to show:

- 1. Larger emissions than classical EPA Greenhouse Gas Inventory methods
- 2. Strong dependence of loss fraction on site productivity
- **3.** Strong "heavy-tailed" behavior of emissions distributions: dependence on large emitters to drive large fraction of emissions

Validating against US estimate of production-segment emissions



US estimate of production-segment emissions by source



- Largest discrepancies between US EPA Greenhouse Gas Inventory and our results:
 - (2.1 Tg CH₄) Tank flashing and venting emissions
 - (1.4 Tg CH₄) Equipment leaks

Results for the upstream US oil and gas sector



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